

P&R 8.284 JRCC

T-727.01

CITY OF THOMPSON

Environment Act Proposal for the Waste Disposal Ground



Certificate of Authorization

J. R. Cousin Consultants Ltd.

No. 234

Date: 16/6/2



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May 2016



ACKNOWLEDGMENTS

To prepare this report various sources of information were investigated and researched. JR Cousin Consultants Ltd. (JRCC) wishes to thank the City of Thompson who contributed to the data and content of this report.

REMARKS

JR Cousin Consultants Ltd. has conducted this environment act proposal in accordance with generally accepted professional engineering principles and practices for the purpose of identifying conditions that may have an environmental impact on the site. The findings and recommendations reached in this report are based on information made available to JRCC during the investigation and conditions at the time of the site investigation. Conclusions derived in this report are intended to reduce, but not wholly eliminate the uncertainty regarding potential environmental concerns on the site, and recognizes reasonable limitations with regards to time, accuracy, work scope and cost. It is possible that environmental conditions may change from the date of this report. If conditions appear different from those encountered and expressed in this report, JRCC should be informed so that mitigation recommendations can be reviewed and adjusted as required. Historical data and information obtained from personal communication used in this report, are assumed to be correct, however JRCC has not conducted further investigations into the accuracy of this data. JRCC has produced this report for the use of the client, and takes no responsibility for any third party decisions or actions based on information contained in this report.

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Crown Lands Permit

Schedule A1 Sketch of WDG Property from file at Lands Branch

Waste Disposal Ground Operating Permit #42877

Crown Lands & Property Agency - Lands Branch, March 9, 2011 Email Correspondence

Table 1: Population and Waste Generation Projections – City of Thompson Waste Disposal Ground

Appendix B

LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report, AECOM 2008

LGD of Mystery Lake Waste Geotechnical and Topographic Investigation for the Waste Disposal Ground, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Scope Change #2 – Additional Test Holes, JR Cousin Consultants Ltd., 2012

Phase I Construction Works - Hydraulic Conductivity Test Results NTL September 14, 2012

Phase II Construction Works - Hydraulic Conductivity Test Results NTL October 29, 2013

Phase III Construction Works - Hydraulic Conductivity Test Results Stantec October 23, 2014

Appendix C

Plan 1: Site Layout with Approximate Location of Property Line

Plan 2: Final Cover Grading Contours and Final Drainage Plan

Phase I Works - Record Drawing Plan Set

Phase II Works - Record Drawing Plan Set

Phase III Works - Record Drawing Plan Set

Phase IV Works - Design Drawing Plan Set

Environment Act Proposal Form



Name of the development: City of Thompson Waste Disposal Ground Type of development per Classes of Development Regulation (Manitoba Regulation 164/88): Class 1 Legal name of the applicant: City of Thompson Mailing address of the applicant: 226 Mystery Lake Road Contact Person: Ms. Carol Taylor Postal Code: R8N 1S6 City: Thompson Province: Manitoba Phone Number: 204-677-7923 email: ctaylor@thompson.ca Fax: 204-677-7936 Location of the development: 4 km south of the City of Thompson Contact Person: Ms. Carol Taylor Street Address: Legal Description: Part NW 1/2 18, S 1/2 and NW 1/2 19 in TWP 77-3 WPM and in Part SE 1/2 24-77-4 WPM City/Town: Thompson Province: Manitoba Postal Code: R8N 1S6 Phone Number: 204-677-7923 email: ctaylor@thompson.ca Fax: 204-677-7936 Name of proponent contact person for purposes of the environmental assessment: Brett McCormac, P.Eng., JR Cousin Consultants Ltd. Mailing address: 91 A Scurfield Blvd Phone: 204-489-0474 Winnipeg, Manitoba Fax: 204-489-0487 R3Y1G4 Email address: bmccormac@jrcc.ca Webpage address: www.jrcc.ca Date: June 2, 2016 Signature of proponent, or corporate principal of corporate proponent: Printed name: Brett Mylormac

EXECUTIVE SUMMARY

General

The City of Thompson recently took ownership of the Thompson waste disposal ground (WDG) from the LGD of Mystery Lake. The WDG currently operates under Permit #42877, which expires on June 1, 2016. The Manitoba Conservation and Water Stewardship has directed that the City of Thompson must submit an Environment Act Licence proposal for the continued operation of a Class 1 waste disposal ground.

Project Background and Description

A four-phase construction project at the WDG for expansion and upgrade of the facility has been recently undertaken including construction of new WDG active cells, leachate collection piping and a leachate evaporation pond, a new contaminated soils remediation area and supply and set up of movable chain link fencing.

The City of Thompson plans to develop a 'One Stop Shop' which will include e-waste, household hazardous waste and used oil.

Population and Waste Generation

The Thompson WDG services the City of Thompson, the LGD of Mystery Lake, the Wuskawatim Generating Station, the Keeyask Generating Station and the Paint Lake Provincial Park. The City of Thompson contributes 94% of the total waste and the other populations contribute 6% of the total waste. The average per capita waste deposited at the WDG is 2.0 kg/person/day. Based on the WDG capacity and the projected incoming waste the WDG should have capacity until 2041.

Topography and Geotechnical Information

The past geotechnical investigations at the site showed there is a suitable in situ horizontal clay liner under the existing WDG area which can be used for the WDG expansion cells and the leachate pond. The test holes showed that sufficient clay does not exist further east of the existing WDG area and the perimeter dike with cut-off wall will have to be positioned close to the edge of the existing WDG area. The investigations also showed that the borrow pit contains suitable clay to use as a re-worked and re-compacted clay liner.

Environmental Effects

No negative residual effects are anticipated through the WDG expansion construction and continued operation, due to the mitigation measures and operating procedures described herein.



1.0 INTRODUCTION AND BACKGROUND

The development described herein is for the continued operation of the existing waste disposal ground (WDG) near Thompson, Manitoba. The WDG receives more than 5,000 tonnes of solid waste per year and is therefore considered a Class 1 WDG under the Waste Management Facilities Regulation 37/2016 which comes into effect on July 1, 2016.

1.1 Introduction

The City of Thompson recently took ownership of the City of Thompson Waste Disposal Ground from the Local Government District (LGD) of Mystery Lake. The WDG currently operates under Permit #42877. This permit expires on June 1, 2016. The Manitoba Conservation and Water Stewardship has directed that the City of Thompson to submit an Environment Act Licence proposal for the continued operation of a Class 1 Waste Disposal Ground. JR Cousin Consultants Ltd. (JRCC) was retained for the engineering services to complete the EAP document.

1.2 Contact Information

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1.3 Background Information

The WDG is located on Part NW $^{1}/_{4}$ 18, S $^{1}/_{2}$ and NW $^{1}/_{4}$ 19 in TWP 77-3 WPM and in Part SE $^{1}/_{4}$ 24-77-4 WPM, approximately 4 km south of the City of Thompson.

The WDG has a property of 55.2 ha (550 m x 1,005 m) of which, approximately 21 ha is used for the waste disposal ground and 34.2 ha is undeveloped. The WDG has been in operation since the late 1950s when the City of Thompson was developed. The WDG was owned and operated by the LGD of Mystery Lake until ownership was transferred to the City of Thompson on July 1, 2015.

The land is surrounded by forest and an established clay borrow pit to the north, forest to the south and west and a Manitoba Hydro transmission line and PTH 6, to the east. Access to site is via a gravel road running west off PTH 6.



A four-phase construction project at the WDG for expansion and upgrade of the facility has been recently undertaken. The four construction phases consisted of:

- Phase I 2012: Construction of a new active cell area surrounded by a perimeter dike with clay cut-off wall, construction of a leachate evaporation pond with leachate collection piping in the new active cell area, drainage works and supply of portable litter control fencing.
- Phase II 2013: Construction of a new active cell area surrounded by a perimeter dike with clay
 cut-off wall, extension of the leachate collection piping in the new active cell area, drainage
 works and construction of an upgraded contaminated soils remediation area.
- Phase III 2014: Construction of a new active cell area surrounded by a perimeter dike with clay cut-off wall, extension of the leachate collection piping in the new active cell area and drainage works.
- Phase IV Currently under construction to be completed in July/August 2016: Construction of a new active cell area surrounded by a perimeter dike with clay cut-off wall, extension of the leachate collection piping, drainage works, supply and set-up of 150 m of moveable chain link panel fencing to surround the active area.

The record drawings from the Phase I - 3 construction works and the design drawings from the Phase IV construction works are attached in Appendix C.

The site currently accepts household waste in a designated area at the north end of the site. The site also accepts metals, tires, white goods (if Freon has been removed by a licensed technician and a sticker is placed on the item), recyclables, burnable materials, batteries, used oil, concrete/ shingles and asbestos material in separate designated areas (permission from the City required prior to disposal). There is also a sludge-drying pit and a soil remediation area for contaminated soils (permission from the City required prior to disposal). The City of Thompson has recently moved the e-waste collection to the WDG and plans to develop a 'One Stop Shop', which will include e-waste, household hazardous waste and used oil. Currently the City collects household hazardous waste one weekend in September including paint, oil, cleaners, pesticides and chemicals.

The following materials are not accepted at the WDG: Oil based paint and varnish etc, hazardous waste (including paint thinner, aerosol cans, drain cleaner, pesticides, propane tanks and household cleaning supplies), fluorescent light ballasts, methyl hydrate, radiator coolant, antifreeze and items containing Freon.

Residential and commercial recycling service for the City is provided by the Thompson Recycling Center. Free curbside pickup is available throughout the city and the hours of operation are Monday to Friday 8:30 am to 4:30 pm. The Thompson Recycling Center recycles mixed paper, glass, aluminum, tin cans, plastics, cardboard, boxboard, and milk cartons.

Thompson operates a compost site at the Public Works Yard located at 120 Seal Road open from May to October 24 hours per day and 7 days per week to divert compostable materials from the WDG.



1.4 Existing Facility

The existing WDG currently operates with the following compounds/facilities:

- Active household waste disposal area below and above grade storage with perimeter dikes constructed as part of the 4-phase construction project from 2012 – 2016
- 2 cell contaminated soils remediation area
- 2-cell burn area
- Separate designated areas for scrap metal, white goods, tires
- A used oil eco-centre for oil and filters
- A battery depot shed
- Asbestos material disposal area
- Sludge drying bed
- Operator building with attached storage garage
- Equipment storage building for site equipment and materials
- A certified weigh scale at the entrance to the site for recording incoming waste tonnage and issuing tipping fees.

The site also has the following features:

- six groundwater monitoring wells located around the perimeter of the property, installed in 2005
- internal access roads constructed with granular material
- a lockable entrance gate
- site signage (i.e. entrance sign and drop off location signs)
- above-ground fuel tank for equipment refueling.

1.5 Existing Site Operations

Waste material is collected from the City of Thompson daily and delivered to the WDG. Commercial and industrial wastes are also known to be received by the WDG. During daily operations, the site has a gate attendant who handles tipping fees and directs individuals to the appropriate drop off locations, while a site operator conducts general site cleanup and waste movement, compaction and intermittent covering.

Based on the current schedule, the hours of operation are from Monday to Friday 8:00 am to 5:45 pm in the winter season and access extended to include Saturday from 9:00 am to 5:00 pm in the summer season. The facility is locked during closure hours.

1.6 Existing Operating Permit

The WDG is operating under the Waste Disposal Ground Operating Permit #42877. A copy of the permit is attached in Appendix A.



1.7 Description of Previous Studies

- LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report (prepared by AECOM, March 2008) to develop a closure plan for the WDG. After the report was reviewed it was decided to develop a plan to extend the lifetime of the WDG rather than decommission it.
- Local Government District of Mystery Lake Waste Disposal Area 2009 Master Plan by AECOM,
 January 2010 describing the current WDG as well as the master plan for upgrading and expanding the entire site.
- Existing Waste Disposal Facility Environmental Assessment Report (prepared by AECOM, February 2010) to complete an environmental assessment of the existing WDG to address any potential environmental liabilities and assess future expansion potential.
- LGD of Mystery Lake Waste Disposal Ground Overall Conceptual Layout and Phase I Design Works Environmental Assessment Submission (prepared by JRCC in June 2011) to obtain a Permit for the Class 1 operating facility for the upgrades and expansion of the WDG.



2.0 DESCRIPTION OF THE DEVELOPMENT

For each heading there is an information request from the Environment Act Proposal Form. These requests are repeated herein in italics followed by the pertaining response.

2.1 Land Title/Location

Certificate of Title showing the owner(s) and legal description of the land upon which the development will be constructed; or, in the case of highways, rail lines, electrical transmission lines, or pipelines, a map or maps at a scale no less than 1:50,000 showing the location of the proposed development:

The WDG is located on Part NW $^{1}/_{4}$ 18, S $^{1}/_{2}$ and NW $^{1}/_{4}$ 19 in TWP 77-3 WPM and in Part SE $^{1}/_{4}$ 24-77-4 WPM in the Province of Manitoba.

The land is leased under the Crown Land Permit No. GP 50804 issued by Manitoba Conservation, dated February 22, 2005, and has been attached in Appendix A. The Permit was transferred from the LGD of Mystery to the City of Thompson on July 30, 2015. See correspondence from the Crown Lands and Property Agency on September 17, 2015 attached in Appendix A.

A sketch available on file at the Lands Branch shows the WDG property lines. The sketch is attached in Appendix A. A legal property plan was never registered at the Land Titles office for the site.

2.2 Owner of Land and Mineral Rights

Owner of land upon which the development is intended to be constructed, and of mineral rights beneath the land, if different from surface owner:

Based on information provided by the Crown Lands and Property Agency Branch the mines and minerals and sand and gravel in NW 18, S $^{1}/_{2}$ and NW 19 in 77-3 WPM and SE 24-77-4 WPM are owned by Her Majesty the Queen in Right of the Province of Manitoba (see e-mail correspondence from the Crown Lands and Property Agency dated March 9, 2011, attached in Appendix A).

2.3 Existing Land Use

Existing land use on the site and on land adjoining it, as well as changes that will be made in such land use for the purposes of the development:

Within the former and active waste disposal areas the site is generally flat with a gentle slope from east to west. A steeper grade to the west is present in the south end of the site where former waste disposal activity may have occurred. The former waste disposal area is approximately 4-6 m higher than the surrounding area. The average elevation changes from 225 m in the east to 210 m in the west. A bedrock outcrop protruding up to 8 m above the surrounding ground exists east of the site, parallel to PTH 6. The area surrounding the site is forested with an undulating slope to the west. North of the WDG is an established clay borrow site located on Crown Land.



2.4 Land Use Designation/Zoning Designation

Land use designation for the site and adjoining land as identified in a development plan adopted under the Planning Act or the City of Winnipeg Act, and the zoning designation as identified in a zoning by-law, if applicable:

Based on information provided by the City of Thompson, the WDG site is currently zoned under LGD Zoning by-law 541 LD as Limited Development which lists "Waste disposal grounds and landfill sites, as regulated by the Province" as an acceptable land use.

2.5 Description of Development

Description of proposed development and schedule for stages of the development, including proposed dates for planning, design, construction, commissioning, operation, and decommissioning and/or termination of operation (if known), identifying major components and activities of the development as applicable (e.g. access road, airstrip, processing facility, waste disposal area, etc.).

2.5.1 Project Schedule

The existing permit expires June 1, 2016 and Manitoba Conservation and Water Stewardship have directed that the City of Thompson submit an Environment Act Licence proposal for the continued operation of a Class 1 waste disposal ground prior to June 1, 2016.

Phase IV of the WDG upgrade are currently underway and are due to be completed in July/August of 2016. No other major construction works are scheduled for the WDG.

The WDG expected lifetime and closure date is discussed in Section 2.5.4.2 below.

2.5.2 Existing WDG Site Evaluation

The location of the WDG will not be altered from the existing footprint.

According to the *Guidelines for the Siting of a Class I Waste Disposal Ground in Manitoba* (1994) and the Waste Management Facilities Regulation 37/2016, Schedule B, the siting of the WDG expansion cells would require the following provincial guidelines and minimum setback requirements:

- Watersheds with surface water flow through the site.
- Sites underlain with sand, gravel, sandstone, limestone.
- Sites on the edge of steep slopes, subject to erosion and land sliding.
- Sites within 2 km of wetlands.
- Bedrock outcrops.
- Karst terrain.
- Fractured bedrock.



- Unstable terrain.
- Areas of unpredictable geology.
- Sites with shallow water tables or perched aquifers.
- Groundwater pollution hazard areas.
- Areas within 100 year flood plain.
- Areas with limited access to roads or utilities.
- Sites within 400 m of a residence.
- Sites within 400 m of a potable water well.
- Sites within 400 m of a cemetery.
- Sites within 400 m of a natural gas pipeline or an underground utility corridor.
- Sites within 2 km of a critical habitat area.
- Sites within 2 km of a designated park or historic site.
- Sites within 100 m from a public road or railway right of way.
- Sites within 1 km from a body of surface water.
- Sites within 8 km of an airport or setback as described in the local zoning plan.

The existing site complies with all the setback criteria with the exception of a surface water body (swamp) located southwest of the existing site which is within 1 km of the WDG. This requires design measures to prevent leachate migration and a variance by Manitoba Conservation to decrease the minimum separation distance. Given the location in northern Manitoba with numerous lakes, it is considered unlikely a WDG could be located such that the minimum setback distance is satisfied. Upon discussion with Manitoba Conservation and Manitoba Water Stewardship, the setback distance can be reduced if design measures are taken to ensure leachate is not able to reach the lake.

An important concern in evaluating Class I WDG sites is the protection of water quality, and human health and safety. The above setbacks also consider aesthetic qualities of the surrounding landscape and safety issues for nearby transportation routes.

The above siting requirements are established to ensure that if a WDG fails to adequately contain leachate, the site's natural conditions will protect groundwater and surface water resources, and control the migration of landfill gases. Preference should be given to sites located in areas where there is clay or till of low permeability $(1 \times 10^{-7} \text{ cm/sec or less})$ to ensure groundwater protection and minimal migration of landfill gases. If soils of sufficiently low permeability are not available, a geomembrane liner should be considered for containment.

Groundwater pollution hazard areas occur where carbonate rock or sand and gravel deposits are at or near ground surface. In these areas seepage from leachate could readily percolate to the water bearing zone and cause groundwater pollution. Groundwater pollution hazard maps were not available for the WDG site, however, based on test holes taken at the site, the existing WDG is



underlain by clay and silty clay in varying depths. Sand and gravel is not present at or near the ground surface in the active or former waste disposal areas. Sand was encountered beneath the clay and silty clay layer in MW401, MW402 and MW407 by AECOM, at depths of 2.1 m, 2.4 m and 5.2 m, respectively. As the WDG has a clay silt layer across the site and likely no direct routes to the groundwater aquifer through sand and gravel, the WDG is not likely located in a groundwater pollution hazard area.

2.5.3 Projected Service Population

2.5.3.1 City of Thompson

Census population information was obtained from Statistics Canada for the City of Thompson, from 1971 to 2011. The population decreased by 5,745 people from 1971 to 2001 but has remained relatively stable from 2001 - 2011. Details of the historic population data is shown in Table 21 below.

Table 2.1 – Historic population data for the City of Thompson

Year	Population	Average Annual Growth Rate
1971	19,001	
1976	17,291	-2.06%
1981	14,288	-4.61%
1991	14,977	0.45%
1996	14,385	-0.80%
2001	13,256	-1.62%
2006	13,446	0.29%
2011	13,123*	-0.49%

^{*}The 2011 census population was adjusted from 12,829 to 13,123.

The future population projections for the City of Thompson will be based on a conservative growth rate of 0.52% as discussed in the City of Thompson Wastewater Treatment Plant Upgrade/Expansion Functional Design Report prepared by Stantec in January 2014 for sizing of the proposed wastewater treatment plant. Table 2.2 below shows the projected future population for the City of Thompson in 5 year increments.

Table 2.2 - Projected future population data for the City of Thompson

Year	Population	Average Annual Growth Rate
2011	13,123	
2016	13,468	0.52%
2021	13,822	0.52%
2026	14,185	0.52%



Year	Population	Average Annual Growth Rate
2031	14,557	0.52%
2036	14,940	0.52%
2041	15,332	0.52%
2046	15,735	0.52%
2051	16,149	0.52%

2.5.3.2 LGD of Mystery Lake

The WDG also services the LGD of Mystery Lake. Population data for the LGD of Mystery Lake from the 2011 census was 10 people. The same future growth rate as Thompson of 0.52% is assumed to continue for the LGD population.

2.5.3.3 Other Populations

The Thompson WDG also accepts waste from the Wuskawatim Generating Station, the Keeyask Generating Station and the Paint Lake Provincial Park.

According to the City of Thompson, waste from the Wuskawatim Generating Station and the Paint Lake Provincial Park is expected to continue at the same rate in the future. Waste from the Keeyask Generating Station is expected to continue at the same rate for the next 3 - 4 years during construction and then drop off. For the purposes of WDG sizing the current rates are expected to continue in the future.

See Table 1 attached in Appendix A for a summary of the current and projected future populations.

2.5.4 Projected Waste Generation

A weigh scale was installed at the WDG in 2010 to monitor incoming waste. The total tonnage from 2010-2015 was provided to JRCC and summarized in the following table. The total quantity of recycled material by the Thompson Recycling Center from 2010-2015 was also provided and shown on the following table.

Table 2.3 – Total Recycled Material and Total Waste Received at the Thompson WDG

	2010	2011	2012	2013	2014	2015
Total Waste Generated (tonnes)	12,672	13,227	11,361	10,785	10,791	11,364
Total Recycled Material (tonnes)	664	838	836	912	991	944
Total Waste deposited at the WDG (tonnes)	12,008	12,389	10,525	9,873	9,800	10,420
Percentage of Waste Recycled	5.2%	6.3%	7.4%	8.5%	9.2%	8.3%



The average waste generation from 2012 - 2015 is 11,075 tonnes per year which is less than the waste generation from 2010-2011 of 12,950 tonnes per year. The average waste generation rate from 2012-2015 was used as a basis of calculation for future waste generation from the City of Thompson residents.

The total amount of recycled material has increased from 5.2% in 2010 to a peak of 9.2% in 2014. The future recycling rate of 8.7% of total waste is expected to continue in the future which is the average recycling rate from 2013 - 2015.

The City of Thompson also operates a composting site at the Public Works Yard which accepted 80 tonnes of material in 2015 which is expected to continue in the future.

The breakdown of waste received at the WDG for 2015 was provided to JRCC. The waste received was categorized by residential and commercial and by City of Thompson waste and waste from other sources. The other sources are the Wuskawatim and Keeyask Generating Stations and the Paint Lake Provincial Park. The following table shows the material breakdown for 2015.

Table 2.4 – Breakdown of Total Waste Received at the Thompson WDG in 2015

Source	Туре	Waste Delivered to WDG (tonnes)	Percentage of Total Waste
	Residential	4,884	47%
City of Thompson	Commercial	4,923	47%
	Total	9,807	94%
	Residential	491	5%
Other Sources	Commercial	123	1%
	Total	614	6%

Based on the breakdown of material received at the WDG the 'Other Sources' represent approximately 6% of the total waste received at 614 tonnes which is expected to continue in the future. The waste generated from the City of Thompson is approximately 50% residential and 50% commercial which is expected to continue in the future.

The following table shows the per capita waste production from the City of Thompson residents (including residential and commercial waste) from 2010 – 2015.

Table 2.5 – City of Thompson Per Capita Waste Generation Rates

	2010	2011	2012	2013	2014	2015
Total Waste from City of						
Thompson Deposited at WDG	11,394	11,775	9,911	9,259	9,186	9,806
(tonnes)						



	2010	2011	2012	2013	2014	2015
Population of the City of Thompson	13,188	13,123	13,191	13,260	13,329	13,398
Per Capita Waste Deposited at WDG (kg/person/day)	2.4	2.5	2.1	1.9	1.9	2.0

To calculate the average per capita waste generation the estimated population per year was utilized. Note the population after 2011 was estimated based on a 0.52% growth rate from the 2011 census population. Based on the calculations the average per capita waste generation rate has ranged from 2.5 kg/person/day to 1.9 kg/person/day with an average from 2012 – 2015 of 2.0 kg/person/day.

Statistics Canada (2012) indicates that a waste generation rate of 1.1 kg/person/day, in Manitoba, is typical for residential waste only, and 2.3 kg/person/day is typical for residential and non-residential (i.e. commercial, industrial, institutional) waste combined. These values do not take into consideration waste diversion efforts through recycling, composting and burning. Including the actual recycling rate in Thompson of 0.2 kg/person/day and the waste sent to the WDG of 2.0 kg/person/day, the total waste generation from the City of Thompson is in line with the Statistics Canada report and the per capita waste sent to the WDG of 2.0 kg/person/day is reasonable to assume for the remaining lifetime of the WDG.

2.5.4.1 Burning at the WDG

According to the City of Thompson approximately 30% of the material received at the WDG is burned at the burn pit and this rate is expected to continue in the future or slightly decrease. The Manitoba Conservation and Water Stewardship released a guideline entitled *Burning Solid Waste at a Waste Disposal Ground or a Waste Transfer Station* effective November 24, 2014. The document outlines the requirements for burning of waste at a WDG, which must be followed including the types of materials suitable for burning which are: separated and readily combustible materials such as boughs, loose straw, leaves, paper products, cardboard non salvageable untreated wood and packing materials made from wood.

The guideline also states that CWS intends on phasing out most burning at waste disposal grounds and waste transfer stations, however, no timelines were provided.

For the purposes of remaining capacity of the WDG it will be assumed that no burning of material will be completed to act as a safety factor on the WDG capacity. If 30% of the incoming material is continued to be burned, the WDG capacity will increase by 30%.

2.5.4.2 Remaining Capacity

The remaining capacity of the WDG was calculated based on a previously conducted survey of the WDG taken on April 14, 2011 and compared to the designed final



contours of the WDG. A maximum waste elevation of 235.75 m was assumed with 4:1 side slopes to the perimeter dikes and a top sloped 1.0% to the west. The proposed final contours are shown on Plan 2 attached in Appendix C. The total remaining capacity of the WDG in 2011 based on the assumptions stated is $906,853 \, \text{m}^3$.

Of the total airspace available approximately 20% of the space will be comprised of cover soil and therefore 725,482 m³ will be available for solid waste. The WDG utilizes a steel-wheeled waste compactor, which can typically compact waste to a density of 475 kg/m³, if compaction occurs regularly. This density was utilized in estimating the volume of waste received in the waste disposal cells, as the operator indicated that compaction occurs regularly at the site. Therefore with the airspace available the WDG can accept an additional 344,604 tonnes of solid waste. The following is a summary of the calculations described above.

Total Remaining Capacity of WDG in 2011 (volume) 906,853 m³

Remaining Capacity of WDG for Waste (volume) 725,482 m³

Remaining Capacity of WDG for Waste (mass) 344,604 tonnes

Therefore based on the previously stated assumptions the WDG has the remaining capacity to allow operation to 2041, which is 25 years from the date of this report. See Table 1 attached in Appendix A for more information. The actual volume of incoming waste, actual compaction rates, the amount of material used for soil cover and the amount of material burned must be monitored to re-assess the remaining capacity on an ongoing basis.

2.5.5 Geotechnical, Topography and Groundwater Investigations

AECOM conducted a site investigation, topographic survey and completed test holes in October 2005. The full results are summarized in the *LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report* prepared by AECOM in March 2008. The report is attached in Appendix B.

On April 13 and 14, 2011, JR Cousin Consultants Ltd. (JRCC) conducted a geotechnical and topographic investigation. The site investigation was conducted over the existing WDG area and the proposed expansion area to supplement existing geotechnical information obtained in past reports and to identify changes in topography since the 2005 AECOM survey. The JRCC report entitled LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground, June 2011 is attached in Appendix B.

JRCC completed a subsequent report entitled *LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works*, September 2011 that investigates a potential WDG expansion east of the existing WDG and recommended additional testing be completed. The report is attached in Appendix B.



JRCC also completed a report entitled *LGD* of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Scope Change #2 – Additional Test Holes, March 2012 which investigated the potential clay borrow area, the depth to clay liner through the existing waste and the boundary of the horizontal clay liner on the east side of the existing WDG area. The report is attached in Appendix B.

The following sections summarize the previously completed reports.

2.5.5.1 Geotechnical Information

From AECOM Report March 2008

A total of 11 test holes were completed by AECOM in 2005. Eight of the test holes were drilled along the perimeter of the WDG and three drilled within the former waste cells to determine the depth of waste. Test hole locations and test hole logs by AECOM are shown on the attached report in Appendix B.

The following is an excerpt describing the soil stratigraphy from the *LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report* prepared by AECOM in March 2008:

"The soil stratigraphy encountered in the test holes completed along the perimeter of the site generally consists of a 1.0 m to 2.1 m thick layer of high plastic clay overlying a layer of varved clay which ranges from 1.0 m to 4.0 m in thickness. Along the bedrock outcrop that runs along the east end of the site, the varved clay is underlain by sand to auger refusal. Beyond the bedrock outcrop, the varved clay is underlain by a layer of varved silt which ranged from 3.7 m to 7.6 m in thickness. In TH403A, the material encountered consisted of 2.1 m of clay fill and 0.6 m of waste underlain by varved clay. Auger refusal was encountered in MW401, TH401A, MW402 and MW407. The refusal depth ranged from 3.0 m to 7.3 m below the surface.

Soils encountered in TH408 consisted of clay fill to the end of the test hole (4.6 m). The test hole was completed near a clay stockpile in the centre of the WDG. The depth of clay fill in this test hole indicates that this location may have been a former clay stockpile area. In TH409, the material encountered consisted of 0.3 m of clay fill underlain by a 2.7 m thick layer of waste, 1.5 m of clay fill, and another 1.5 m thick layer of waste followed by native soils composed of high plastic clay varved with clayey silt. Similarly, the material encountered in TH410 consisted of 0.3 m of clay fill underlain by a 2.4 m thick layer of waste followed by native varved clay soils."

Shelby tube samples and laboratory analysis of soil samples taken in the expansion cell area were not completed as part of the report.



From JRCC Report June 2011

A total of 13 test hole were drilled at the WDG site. Three test holes were drilled in the leachate pond area (TH1-TH3), seven test holes were drilled in the WDG expansion cell areas (TH4-TH10) and three test holes were drilled through the former waste disposal areas (TH11-TH13). Bagged samples were sent for laboratory analysis and three Shelby tube samples for hydraulic conductivity analysis.

The general soil profile observed in TH1 – TH10 was an average of 0.4 m of peat followed by 3.1 m of brown high plastic clay, in some instances with trace silt, followed by grey low – high plastic clay, with trace silt to a depth of 6.0 m below ground. Laboratory analysis of the soil samples found a Plasticity Index from 18 to 43 and the percentage of clay from 85.5% - 96.4%. The test results show that all samples tested most likely meet the Manitoba Conservation guideline of a hydraulic conductivity of 1 x 10^{-7} cm/s, with the exception of a sample from TH8 [3.9-6.0 m] which had a Plasticity Index of 18 and a clay content of 85.5%. Three Shelby tube samples were analyzed from TH3, TH6 and TH8 and hydraulic conductivities of 8.9×10^{-9} cm/sec, 1.4×10^{-8} cm/sec and 9.9×10^{-9} cm/sec, respectively were obtained which are less than the required 1×10^{-7} cm/sec for a clay lined cell.

Laboratory analysis of the bagged samples from the clay liner beneath the existing waste (TH12 and TH13) found an average plasticity index of 41 and average clay content of 91.3% and a similar soil structure to the samples which did have an in situ hydraulic conductivity of less than 1×10^{-7} cm/sec. Based on these results, it is likely that the clay liner under the existing waste does meet the Manitoba Conservation guidelines for a WDG liner. Shelby tube samples could not be obtained in the layer and therefore in situ hydraulic conductivity testing could not be completed.

From JRCC Report September 2011

A total of 13 test holes were excavated, 11 at the proposed expansion area east of the existing WDG (TH14-24) and two test holes at the borrow pit area (TH25-26). The soil profile in the test holes taken east of the WDG area varied significantly with some holes consisting of sandy, silty low plastic clay and others with high plastic clay present, some beneath a layer of waste. See the test hole logs for more details. The test holes taken in the borrow pit area found high plastic clay.

Laboratory analysis was completed on eight bagged samples from the test holes. The analysis concluded that the soils from TH23 (0.4 – 3.2 m), TH24 (1.2 – 3.7 m), TH25 (0 – 1.6 m) and TH26 (0 – 2.2 m) were considered suitable for use as an in situ clay liner or when re-worked and recompacted. The soils from TH15 (0.6 – 1.9 m), TH21 (1.5 – 3.4 m), TH22 (2.4 – 4.5 m) and TH25 (1.6 – 4.1 m) had clay contents above 50% but had Plasticity Index less than 25 and therefore hydraulic conductivity testing of the soils would be required to determine if the soils could achieve a hydraulic conductivity of 1 x 10^{-7} cm/sec or less.



The report recommended that a perimeter dike with vertical cut-off walls extending a minimum 1.0 m into the horizontal clay liner be installed at the edge of the suitable horizontal clay liner. However, the location of the edge of the horizontal clay liner would require additional testing. The report also recommended additional test holes in the borrow pit and additional laboratory analysis of the borrow pit soil.

Based on the recommendations of this report a subsequent geotechnical investigation was completed by JRCC.

From JRCC Report March 2012

A total of 14 test holes were excavated during the investigation. Two test holes were excavated to determine the depth of waste near the vertical cut-off wall to be constructed as part of the Phase I Works (TH27 – TH28). Seven test holes were excavated along the east edge of the WDG to determine the edge of the in situ horizontal clay liner (TH29 – TH33 and TH 39 – TH40). Five test holes were excavated in the borrow pit area to determine the suitability of the clay soil for use as a reworked and re-compacted clay liner (TH34 – TH38).

The soil profile at the borrow pit was found to be a combination of high and medium plastic clay. The soil profile east of the WDG varied considerably between test holes and included layers of existing waste, high plastic clay and some silty, sandy, low plastic clay. The test holes taken on top of the existing WDG area were waste from 0-5 m which was the capacity of the excavator.

Four representative bagged soil samples from the borrow pit area and four representative bagged samples from the area east of the WDG were submitted for laboratory testing. All samples except one from TH31 were deemed suitable for use as a clay liner. One Shelby tube sample from east of the WDG area was tested and found to have an in situ hydraulic conductivity of 2.1 x 10^{-8} cm/s. One sample from the borrow pit was re-worked and re-compacted and found to have a hydraulic conductivity of 2.1×10^{-8} cm/s.

Summary of Geotechnical Information

Overall the geotechnical investigations showed there is a suitable insitu horizontal clay liner under the existing WDG area which can be used for the WDG expansion cells and the leachate pond. The test holes showed that sufficient clay does not exist further east of the existing WDG area and the perimeter dike with cut-off wall will have to be positioned close to the edge of the existing WDG area. The investigations also showed that the borrow pit contains suitable clay to use as a re-worked and recompacted clay liner.



2.5.5.2 Topographic Information

The topography of the WDG was surveyed and found that the top of the existing former and current waste disposal area slopes from east to west. The existing ground surrounding the WDG is approximately 4 m - 6 m lower than the top of waste and slopes to the southwest. The proposed leachate pond area slopes to the southeast with a maximum elevation of approximately 209.37 m at the northwest end and a minimum elevation of approximately 207.64 m at the southeast corner. There is a rock outcrop east of the former and current waste disposal area which slopes up to an elevation of 225.0 m towards PTH 6.

2.5.5.3 Groundwater Information

Groundwater Investigation from Past Report

Six monitoring wells were installed around the WDG site by AECOM in 2005. Two wells were installed up gradient of the groundwater flow (MW 401 and 407), two wells installed cross-gradient of the groundwater flow (MW 402 and 406) and two wells were installed down gradient from the groundwater flow (MW 403 and 405). Monitoring well locations by AECOM are shown on the attached report in Appendix B.

The following is the description of the groundwater table from the *LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report* prepared by AECOM in March 2008.

"The groundwater levels recorded in the overburden monitoring wells on November 21, 2005 range from 0.87 m to 2.35 m below ground surface, with the exception of MW403, in which the water level was 0.19 m above ground. Based on these water levels, the direction of flow within the overburden is towards the west-southwest. This direction corresponds with the general slope of the topography in this area. The magnitude of the horizontal gradient within the overburden soils (change in water elevation with distance) is about $0.069 \, \text{m/m}$ "

Groundwater Investigation from JRCC Report June 2011

No standing water was observed in the test holes, with the exception of TH1 and TH2, taken in the proposed leachate pond area. The water in the test holes was caused by standing water on the ground surface around the test holes which flowed into the test holes.

TH6 was left open for four hours to allow for longer-term water infiltration to occur. After the elapsed time no standing water was observed in the hole, however, there was caving at approximately 3.6 m below the ground surface.



Groundwater Investigation from JRCC Report September 2011

Short-term groundwater conditions were assessed in each test hole by observing standing water in the test holes prior to backfilling the holes. No standing water was observed in the test holes with the exception of TH20, which had leachate water infiltration at the bottom of the waste layer and TH21, which had high rate water infiltration from the surface.

TH15 was left open for approximately two hours to allow longer-term water infiltration to occur. When the hole was re-visited caving of the test hole walls occurred and no standing water was observed.

Groundwater Investigation from JRCC Report March 2012

Short-term groundwater conditions were assessed in each test hole by observing standing water in the test holes prior to backfilling the holes. Water infiltration was observed in TH33 at a depth of 3.6 m with a cave-in observed at 1.0 m. Water infiltration was observed in TH29 at a depth of 1.3 m and leachate infiltration to the test hole was observed in TH40 at a depth of 2.2 m. No standing water or water infiltration was observed in the remainder of the test holes.

The JRCC report notes: "Groundwater in the test holes depends on high static groundwater conditions and on seasonal conditions, i.e. snowmelt and rainy seasons. Other assumptions relating to the groundwater elevation cannot be made at this time as water levels will normally fluctuate seasonally."

2.5.6 WDG Cell Liner Requirements

The Manitoba Siting Guidelines for Class I WDG Sites require a clay liner of a waste disposal cell to have a minimum thickness of 1.0 m and have a hydraulic conductivity of $1 \times 10^{-7} \text{ cm/sec}$ or less. If suitable soils are not available for this construction, then a synthetic geomembrane liner can also be utilized. This low level of permeability in the active cell liner is required to ensure that leachate or wastewater does not impact surrounding groundwater resources.

2.5.6.1 Liner for the WDG

The existing former and active cell area will utilize the insitu soil beneath the existing waste as the cell liner. During the site investigation by JRCC on April 13, 2011, three test holes were drilled in the existing waste, and two of the holes, TH12 and TH13, were taken through the existing waste and into the soil beneath. The soil layer under the existing waste was described as brown/ grey high plastic clay, very stiff with some silt lenses. Laboratory analysis of the clay found the plasticity index to be 39 and 43, and a clay content of 87.0% and 95.5% which means the clay would most likely meet the Manitoba Conservation minimum hydraulic conductivity of 1×10^{-7} cm/s. Typically soils with a Plasticity Index above 25 and a clay content above 50% should have a hydraulic conductivity of 1×10^{-7} cm/s or less.



Shelby tubes could not be taken in the clay beneath the garbage due to caving in of the garbage layer that did not allow the Shelby tube to pass. Although the permeability test could not be performed, the plastic index above is an indicator that the clay soils would have a low permeability, and would meet the Manitoba Conservation requirements. The clay layer will continue to serve as the WDG liner of the existing and former waste disposal area.

AECOM drilled two test holes, TH409 and TH410, in the former waste disposal area through the waste. Both test holes found a layer of clay and silt beneath the waste described as "silty, brown, moist, firm, high plastic clay, varved with clayey silt lenses". Laboratory analysis was not completed on the soils, however, the description of the layer is consistent with the JRCC site investigation findings.

Based on test holes and laboratory analysis, a minimum 1.0 m thick insitu clay liner which meets the Manitoba Conservation guideline of hydraulic conductivity less than 1×10^{-7} cm/s also exists in the cell expansion areas and leachate pond area. The expansion cell perimeter dikes included a 3 m wide vertical clay cut-off wall constructed of clay excavated from the cell area or from the clay borrow pit located north of the WDG and tied into the horizontal clay liner.

The new WDG cells, contaminated soils area and leachate pond construction works included Shelby tube testing at the end of each construction phase to verify the asconstructed liner met the hydraulic conductivity requirements. All test results exceeded the Manitoba Conservation requirements. The following is a summary of the as-constructed test results from the construction works. Test results are included in Appendix B.

Phase I

•	TH1 - 1.5-2.1 m	$1.6 \times 10^{-8} \text{cm/s}$
•	TH2 - 0.2-0.8	$9.7 \times 10^{-9} \text{cm/s}$
•	TH4 - 4.5-5.1	$3.1 \times 10^{-8} \text{cm/s}$
Phase I	I	
•	TH5 - 0.3-0.9 m	$3.6 \times 10^{-8} \text{cm/s}$
•	TH7 - 0.3 - 0.9 m	$9.5 \times 10^{-9} \text{cm/s}$
•	TH8 - 0.3 - 0.9 m	$1.9 \times 10^{-8} \text{cm/s}$
Phase I	II	
•	TH2 – 1.5 – 2.1 m	$7.5 \times 10^{-9} \text{cm/s}$
•	TH5 - 0.3 - 0.9 m	$2.0 \times 10^{-8} \text{cm/s}$
•	TH6 - 0.3 - 0.9 m	$1.2 \times 10^{-8} \text{ cm/s}$



2.5.6.2 Contaminant Migration

The potential impact of leachate from the WDG on the underlying groundwater aquifer was evaluated to determine the geological sensitivity rating for the site. The following assumptions were made:

- leachate movement by advection
- no natural attenuation of leachate
- an average hydraulic conductivity of 1.61 x 10⁻⁸ cm/s for the clay layer determined by averaging the hydraulic conductivity of the Shelby tube samples from TH3, TH6 and TH8 and the 9 samples from the as-construction tests
- a downward vertical gradient of 0.67 m/m calculated by averaging the vertical gradients between the 6 monitoring wells based on November 21, 2005 water levels recorded by AECOM
- an average effective porosity of 0.35 calculated by averaging the porosity from the three Shelby tube samples and assuming effective porosity is 70% of total porosity.

The vertical rate of contaminant migration was calculated using Darcy's Law where:

$$q=rac{\mathit{Ki}}{\mathit{n_e}}$$
 where q = average linear velocity of the contaminant K = average hydraulic conductivity of the soil i = average hydraulic gradient $\mathit{n_e}$ = average effective porosity of the soil

Using the above parameters the average downward velocity of the contaminant is calculated as:

$$q = \frac{(1.61 \times 10^{-8})(0.67)}{(0.35)} = 3.09 \times 10^{-8} \frac{cm}{s} = 0.00973 \, m/year$$

Using a minimum liner thickness of 1 m, the contaminant would reach the bottom of the clay liner in 103 years corresponding to a geological sensitivity rating of low – water moving vertically will reach the aquifer within several decades to a century.

From the test hole information the high plastic clay layer was observed to be between 3.1 and at least 5.6 m thick. Also, no infiltrating water was observed in any of the test holes taken to a depth of 6 m. This suggests that the ground water aquifer exists below 6 m from existing ground and contaminants must pass through at least 3.1 m of liner material, greatly increasing the time it would take for a contaminant to reach the groundwater aquifer.



2.5.7 Cover System

Based on the Waste Management Facilities Regulation 37/2016, which comes into effect on July 1, 2016, a Class 1 WDG must cover the waste with a layer of soil or another material approved by the director, compacted to a depth of at least 15 cm on a daily basis. The current permit specifies cover in accordance with M.R. 150/91 which indicates all solid waste must be covered once per month.

From discussion with Manitoba Conservation, based on the size of the City of Thompson WDG an alternate cover schedule may be approved. The City of Thompson WDG is considered a Class 1 WDG, however, the size is smaller than a 'typical' Class 1 WDG in Manitoba and daily covering of material would result in very low waste:soil ratios, reducing the lifetime of the WDG. The WDG accepts an average of 27.5 tonnes/day, which would occupy approximately 58 m³ of space based on a compaction rate of 475 kg/m³. The active portion of the active area is expected to have a surface area of approximately 1,700 m². Therefore the average daily waste accumulation will be approximately 0.035 m per day. If daily cover of 150 mm of soil was applied, the waste:soil ratio would be 0.2:1, which is much too low for efficient operation of the WDG. A typical waste:soil ratio at a WDG should be approximately 5:1. To achieve the ideal waste:soil ratio the waste would have to be covered once every 21 days. It is therefore requested that the licence indicate cover material is required once every three weeks.

Hydrocarbon contaminated soils delivered to the WDG for remediation are intended to be utilized as some of the cover material, after meeting criteria for daily cover. The remainder of the soils used for cover material will be borrowed from a clay borrow area identified near the WDG site.

The WDG operations plan, Plan 7 of the Phase I Works record drawings attached in Appendix C indicates that the depositing of waste and cover material will continue until the elevation is a maximum of 235.75 m, approximately 15 metres above the existing waste. The maximum waste height will be approximately 25 m above the leachate collection piping. As the land filling progresses above ground, temporary berms will be created around the active portion of the active cell as indicated on the plan. This will ensure precipitation in contact with the wastes is sent to the leachate evaporation pond and clean water is shed off the cell and directed to the perimeter ditches.

The proposed method of final WDG cover is discussed under the closure criteria Section 2.5.17 in this report.

2.5.8 Leachate Management System

The new active cell floors were graded in such a way that liquid or leachate from within the active portion of the active cell area is collected by 200 mm corrugated polyethylene piping at one end, and drained by gravity to the leachate evaporation pond. The pond is a one cell structure with a clay liner of permeability less than 1×10^{-7} cm/s to prevent groundwater contamination. The operator would be required to set up temporary berms in the active cell to divert clean run-off water away from the active portion of the cell and minimize leachate production.



Leachate Pond Sizing

Sizing of the leachate evaporation pond is based on the expected hydraulic loading created by precipitation in the active portion of the active cell of the WDG. Environment Canada precipitation data for the Thompson A data station listed an average annual precipitation of 509.2 mm for the years of 1981 - 2010. This average will be assumed for future precipitation quantities. The leachate pond will be sized to accommodate one year's worth of precipitation falling on the active portion of the active cell area, as well as the precipitation falling directly on the leachate pond. Based on the Phase I active cell area of 5,150 m², and an active portion of the active cell of 1/3 the surface area or 1,717 m² the volume of leachate produced by the active portion of the active cell is 874 m³/year.

It is preferred to operate the evaporation pond with a liquid level of 0.5 m. The shallow liquid level will assist with evaporation by increasing the surface area exposed to the atmosphere and allowing more sunlight to be absorbed to increase the water temperature, to assist with evaporation. However, the yearly precipitation for Thompson is 509.2 mm, which is already over the 0.5 m liquid level in the cell (assuming 1 year of precipitation in the cell at one time). If the evaporation pond was larger, more precipitation would be stored, and the liquid level from precipitation would continue to be over the 0.5 m. Therefore, the cell was sized so that the expected leachate quantity resulted in a 0.5 m liquid level in the pond. The maximum liquid level in the pond would be 1.01 m which would occur if 1 year of leachate (0.5 m) and 1 year of precipitation (0.501 m) was present in the cell at once.

The leachate pond was constructed with a top of dike elevation of 209.2 m and a cell floor elevation of 207.7 m for a total depth of 1.5 m. The cell has a 40 m x 40 m flat bottom area, 4:1 inner side slopes, 3:1 outer side slopes and a 2 m wide top of dike. The pond can hold 885 m^3 of liquid with a liquid level of 0.5 m and $1,964 \text{ m}^3$ with an operating level of 1.01 m.

Evaporation Rates and Alternative Disposal Options

The City of Thompson has a total of 142.9 degree days above 15°C compared to 421.5 for the City of Winnipeg according to Environment Canada Canadian Climate Normals data from 1981 - 2010. The average humidity in Thompson for the months of May – September is 67.4% and for Winnipeg is 68.9%. The City of Thompson annual precipitation is 509.2 mm compared to 521.1 mm for Winnipeg. Evaporation from the leachate pond will depend primarily on precipitation, temperature and humidity. With similar precipitation and humidity to Winnipeg and significantly lower temperatures it is expected that the evaporation rates at Thompson will also be significantly lower than Winnipeg. Also, during years of higher than average precipitation, net evaporation rates will be lower and successive years of high precipitation will result in increased liquid levels in the pond.

The Leachate Management at Waste Disposal Grounds and at Waste Transfer Stations produced by Manitoba Conservation and Water Stewardship dated June 9, 2015 was reviewed to determine alternative leachate disposal options permitted by Manitoba Conservation. The



following are the four options described in the report with discussion related to the City of Thompson WDG:

- Leachate Evaporation: The document lists evaporation ponds as the preferred method
 to manage leachate and discusses the use of floating aerators to reduce odors and help
 increase evaporation rates. The WDG have experimented with mechanical evaporators
 at the site with some limited success. Even with mechanical evaporators, the
 evaporation rate is limited by the temperature and humidity of the air, as discussed
 above.
- Leachate Treatment: The document discusses pre-treatment and complete treatment methods consisting of both biological and physical/chemical treatments. Following complete treatment, surface discharge may be considered by Manitoba Conservation. Complete leachate treatment at the Thompson WDG would require an advanced treatment plant to be constructed which would require extensive design based on the expected leachate characteristics. A treatment plant would have high capital costs and high operating costs including power consumption and chemical costs and would require a highly trained operator to maintain. Even with complete treatment, surface discharge may not be approved. Overall, on-site leachate treatment would not be feasible for the Thompson WDG.
- Discharge to a Wastewater Treatment Plant: The document states leachate may be sent to a WWTP depending on the treatment type and capacity of the WWTP. Authorization would be required from the Director of Conservation and Water Stewardship. The City of Thompson is planning to construct a new WWTP to service the City. Tanker trucks could potentially collect liquid from the pond and haul it to the WWTP for co-treatment with municipal wastewater. Laboratory test results from the leachate would be required to ensure the WWTP could handle the loading and provide treatment of the parameters of concern. This option would likely require a road to be constructed to access the pond. Assuming a tanker truck volume of 9,092 L (2,000 gal) it would take 116 truck loads to lower the pond liquid level by 0.5 m. This option would potentially be feasible for the WDG if the new WWTP was able to accept the leachate and the option was approved by Manitoba Conservation, however the capital costs for road construction and on-going trucking costs would be very high.
- Leachate Collection and Recirculation: The document discusses leachate re-circulation
 to essentially create a bioreactor landfill. The document states that the option would
 only be considered in Manitoba for sites with a double liner system compatible with
 high strength leachate. From discussion with Manitoba Conservation, this option would
 not be approved for the Thompson WDG as the insitu clay liner would not be sufficient
 for this type of system.

Overall the only feasible option for the Thompson WDG, permitted by Manitoba Conservation is to operate the evaporation pond. The operator must minimize leachate production through the use of cover material, operating a small active cell and constructing temporary berms to divert clean surface water to the perimeter ditches. If liquid levels cannot be maintained at an acceptable level, hauling to the WWTP could be investigated.



2.5.9 Monitoring Wells

Manitoba Conservation guidelines suggest a groundwater monitoring system comprised of three monitoring wells (one upstream and two downstream of the WDG, on the basis of the assumed direction of the groundwater flow). Typically the installation of three monitoring wells is required for the construction of any new WDG. Six monitoring wells installed by AECOM in October 2005 exist on the current WDG site.

Three of the monitoring wells are within the proposed final berms around the former and active WDG cell. It was discussed with Manitoba Conservation and agreed that if these wells continue to be accessible and functional they will remain within the berms and continue to be used by extending the casing, as waste accumulates in the cells.

It is recommended that the City of Thompson perform sampling and testing from all monitoring wells on a regular basis as part of its operation and maintenance plan. Every sample should be tested for the baseline ground water chemistry parameters listed in the Guidelines for the Siting of a Class 1 Waste Disposal Ground in Manitoba. Test results should be compared to past samples to determine if any concerns exist.

2.5.10 Drainage

The WDG has a perimeter drainage ditch around the active cell to intercept surface water from outside of the WDG to prevent the surface water from entering the site. The entire WDG site, by design, will be graded to ensure any surface water will drain away from the site into the perimeter ditches.

Within the active cell area, small temporary berms are to be constructed around the active portion of the cell to ensure clean surface water does not enter the active portion of the cell. Only precipitation falling on the active portion of the active cell, in contact with waste will be directed to the leachate collection pond. Clean surface water falling in the active cell area, but not the active portion will be directed to the perimeter berms through grading of the cell cover. Clean surface water will then be pumped over the perimeter berms of the active cell into the perimeter ditches.

The perimeter ditch directs clean surface water to a discharge ditch which will send water to the surface water body located southwest of the WDG. The final drainage plan is shown on Plan 2 attached in Appendix C.

2.5.11 Contaminated Soils Remediation Area

The contaminated soil remediation area was upgraded as part of the Phase II construction works. The area was constructed with two cells using a 0.5 m thick re-worked clay horizontal liner, new 1 m high berms surrounding the area with 3:1 side slopes and leachate collection piping along the west side of the remediation area. Cell 1 has a surface area 1,531 m² and Cell 2 has a surface area of 1,019 m².



2.5.12 Burn Area

Separated and readily combustible materials such as boughs, loose straw, leaves, paper products, cardboard non salvageable untreated wood and packing materials made from wood will be burned in the designated burning area. Burning activities will only take place under the direct supervision of the facility operator, when weather conditions are favourable and only an amount of material that can be extinguished by the end of operating hours.

As per Regulation 37/2016 the burn pit must be located 400 m from a building not located on the facility site, 50 m from an active area and 50 m from a compost area or an area used to collect flammable materials. The burn pit location with 50 m setback is shown on Plan 1 attached in Appendix C. The WDG active area cannot be within the setback area shown.

2.5.13 Asbestos Disposal Area

It was originally intended to construct the new perimeter dikes of the WDG on the east side to surround the existing asbestos disposal area. However, during the geotechnical site investigations east of the existing WDG area it was discovered that a suitable insitu clay horizontal liner does not exist at all areas. From discussion with Manitoba Conservation at the time, it was decided to leave the existing asbestos area undisturbed and construct the perimeter dikes closer to the existing WDG cell area, rather than excavating and re-compacting a horizontal liner beneath the asbestos area.

A new asbestos disposal area will have to be established within the perimeter dike area, once the Phase IV construction works are complete. Asbestos will be deposited at the WDG only if asbestos is packaged in accordance with the current edition -of *Guidelines for an Asbestos Operations and Maintenance Program* from Workplace Safety and Health Division. All asbestos shall, be covered immediately with a minimum of metre of material and the location for disposal shall be documented and recorded in the Facility operation and maintenance plan accessible to all operators.

2.5.14 Sludge Drying Area

The existing WDG site includes a sludge drying bed which accepts dewatered biosolids (stabilized sludge) from the City of Thompson WWTP. Sludge is also accepted from the Keeyask Generating Station.

2.5.15 Access Road

The existing access road is an all weather road in good condition. The main access highway is PTH 6 located approximately 150 m east of the site. The interior roads appear to be in good condition and are maintained by the WDG operator on an ongoing basis.



2.5.16 Fencing and Signage

The existing locking gate will be utilized at the entrance to the site. The gate will be locked except during hours of operation. Three sections of litter control fencing are currently being utilized at the active face of the active cell to help control wind-blown litter.

The Phase IV construction works currently under contract includes the supply and set-up of 150 m of 1.8 m high moveable chain link fencing. The fencing will be installed surrounding the active portion of the active cell to contain wind-blown litter. The fencing can be re-located as the active cell moves.

The leachate pond is surrounded by a 1.2 m high 4-stranded barbed wire fence.

Currently signs are located at the entrance to the site and at various locations within the site to direct the public to the correct waste disposal areas, and to ensure public safety on site. Signage will continue to be used on the site.

According to the Waste Management Facilities Regulation 37/2016 the signage at the entrance to the WDG facility must contain the following information:

- the name of the facility
- · the operating hours of the facility
- the types of materials that may be deposited at the facility
- the types of materials that are not accepted at the facility
- a 24-hour emergency contact telephone number.

The existing sign at the entrance to the facility contains the name of the facility and the hours of operation but does not contain information about the types of waste accepted at the site and does not contain an emergency telephone number.

2.5.17 Proposed 'One Stop Shop'

The City of Thompson is planning to create a 'One Stop Shop' at the WDG site to accept household hazardous waste, e-waste, used oil, and fridges. The project is currently in the early stages of planning. The current plan is to hold the e-waste in an existing building on-site and collect household hazardous waste in a steel storage container (sea can). The used oil building will be re-located at the 'One Stop Shop'. Thompson is working with Product Care Manitoba (household hazardous waste) and the Manitoba Association for Resource Recovery Corp. (MARRC) for oil recovery and e-waste.

The 'One Stop Shop' will be open part time year round (Tuesday and Thursday in the winter and Tuesday, Thursday and Saturdays in the summer).



2.5.18 Decommissioning and Closure

The waste disposal cells, when at maximum height above ground, will be decommissioned in accordance with the Waste Management Facilities Regulation 37/2016 Part 4 - Closure Requirements and the Manitoba Conservation and Water Stewardship Supporting Document for Waste Disposal Ground or Waste Transfer Station Site Closures April 2014 guideline.

A preliminary closure plan will be submitted to the director within 12 months of the licence being issued. A final closure plan will be submitted to the director at least six months before the permanent closure of the facility.

Upon closure, the WDG household waste are will be covered with a minimum of 0.5 m compacted clay soil and topsoil for seeding. The surface of the capped cells will be graded to allow positive drainage away from the cell towards the perimeter ditching. The decommissioned cells will be seeded with grass to provide an aesthetically pleasing environment, and regular monitoring of the site will continue to occur to determine if there are any impacts to groundwater at the site.

2.5.19 WDG Maintenance and Operation

The intended method of land filling is to compact (a typical municipal compaction rate of 475 kg/m³ has been assumed) and cover the active area of the active cell with 0.15 m thickness of clean soil cover material once every three weeks, or as stipulated in the Environment Act Licence. The cover material in each instance will serve to eliminate the wind-blown wastes, rodents, birds, moisture and fires. Active areas in the cell will propagate in an upward direction as waste collects and is compacted.

As the active portion of the active cell is re-located, temporary berms are to be constructed at the edge of the active portion to prevent clean surface water from entering the new active portion of the cell. Clean surface water will either be directed to the perimeter ditching by surface grading or pumped into the perimeter ditches, if grading is not possible. The general operation/filling of the active cells is shown on Plan 7 of the Phase I Works record drawings attached in Appendix C.

By way of this document and plans the operator is instructed that the solid waste disposal ground cells, when at their maximum height above existing waste level, as previously described must be decommissioned by covering with clay soil and topsoil as per Manitoba Conservation guidelines. Positive drainage away from the site must be provided and maintained.

In accordance with Regulation 37/2016 the City of Thompson must employ at least one person certified with the Manager of Landfill Operation certificate provided by the Solid Waste Association of North America (SWANA) by July 1, 2019. This person does not have to be at the WDG at all times. However, at all times when the WDG is open to the public, at least one operator at the facility must have their Landfill Operations Basics certification or equivalent.



The active cell area will be restricted to employees only, with the public having access to the dumping area of the active portion of the active cell. The operator is to limit the waste type to those previously discussed. The operator is to provide onsite signage to direct public to the dumping areas of acceptable wastes.

The life expectancy of the WDG is based upon the application of the above operation and management practices. The usable life of the WDG will be reduced if these practices are not followed.

The WDG operators will also handle the following various tasks:

- collecting tipping fees at the gate entrance
- recording waste tonnage dropped off at the site
- directing the public to the appropriate drop off locations
- moving, covering and compacting waste material in the active waste disposal cells
- moving ash from the burn cells into the active cells after material is completely extinguished
- inspecting and maintaining the fencing, gate and lock
- ensuring the entrance gate is locked at all times when the operators are not present
- ensuring burning activities are continuously monitored and recorded
- ensuring the liquid level in the leachate pond is maintained at an acceptable height
- ensuring only leachate from the active cell is drained to pond
- ensuring recyclable materials and tires are hauled off site regularly
- ensuring that unacceptable waste products are not dumped at the site
- ensuring internal access roads are cleared and maintained regularly
- ensuring the movable chain link fencing is properly positioned around the active cell area to prevent blown litter
- ensuring windblown waste material is cleaned up regularly
- controlling insects, rodents and other vectors onsite.



3.0 POTENTIAL ENVIRONMENTAL IMPACTS

The biophysical and socioeconomic environment as related to the development, and potential impacts of the development on the environment.

3.1 Releases to Air, Water, Land

3.1.1 Air

Prevailing winds in the area can carry odours if the waste disposal areas are exposed and there is unobstructed wind sweep across the site. These odours have the potential to be a nuisance to nearby residents.

While there is potential for odours at the WDG site during operation, the active waste disposal activities are located well beyond the minimum distance of 400 m from the nearest resident. In addition, with waste cover material being utilized, odours are not likely to become a nuisance. The site is also bordered by forest which acts as a windbreak to reduce the spread of odours. Due to the evaporation of liquid leachate, odours from the leachate pond are not expected to be significant.

There is also a potential for greenhouse gas emissions during operation works from heavy equipment and transport vehicles.

3.1.2 Water

Pollutants that have the potential to be released into surface water and groundwater during the operation of WDG would be from leachate production. Pollutants potentially produced in waste disposal cells would generally include nutrients, coliforms, volatile organics, suspended solids, heavy metals, inorganic compounds and organic carbons that are typical for leachate produced from residential and commercial wastes.

Pollutants that have a potential to be released into the surface water or groundwater during the WDG expansion construction activities, would include petroleum hydrocarbons (PHCs) from heavy equipment spills/leaks and sediments from soil erosion.

3.1.3 Land

The footprint of the WDG will not be altered from the current layout with the exception of the Phase IV construction works to be completed in the summer of 2016 on the east side of the WDG area. Leachate and windblown litter can impact surrounding lands if not contained. Ground areas disturbed by construction activities can be impacted through soil erosion if not covered or revegetated shortly after works are completed.

Pollutants that may be released to the land are predominantly PHCs, which could be released during construction activities from equipment leaks, and/or re-fuelling incidences and could result in impacts to the soils/land.



3.2 Wildlife

The typical concern on any construction project is that wildlife species would be displaced through the construction works. However, the footprint of the WDG will not be altered.

3.3 Fisheries

The typical concerns with impacts to fish and fish habitat are from sediments released during construction and the leachate discharges into a body of surface water utilized by fish species. These impacts could include the reduction of water quality or physical disturbances that would create an unfavorable environment for fish or fish eggs. As leachate will be contained on site and silt fencing will be maintained during construction works, significant impacts on fisheries are not expected.

3.4 Vegetation and Forestry

The typical concern on any construction project is the removal of vegetative species through the construction works, however the footprint of the WDG will not be altered.

3.5 Noise Impacts

There is a potential for noise impacts in the immediate area of expansion due to the heavy equipment utilized during construction, however these impacts are not expected to be significant, as heavy equipment is already being used at the site during daily maintenance. No additional noise impacts are expected during the continued operation of the WDG as no additional maintenance equipment will be utilized.

3.6 Health and Safety

There is a potential for impacts to the health and safety of workers and the public during the construction works and operating of the WDG, as heavy equipment is utilized on site while the public has access to other areas of the WDG.

3.7 Socio-Economic Implications

The final phase of the WDG expansion is not expected to have adverse socio-economic impacts. In fact, construction related economic activity is likely to have a positive economic impact on the City of Thompson.

3.8 Aesthetics

The WDG will have an impact on the general aesthetics of the area, as the active cell area is currently several metres above the original ground elevation and is planned be extended several more metres prior to WDG closure. The site is surrounded by forest on the north, west and east side and a tree line existing on the east side between the WDG and PTH 6. Windblown litter is also a concern at WDG sites as it creates a site which can be aesthetically unpleasing.



4.0 MANAGEMENT PRACTICE

Proposed environmental management practices to be employed to prevent or mitigate adverse implications from the impacts identified above.

4.1 Mitigation of Impacts to Air

The WDG is located well beyond the minimum setback distances to nearby residents which reduces the potential for nuisance odours. Regular covering of the waste disposal cells will reduce the odours generated from the site.

Emissions from construction equipment and WDG equipment will be controlled through regular maintenance, and should meet all provincial and local emission standards. Dust suppression methods (i.e. water spraying) can be utilized at the construction site if dry conditions create excessive dust through construction activities and transport, and becomes a nuisance to nearby residents.

4.2 Mitigation of Impacts to Water

Impacts to surrounding surface waters and groundwater from leachate production in the waste disposal cells will be reduced by the WDG clay liner, which meets the permeability requirements of Manitoba Conservation.

Leachate produced will be collected and contained in a leachate evaporation pond as per Manitoba Conservation requirements. Leachate production will be minimized by covering all waste except for the active portion of the active cell and diverting clean surface water to perimeter ditches. Leachate management is discussed in detail in Section 2.5.8.

Siltation in the drainage ditch from disturbed soil areas during the construction works will be mitigated through the installation of silt fencing. Dike and ditch slopes would also be seeded with grass to control erosion.

4.3 Mitigation of Impacts to Land

To minimize impacts to the surrounding land, perimeter dikes around the WDG cells will act to contain leachate and movable fencing installed around the active area will act to contain windblown litter to the designated areas. Intermittent cover will also act to prevent windblown litter and the production of leachate in the waste disposal cells. Disturbed ground surface areas will be seeded upon completion of construction works to minimize soil erosion.

4.4 Mitigation of Impacts to Vegetation

Tree removal will not be required, as the footprint of the WDG will not be expanded. Vegetation outside of this construction area will not be damaged and the tree line surrounding the site will remain intact.



4.5 Mitigation of Noise Impacts

To minimize the potential for noise impacts, construction equipment and WDG maintenance equipment should have mufflers working properly, and construction activities should be limited to daylight hours only.

4.6 Mitigation of Impacts to Health and Safety

To minimize impacts to health and safety of workers and the public, the construction contractor should have a safety program in place, in accordance with all federal and provincial health and safety regulations. During construction, access to the construction areas will be limited to the construction crew only. Personal protective equipment will be worn by all personnel while in the construction area, in accordance with the contractor's safety program.

The WDG will develop an operations manual that includes an emergency response plan, waste acceptance procedures and policies and drawings and descriptions necessary for the safe and efficient operation of the facility.

4.7 Aesthetics

Impacts to aesthetics at the WDG site would be mitigated by maintaining the tree line along the east border of the site to reduce the visual impacts of the WDG from PTH 6. Windblown litter would be reduced by cover material placement in the waste disposal cells and would be cleaned up regularly as part of the WDG operations, which would increase aesthetics of the site.



5.0 RESIDUAL AND CUMULATIVE EFFECTS

Residual environmental effects remaining after the application of mitigation measures, to the extent possible expressed in quantitative terms relative to baseline conditions

No negative residual effects are anticipated through the WDG expansion construction and continued operation, due to the mitigation measures described above. Positive residual effects to the service area are expected from the increased waste disposal capacity, which will allow for continued growth of the service population without immediate concern for waste disposal availability. In addition, the construction of a containment liner around the existing and proposed waste disposal cells, would minimize the potential for contaminants leaving the WDG site.



6.0 MONITORING AND FOLLOW-UP

Proposed follow-up activities that will be required at any stage of development (eg. Monitoring, inspection, surveillance, audit, etc.)

The clay liner around the WDG cells will be inspected and tested in the presence of Manitoba Conservation after the Phase IV construction works are complete. The liner would be tested for hydraulic conductivity to ensure that the requirements of the Environment Act Licence are met. The WDG liner and leachate pond liner was tested after construction phases 1-3 and met the Manitoba Conservation requirements.

Long-term monitoring on the WDG site would include regular testing of the groundwater monitoring wells for water quality parameters described in the Environment Act Licence. The operator is to monitor and record the liquid level in the leachate pond to establish long-term evaporation rates and determine the need for alternative leachate management options as discussed in Section 2.5.8. The operator is to maintain records of type and quantity of waste received at the site, a record of all burning activities. If there are any concerns with the operation of the WDG or with possible groundwater contamination, the City of Thompson is to contact the local environment officer and the Environmental Approvals Branch of Manitoba Conservation to discuss options.



7.0 FUNDING AND APPROVALS

Name and address of any Government Agency or program (federal, provincial or otherwise) from which a grant or loan of capital funds have been requested (where applicable). Other federal, provincial or municipal approvals, licences, permits, authorizations, etc. known to be required for the proposed development, and the status of the project's application or approval.

Funding for preparation of the EAP document will be undertaken by the City of Thompson. Funding for WDG equipment and maintenance including any minor projects at the WDG such as development of the 'One Stop Shop' will be undertaken by the City of Thompson. No other approvals, licences or permits are expected for continued use of the Waste Disposal Ground.



8.0 PUBLIC CONSULTATION

Results of any public consultations undertaken or to be undertaken in conjunction with project planning.

Public consultation by the City of Thompson through a designated public forum has not been conducted. Public comments received by Manitoba Conservation through the public registry during the Environmental Act Proposal review period will be reviewed and addressed.



9.0 CONCLUSION

Based on the construction works that have been completed at the WDG and the implementation of the mitigation measures identified in Section 4.0 above, no significant negative environmental impacts are anticipated.

The proponent would like to complete the requirements of the Environment Act Proposal as soon as possible so that the WDG will be in compliance with Provincial regulations.

JR Cousin Consultants Ltd. requests that a draft copy of the Environment Act Licence be forwarded for review prior to the issue of the final licence.



APPENDIX

Appendix A

Letter from Crown Lands and Property Agency September 17, 2015

Crown Lands Permit

Schedule A1 Sketch of WDG Property from file at Lands Branch

Waste Disposal Ground Operating Permit #42877

Crown Lands & Property Agency - Lands Branch, March 9, 2011 Email Correspondence

Table 1: Population and Waste Generation Projections – City of Thompson Waste Disposal Ground

Appendix B

LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report, AECOM 2008

LGD of Mystery Lake Waste Geotechnical and Topographic Investigation for the Waste Disposal Ground, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Scope Change #2 – Additional Test Holes, JR Cousin Consultants Ltd., 2012

Phase I Construction Works - Hydraulic Conductivity Test Results, NTL, September 14, 2012

Phase II Construction Works - Hydraulic Conductivity Test Results, NTL, October 29, 2013

Phase III Construction Works - Hydraulic Conductivity Test Results, Stantec, October 23, 2014

Appendix C

Plan 1: Site Layout with Approximate Location of Property Line

Plan 2: Final Cover Grading Contours and Final Drainage Plan

Phase I Works – Record Drawing Plan Set

Phase II Works - Record Drawing Plan Set

Phase III Works – Record Drawing Plan Set

Phase IV Works - Design Drawing Plan Set

Appendix A

Letter from Crown Lands and Property Agency September 17, 2015

Crown Lands Permit

Schedule A1 Sketch of WDG Property from file at Lands Branch

Waste Disposal Ground Operating Permit #42877

Crown Lands & Property Agency - Lands Branch, March 9, 2011 Email Correspondence

Table 1: Population and Waste Generation Projections – City of Thompson Waste Disposal Ground

Letter from Crown Lands and Property Agency September 17, 2015



308-25 Tupper Street North Portage la Prairie, MB R1N 3K1 P. (204) 239-3510 F. (204) 239-3560 Toll Free 1-866-210-9589

Writer's direct line – (204) 239-3810 Email: kelsey.little@gov.mb.ca

September 17, 2015

The City of Thompson Attention: Gary Ceppetelli 226 Mystery Lake Road Thompson MB R8N 1S6

Dear Mr. Ceppetelli:

Re: Site in Part NW 1/4 18, S 1/2 & NW 1/4 19 in TWP 77-3 WPM and in Part SE 1/4 24-77-4 WPM

Assignment of Crown Land Permit No. 50804

Specific Use: Waste Disposal Site

The application to assign Crown Land Permit No. GP 50804 from LGD of Mystery Lake to the City of Thompson has been approved and registered in the office of Crown Lands and Property Agency, Portage la Prairie, on the <u>30th</u> day of <u>July</u>, <u>2015</u> as No. <u>4612</u>-Electronic.

Enclosed is your copy of the registered assignment for your records and a copy of Crown Land Permit No. GP 50804.

In addition to payment of the rent, you may be responsible for the payment of taxes to the LGD of Mystery Lake.

Tax issues are to be dealt with directly with the taxing authority. Both taxes and rent must be kept current to constitute a valid permit. Failure to do so may result in cancellation of the permit. As well, it is imperative that all conditions of the Crown Land Permit are adhered to.

If you have any questions or require further information please contact me at the above noted number.

Yours truly,

Kelsey Little

Land Administrator

General Leases & Permits

KAL/kal

cc: Dave Hastman, Regional Land Manager (copy of signed Schedule A)

Lori Stevenson, Manitoba Conservation and Water Stewardship

Tannis Bohn, Department of Local Government - Assessment Branch

Rico Penamante, Department of Local Government - Assessment Branch

LGD of Mystery Lake

P.O. Box 189

Thompson MB R8N 1N1



Manitoba

Conservation

Lands Branch



Box 20000, 123 Main Street W Neepawa Mb. R0J 1H0 CANADA Tel: (204)-476-7060 Fax: (204)-476-7539

February 22, 2005

Local Government District of Mystery Lake Attention: Louise Hodder Box 730 Thompson, Mb. R8N 1N5

Dear Madam:

Re: Site in Part NW1/4 18, S1/2 & NW1/4 19 in Twp 77-3 WPM and in Part SE1/4 24-77-4 WPM as

shown on a sketch on file at Lands Branch.

waste disposal site

Crown Land Permit No. GP 50804

I am pleased to advise that your Crown Land Permit application for the above noted land has been conditionally approved under the terms and conditions outlined in the enclosed Schedule A.

Please review Schedule A. If the terms and conditions are acceptable to you, please sign and date both copies where indicated and have your Witness sign and date both copies where indicated.

Return one copy of the signed Schedule A to this office.

If we have not received a signed copy of Schedule A by April 22, 2005, we will assume that you are no longer interested in this property and your application will be cancelled. Any new application received after that date will be dealt with in accordance with the policies and regulations in effect at that time.

Your permit will be issued upon receipt of the signed copy of Schedule A.

If you have any questions concerning Permit No. GP 50804, please contact Larry Krakowka, Land Administrator at (204) 476-7515.

Yours truly,

Harley Johasson

Director

/km

Copy: Brian Barton, Regional Land Manager

PROVINCE OF MANITOBA MANITOBA CONSERVATION

SCHEDULE "A" TO CROWN LAND PERMIT NO. GP 50804 ("the Permit")

ISSUED BY:

HER MAJESTY THE QUEEN IN RIGHT OF THE PROVINCE OF MANITOBA represented herein by the Honourable Minister of Conservation

("Manitoba")

ISSUED TO:

Local Government District of Mystery Lake

(the "Permittee")

pursuant to The Crown Lands Act as amended from time to time.

WHEREAS:

- A) The Permittee has made an application to Manitoba for a Crown Land Permit for the Land (as described further in this Schedule);
- B) The Permittee is eligible for a Crown Land Permit for the Land and the Land has been determined by Manitoba to be suitable for the use and purpose as described in this Schedule; and
- C) Manitoba agrees to issue a Crown Land Permit to the Permittee, subject to the terms and conditions set out in this Schedule, which is Schedule "A" to the Permit, and the Standard Conditions attached to the Permit, for the land described as follows and as substantially similar to that set out on the map attached as Schedule A1:

Site in Part NW½ 18, S½ & NW½ 19 in Twp 77-3 WPM and in Part SE½ 24-77-4 WPM as shown on a sketch on file at Lands Branch.

Area: 136.38 acres (1,800 ft. x 3,300 ft.)

(the "Land")

THE PERMIT IS SUBJECT TO THE FOLLOWING TERMS AND CONDITIONS:

1.00 TERM AND RIGHT TO USE AND OCCUPY THE LAND

- 1.01 The Permit shall be effective from the date it is issued by Manitoba until December 31, 2005, subject to termination or extension under section 7.
- 1.02 Subject to the terms and conditions of the Permit, Manitoba grants to the Permittee the right to use and occupy the Land.

2.00 PAYMENT OF FEES AND TAXES

- 2.01 The Permittee shall pay to Manitoba rent equal to the annual fee prescribed from time to time by the Regulations under *The Crown Lands Act*, in accordance with such Regulations and the Permit, within 30 days of receipt of an invoice from Manitoba. The Permittee acknowledges that the current annual fee is \$0.00, as per Item No. 4 of an Agreement dated December 16, 1966 and signed by Manitoba, the International Nickel Company of Canada Limited, the Local Governmet District of Mystery Lake, the School District of Mystery Lake No. 2355, the Town of Thompson and the Resident Administrator of the Local Government District of Mystery Lake.
- 2.02 The Permittee acknowledges that an application for renewal and administration fee in relation to the Permit shall be paid by the Permittee, as prescribed by the Land Administration Fees Regulation (M.R. 216/89) and as amended from time to time.
- 2.03 Payments of the annual fee and the administration fees shall be made in accordance with the directions contained in the invoice from Manitoba.
- 2.04 Manitoba may establish a new annual fee rate where there is a change in one or more of the following factors in order to reflect these changes:
 - a) the appraised value of the Land as determined by Manitoba;
 - b) the appraised value of the buildings and improvements owned by Manitoba;
 - the policy of Manitoba as set out in an Act of the Legislature or a Regulation relating to the determination of annual fee; or
 - d) the use of the buildings, infrastructure or Land.

- 2.05 Manitoba shall give notice to the Permittee 30 days prior to the effective date of an increase the annual fee.
- 2.06 The Permittee shall pay all taxes, rates, duties and assessments whatsoever, whether municipal or otherwise, now or hereafter charged on the Land or in respect of the Permittee's use and occupation thereof.
- 2.07 The Permittee shall pay interest to Manitoba on any arrears of annual fee or administration fees at rate equal to the rate fixed from time to time by the Minister of Finance of Manitoba under section 25(1) of *The Financial Administration Act.* Failing such rate being fixed, interest shall be payable thereon at a rate equal to the rate fixed from time to time by Manitoba.
- 2.08 The Permittee shall pay to Manitoba an amount equal to any and all goods and services taxes now or hereafter imposed on, or collectible by Manitoba with respect to any amounts payable by the Permittee to Manitoba hereunder, whether characterized as a goods and services tax, sales tax, value added tax or otherwise ("Sales Taxes"). The intention of the parties is that Manitoba shall be fully reimbursed by the Permittee with respect to any and all Sales Taxes payable or collectible by Manitoba now or in the future.
- 2.09 The Permittee is responsible for and shall pay any and all costs, charges, impositions and expenses related to the Land, including, without limitation, all water, sewer, gas, telephone, or electric power charges.
- 2.10 If the Permittee fails to pay any and all taxes or water, sewer, gas, telephone, or electric power charges as required, Manitoba may pay them or any of them and charge those payments to the Permittee who shall reimburse Manitoba forthwith and Manitoba may take the same steps for the recovery of those payments as it would be for the recovery of rent arrears.
- 2.11 The Permittee shall pay all amounts payable to Manitoba hereunder without any deduction or setoff whatsoever.

3.00 USE OF THE LAND

- 3.01 The Permittee shall use the Land for a waste disposal site and for no other purpose, including non-use, without prior permission in writing from Manitoba.
- 3.02 The Permittee agrees that the following structures and improvements on the Land are authorized under the Permit: 1 office building (35 ft. x 20 ft.).
- 3.03 Other than those developments and uses permitted under paragraphs 3.01 and 3.02 of this Schedule, the Permittee shall not construct, erect or alter any other buildings or structures on the Land or effect any change in use of the Land without prior permission in writing from Manitoba.
- 3.04 The Permittee agrees to notify Manitoba of any building destroyed, demolished, or removed from the Land within 30 days of that occurrence; and to rebuild, replace or reinstate the building within 24 months of that occurrence.
- 3.05 It is the responsibility of the Permittee to place and maintain all buildings within the boundaries of the Land, and to obtain any Surveyor's Certificates necessary to effect or verify this condition.
- 3.06 Manitoba has no obligation to survey or resurvey the Land, and the Permit shall create no such obligation on Manitoba to survey or resurvey the Land.
- 3.07 The Permittee agrees that removal or relocation of any existing Manitoba Hydro facilities shall be at his/her expense.
- 3.08 The Permittee and its officers, directors, agents, invitees and employees, as applicable, shall be bound by the rules, regulations and guidelines made by Manitoba from time to time. All such rules, regulations and guidelines will be deemed to be incorporated into and form part of the Permit. Some form of advance public notice shall be provided for changes in these rules, regulations and guidelines.
- The Permittee shall comply with all federal, provincial and municipal laws and regulations, and obtain all licences and permits necessary for the lawful use of the Land, which, without restricting the generality of the foregoing, includes obtaining a work permit from the local District Resource Officer before cutting any trees or commencing any work on the Land, obtaining a building permit from the Department of Labour before constructing any structures, as may be authorized by Manitoba, in accordance with the Manitoba Building Code and applicable Municipal By-laws and regulations. The Permittee shall provide Manitoba with a copy of work permits or building permits obtained at the request of Manitoba.

- 3.10 The Permittee understands and agrees that the Issuance of this Permit in no way implied either Manitoba or the local government authority shall provide any services.
- 3.11 The Land is contained in the "Burntwood River Water Power Reserve" and this Permit is issued subject to The Water Power Act and Regulations thereunder.
- 3.12 The Permittee acknowledges that the Land is affected by Mineral Lease Nos. M4795, M4796, M4798, M4801, M4802, M4804 and M4805 and the leases are in good standing under *The Mines and Minerals Act*. These leases are held in the name of Inco Ltd, and this company retains the right to travel across the Land and to mine thereunder.
- 3.13 The Permittee acknowledges that the operation of the waste disposal site on the Land is governed by Operating Permit #N-02. Any expansion of the Land would require an Environment Act Licence which would require the filing of a proposal for a Class 2 development.
- 3.14 The Permittee acknowledges that a Manitoba Telephone System fibre optic cable is situated within the Hydro Right-of-Way paralleling Provincial Trunk Highway #6 or immediately adjacent to that Hydro facility. The Permittee understands and agrees to contact the Manitoba Telephone System before any excavation occurs near this area.

4.00 MAINTENANCE OF LAND

- 4.01 The Permittee agrees:
 - to keep the Land, and all buildings and structures thereon, in a clean and sanitary condition free from inflammable materials, other than those contained in containers approved by the Canadian Standards Association;
 - b) to comply with all federal, provincial and municipal by-laws, Acts and regulations relating to the Permittee and/or the Land including, but not limited to, The Crown Lands Act and Regulations, The Dangerous Goods Handling and Transportation Act and Regulations and The Environment Act and Regulations, all as amended, replaced or substituted from time to time;
 - not to commit waste or damage the Land;
 - d) to keep the Land, and all buildings and structures thereon, in good and safe repair; and in a proper and neat condition and to repair in accordance with any notice from Manitoba;
 - e) to allow a person or persons on behalf of Manitoba to enter the Land, including all buildings and structures, at all reasonable times to examine the state of repair;
 - f) not to cut or remove any trees without prior written consent of Manitoba
 - g) any shoreline development to be minimal on Crown land adjacent to lakes or rivers and limited only to facilities or uses approved in writing by Manitoba. Natural vegetation and features should have minimal disturbance, and a vegetative riparian zone should be maintained or encouraged.
- 4.02 The Permittee shall not release upon the Land or any part thereof any Pollutants (as defined in paragraph 4.05), but if Permittee does release any Pollutants, the Permittee shall
 - a) at his/her expense, immediately give Manitoba notice of the release; remove the Pollutants from the Land in a manner which conforms with all laws and regulations covering the handling, removal and management of the Pollutants and as may be directed or ordered by an Environment Officer or Director of the Environmental Approvals Branch, or such successor as appropriate, as soon as reasonably practicable; and
 - b) obtain from an independent Qualified Environmental Consultant, a report verifying the complete and proper removal thereof from the Land, if requested by Manitoba, otherwise the Permittee shall report as to the extent and nature of any failure to comply with this Section.
- 4.03 Any Pollutants noted in paragraph 4.02 shall not become the property of Manitoba notwithstanding any rule of the law to the contrary (save and except where such Pollutants are brought or created upon the Land by Manitoba or its servants, employees or agents, and provided such person is not the Permittee or an officer, director, agent or employee of the Permittee). At the option of Manitoba, any substance contaminated by such Pollutants shall become the property of the Permittee and at the Permittee's expense, the Permittee or, at Manitoba's option, Manitoba, shall remove the contaminated substance from the Land and make good any damage
- 4.04 The Permittee shall indemnify and save harmless Manitoba from all costs or expenses, liabilities, losses, claims, damages (including consequential damages, interest, penalties, fines or monetary sanctions), legal costs or fees on a solicitor and own client basis, and fees or expenses of professional consultants incurred by Manitoba by reason of Pollutants being present on the Land and resulting from the Permittee's use or occupation of the Land or the breach of any warranty or covenant of the Permittee in this Section.

- 4.05 In this Section, "Pollutants" means any product, solid, liquid, gas, smoke, odour, waste, radiation or organism, or any combination of these, that is foreign to or in excess of the natural constituents of the environment on the Land and that:
 - has affected, is affecting or may affect the natural, physical, chemical or biological quality
 the air, land and water; or
 - ls, or is likely to be, injurious or damaging to the health or safety of a person(s), or injurious or damaging to property or to plant or animal life.

5.00 NO ASSIGNMENT OF PERMIT WITHOUT CONSENT

- 5.01 The Permittee shall not assign the Permit without the prior written consent of Manitoba, that consent not be unreasonably withheld. If the Permittee is a corporation, any change in ownership or control of the Permittee is deemed to be a proposed assignment.
- 5.02 Manitoba shall not unreasonably withhold consent to the assignment of the Permit for collateral (financing and security) purposes.
- 5.03 The Permittee shall submit an application on a form specified by Manitoba for approval to assign the Permit or any interest in the Permit.
- 5.04 Notwithstanding paragraphs 5.01 or 5.02, Manitoba may, in its sole discretion, refuse to assign the Permit if:
 - a) the Permittee has not paid any and all outstanding rent and taxes in respect of the Land and improvements, or
 - b) the proposed assignee is not eligible to hold a Permit in accordance with then current laws, regulations and policies of Manitoba.
- 5.05 The Permittee shall not sublet or rent out the Land.
- 5.06 The Permit shall be binding upon the executors, administrators, heirs, successors and any permitted assigns of the Permittee.

6.00 RESPONSIBILITY AND INSURANCE

- 6.01 Nothing contained in the Permit shall create any liability on the part of Manitoba or Manitoba Hydro for any damages caused or purported to be caused in respect to the Land by raising or lowering waters bordering upon or adjacent to the Land.
- 6.02 The Permittee shall use due care in the occupation of the Land to ensure that no person is injured, no property is damaged or lost and no rights are infringed.
- 6.03 The Permittee shall be solely responsible for and indemnify and save harmless Manitoba, its officers, employees and agents from and against all claims, liabilities and demands with respect to:
 - a) any injury to persons (including death), damage or loss to property caused by, or related to the occupation of the Land or the performance of the Permit or the breach of any term or condition of the Permit by the Permittee, any agent, invitee, officer, director or employee of the Permittee or any other person authorized by the Permittee to occupy the Land, and
 - any omission or wrongful or negligent act of the Permittee, any agent, invitee, officer, director or employee of the Permittee or of any other person authorized by the Permittee to occupy the Land;

unless such claims, liabilities, and demands arise out of the acts or omissions of Manitoba, its officers, employees or agents, and provided such person is not the Permittee or an officer, director, agent or employee of the Permittee.

It is the responsibility of the Permittee to discuss his/her insurance requirements with his/her insurance adviser/broker and to arrange for his/her own insurance coverage(s). However, at a minimum, the Permittee shall purchase and maintain comprehensive general liability insurance with a minimum limit of \$1,000,000 per occurrence or claim. Manitoba reserves the right to require the Permittee to purchase and maintain a different minimum amount of liability insurance as specified by Manitoba from time to time by providing at least 180 days notice in writing of the change in the minimum amount to the Permittee. Evidence of insurance in the form of a Certificate of Insurance shall be provided by the Permittee upon request.

- 6.05 Notwithstanding paragraph 6.03, the Permittee agrees that any buildings, including any buildings existing at the issuance of the Permit, on the Land shall be maintained entirely at the Permittee's own risk, and the Permittee agrees to assume full responsibility for any damage injury to persons or property situated on the Land resulting from flooding, erosion, ice damage, or temporary or permanent loss of Land accessibility. The Permittee agrees not to institute any action or make any claim against Manitoba or any employee or agent of Manitoba, including Manitoba Hydro, in respect to any personal injury caused by or related to flooding, whether or not the damage was occasioned by flooding resulting from the regulation or control of the adjacent waterway by Manitoba or Manitoba Hydro.
- 6.06 Notwithstanding paragraph 6.03, the Permittee agrees to indemnify and save harmless Manitoba and all employees and agents of Manitoba, including Manitoba Hydro, from and against all claims, liabilities and demands in respect of any damage to property or injury to persons located on the Land, which has been caused by flooding, erosion, ice damage, or temporary or permanent loss to Land accessibility.
- 6.07 The Permittee agrees not to institute any action or make any claim against the local government authority with respect to damage to any building or personal property or any injury to persons located on the Land that may be caused by flooding, erosion, ice damage, or temporary or permanent loss of land accessibility, as described herein and the Permittee agrees to enter into a written Agreement with the local government authority if the local government authority deems it necessary.

7.00 TERMINATION AND EXTENSION

- 7.01 The Permittee acknowledges that the Permit does not operate to prevent the sale or lease of the Land at any time during its term and is subject to the condition that Manitoba may give the Permittee notice of the cancellation thereof; and at the expiration of 30 days from the service of the notice, the Permit shall be cancelled.
- 7.02 Subject to 7.01 and provided that there has been no uncured default by the Permittee, including payment of rent, Manitoba may, in its discretion automatically renew the Permit for a 1 year term on an annual basis and in accordance with then current laws, regulations or policies respecting rental rates and rental property of this type, unless otherwise notified by the Permittee.
- 7.03 Without restricting any other remedies available, Manitoba may, at its sole option, immediately terminate the Permit in writing if:
 - a) the Permittee has failed to make any payment due hereunder, has misrepresented any fact on the application for the Crown Land Permit, or has failed to comply with anyterm or condition of the Permit and has not remedied that failure to comply within 30 days of receipt of notice in writing from Manitoba;
 - b) the Permittee makes an assignment for the benefit of creditors, becomes bankrupt or insolvent, takes the benefit of, or becomes subject to, any statutes that may be in force relating to bankrupt or insolvent debtors (the appointment of a receiver or receiver and manager of the assets of the Permittee being conclusive evidence of insolvency), or if any certificate or order is made or granted for the winding-up or dissolution of the Permittee, voluntarily or otherwise;
 - c) the Permittee suffers a lien under The Bullders' Lien Act (Manitoba) or any similar or successor legislation registered against the Land or Manitoba's interest therein and does not contest the validity or the amount of the lien and do all things necessary to obtain and register a discharge forthwith after the lien has come to the notice of the Permittee.
- 7.04 Where the Permittee terminates the Permit under paragraph 7.02 or Manitoba terminates the Permit in accordance with paragraph 7.01 or 7.03, or upon the expiration of the term or any renewal term of the Permit:
 - a) the Permittee shall deliver up possession of the Land to Manitoba and shall not remain in possession of the Land following the date of expiration or termination of the Permit; and
 b) at the option of Manitoba:
 - (i) the Permittee and Manitoba may agree on the fair market value of the buildings or structures added to the Land by the Permittee and Manitoba may purchase such buildings or structures by paying to the Permittee that fair market value. If they fail to reach an agreement regarding the fair market value within 180 days of notice of termination being given by Manitoba, such value shall be determined by reference to the Land Value Appraisal Commission, or such other body as may hereafter be substituted therefor from time to time, or

- (ii) the Permittee shall remove all buildings and structures added to the Land by he Permittee within six months of such expiry or termination, or such other term as agreed Manitoba, and where those buildings and structures are not removed within six months or term agreed to by Manitoba, they shall become the property of Manitoba. At the end of such six months or term agreed to by Manitoba, any assets left on the property as at such date shall vest in Manitoba, and the Permittee shall be deemed to have released and quit-claimed any interest therein to and in favour of Manitoba. No compensation or payment whatsoever shall be payable therefor by Manitoba to the Permittee in such event.
- 7.05 Where Manitoba terminates the Permit in accordance with paragraph 7.01 in instances where the Permittee is entering into a purchase or lease Agreement in respect of the Landwith Manitoba, all buildings and structures added to the Land by the Permittee shall be dealt with in accordance with the terms of that Agreement.
- 7.06 Where Manitoba terminates the Permit in accordance with paragraph 7.01 and 7.03 in instances where collateral assignments are recorded, it shall provide notice in writing of such termination to the holder of such collateral assignments (the "Security Holder"). The Security Holder:
 - a) shall then be allowed a reasonable time frame of not less than 30 days as stipulated in the notice, to cure defaults of the Permittee, and upon doing so the Permit shall be deemed not to have terminated;
 - b) shall not be obligated to go into possession; and
 - c) shall be allowed to assign the Permittee's interest in the Permit to a third party purchaser, subject to the prior written consent of Manitoba being required, but which shall not be unreasonably withheld; provided that as a condition of any such assignment, such subsequent assignee shall execute such documentation as Manitoba considers reasonable to bind the assignee directly to Manitoba on the terms and conditions as contained in the Permit, and all defaults of the Permittee shall be cured and brought to good standing. In the event of such permitted assignment, the Permit shall be deemed not to have terminated.

8.00 ENTIRE PERMIT

- 8.01 The Permit, including this Schedule and any Standard Conditions attached to the Permit, constitutes the entire Permit. There are no undertakings, representations, warranties, covenants, guarantees, agreements or promises, express or implied, verbal or otherwise, other than those contained in the Permit.
- 8.02 No amendment or change to, or modification of, the Permit shall be valid unless it is in writing.

9.00 APPLICABLE LAW

9.01 The Permit shall be governed by, interpreted, performed and enforced in accordance with the laws of Manitoba.

10.00 NOTICES

- 10.01 Any notice or other communication to Manitoba under the Permit shall be in writing and shall be delivered or sent by mail, postage prepaid to: Manitoba Conservation, Lands Branch, Attention: Director, Box 20,000, 123 Main Street West, Neepawa, Mb., R0J 1H0.
- 10.02 Any notice or other communication to the Permittee under the Permit shall be in writing and shall be delivered personally to the Permittee or an officer, director or employee of the Permittee or sent by mail, postage prepaid, to: Box 730, Thompson, Mb., R8N 1N5.
- 10.03 Any notice or communication sent by mail shall be deemed to have been received on the third business day following the date of mailing. If mail service is disrupted by labour controversy, notice shall be delivered personally.
- 10.04 Either party may provide notice of change of address to the other in writing and thereafter all notices or communications shall be provided to the new address.
- 10.05 Any notice or other communication signed by any employee, officer or minister of Manitoba acting in that capacity shall be deemed for the purposes of the Permit to be a notice or other communication executed by Manitoba.
- 10.06 Notwithstanding paragraphs 10.02 and 10.03 any written notice to be served or given by Manitoba to the Permittee under the Permit shall be effectively given or served by posting the same in a conspicuous place on the Land.

11.00 ADDITIONAL PROVISIONS

11.01 Time shall be of the essence of the Permit.

- 11.02 If any provision of the Permit is illegal or invalid or unenforceable at law it shall be deemed to be severed from the Permit and the remaining provisions shall nevertheless continue to be in full force and effect.
- 11.03 No waiver of any default under the Permit shall be binding unless acknowledged in writing by Manitoba. Any condoning, excusing or overlooking by Manitoba of any default shall not operate as a waiver of Manitoba's rights hereunder in respect of any subsequent default.
- 11.04 All headings in this Schedule are inserted for convenience of reference only and will not affect the construction and interpretation of the Permit.
- 11.05 If this Permit is Issued to two or more persons as Permittee, the liability of each to pay rent and taxes and to perform all other obligations hereunder shall be joint and several. If the Permittee is a corporation, each person acknowledging the terms of the Permit on behalf of the Permittee by so signing hereby agrees to guarantee to Manitoba the performance by the Permittee of all obligations of the Permittee hereunder, and each such person shall be jointly and severally liable with the Permittee as Permittee hereunder.
- 11.06 If the Permittee remains in possession of the Land after the termination of the Permit and Manitoba accepts rent, the tenancy, in the absence of written Agreement, will be from month to month only and shall be subject to all terms of the Permit, including rent, except that the tenancy shall be from month to month.
- 11.07 The Permittee shall not be entitled to file a caveat against title to the Land respecting the Permit under *The Real Property Act* (Manitoba) as it may be amended, replaced or substituted from time to time.
- 11.08 Sections 4 and 6 shall survive the termination or expiration of the Permit

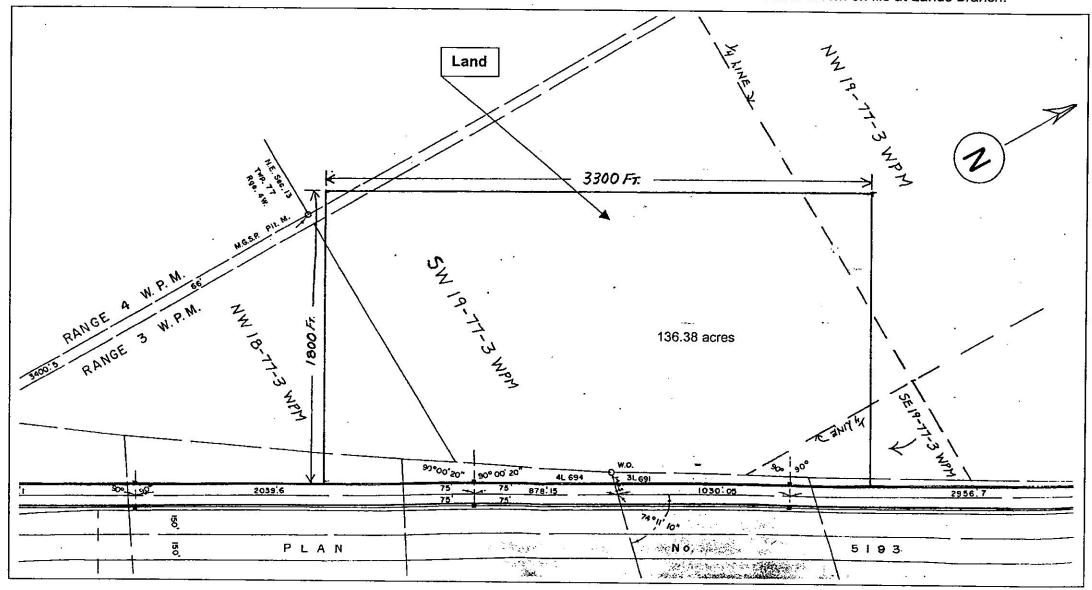
THE PERMITTEE or the Permittee's duly authorized representative, on the dates noted below, acknowledges that he/she has read and understands all the terms and conditions of the Permit and agrees to be bound by same.

WITNESS SIGNED IN THE PRESENCE OF	PERMITTEE Local Government District of Mystery Lake				
Print Name of Witness					
Frint Name of Witness	Name of Permittee				
Signature of Witness					
Signature of withess	Signature of Permittee				
DATE:	DATE:				



SCHEDULE A1

Site in Part NW¼ 18, S½ & NW¼ 19 in Twp 77-3 WPM and in Part SE½ 24-77-4 WPM as shown on a sketch on file at Lands Branch.







Conservation and Water Stewardship

Environmental Stewardship Division Environmental Approvals Branch 123 Main Street, Suite 160, Winnipeg, Manitoba R3C 1A5 T 204 945-8321 F 204 945-5229 www.gov.mb.ca/conservation/eal

September 22, 2015

Mr. Gary Ceppetelli City Manager City of Thompson 226 Mystery Lake Road Thompson, MB R8N 1S6

Dear Mr. Ceppetelli:

Re: Thompson Waste Disposal Grounds, Permit 42877

Enclosed please find the permit for your waste disposal ground.

Please note that failure to comply with any condition of the permit may result in prosecution pursuant to the Waste Disposal Grounds Regulation.

Pursuant to Section 27 of *The Environment Act*, this permit may be appealed to the Minister of Conservation and Water Stewardship by any person who is affected by the issuance of this permit within 30 days of the date of issue.

In addition to the enclosed Permit requirements, please be informed that all other applicable federal, provincial and municipal regulations and by-laws must be complied with.

If you have any questions concerning the permit or procedures, please call Jeff Fountain in Thompson at (204) 677-6703 or via electronic mail at <u>jeff.fountain@gov.mb.ea</u>.

Yours sincerely,

Tracey Braun, M.Sc.

Lang Dames

Director

Environmental Approvals Branch

c: D. Labossiere/T.Prawdzik/D.Smiley, Environmental Compliance and Enforcement Branch

NOTE: Confirmation of Receipt of this Permit No. 42877 (by the Permitee only) is required by the Director of Environmental Approvals. Please acknowledge receipt by signing in the space provided below and faxing a copy (letter only) to the Department by October 5, 2015.

Waste Disposal Ground Operating Permit



Permit No: 42877 Client File: 11587

In accordance with the Waste Disposal Grounds Regulation, made under The Environment Act, the City of Thompson is hereby permitted to operate a Waste Disposal Ground, to be known as the Thompson Waste Disposal Ground situated at Pt NW ¼ 18, S ½ & NW ¼ 19 Twp 77-3 WPM and Pt SE ½ 24-77-4 WPM in the Province of Manitoba.

THIS OPERATING PERMIT is subject to being AMENDED, SUSPENDED or REVOKED under section 6 of the *Waste Disposal Grounds Regulation*.

THIS OPERATING PERMIT is issued subject to the following TERMS AND CONDITIONS:

General Terms and Operating Conditions

- 1. This permit expires on June 1, 2016.
- 2. The Operator shall, prior to **June 1, 2016** submit to the Director an Environmental Act Licence proposal for continued operation of a Class 1 Waste Disposal Ground.
- 3. The Operator shall construct, maintain and operate the **Thompson Waste Disposal Ground** (the Facility) in accordance with the most current version of the *Waste Disposal Grounds Regulation*, (M.R. 150/91), the engineering submission prepared by J.R. Cousin
 Consultants Ltd dated June 30, 2011 inclusive of supporting documentation from AECOM
 (2009 Master Plan) dated January 2010 and AECOM Environmental Assessment Report
 dated February 2010 hereafter referred to as The Plan, and this Operating Permit.
- 4. In accordance with section 8 of the Waste Disposal Grounds Regulation, this permit is issued to the Facility with a variance to the distance from a body of surface water requirements. Based upon the proximity of the surface water body to the waste disposal ground, the Operator shall sample the surface water body for the baseline parameters stipulated in Appendix B once annually starting in Summer 2015.
- 5. The Operator shall operate the Facility as per the operation and maintenance parameters included in The Plan.
- 6. The Operator shall provide site supervision when the Facility is open to the public.
- 7. The Operator shall restrict access to the Facility with a locked gate or barrier when site supervision is not provided.

Materials Acceptance and Handling

8. The Operator shall maintain a sign at the entrance of the Facility indicating the type of waste accepted, days and hours of operation, and the location for disposal of wastes not accepted on site.

- Recyclable materials such as, but not limited to, bulky metallic waste, E-Waste, and rubber tires must be segregated in an area of the Facility other than the waste disposal cells (active area) and those areas must be appropriately signed.
- 10. The Operator shall remove any litter accumulated along the access road and around the perimeter of the site at minimum twice annually or as required by an Environment Officer.
- 11. The Operator shall only accept asbestos that is packaged in accordance with the current edition of Guidelines for an Asbestos Operations and Maintenance Program from Workplace Safety and Health Division. All asbestos shall be covered immediately with a minimum of 1 metre of material and the location for disposal shall be documented and recorded in the Facility operation and maintenance plan, accessible to all operators.

Liquids and Dangerous Goods

- 12. The disposal of liquid wastes or liquid industrial wastes shall not be allowed at the Facility.
- 13. The Operator shall collect and dispose of hazardous waste in accordance with *The Dangerous Goods Handling and Transportation Act*, and other Provincial and Federal Regulations.

Placement and Cover

- 14. Any animal mortality disposed of at the Facility must be covered within 24 hours of deposit with a minimum one (1) metre of soil, or within such time as is approved by an environment officer.
- 15. Cover of waste shall occur in accordance with M.R. 150/91 or as required by an environment officer. The use of cover materials other than those specified in M.R. 150/91 may be permitted with written approval of the Director.
- 16. The Operator shall implement control measures to prevent attraction and sustenance of rodents and scavenging vectors.

Surface Water Management

17. The Operator shall grade and maintain the site so that all uncontaminated surface water flows to the perimeter ditch or away from the Facility and impacted water from all material storage and disposal areas shall be directed to a leachate evaporation pond or contained within the site.

Site Construction and Upgrading

- 18. The Operator shall have all new waste disposal cells designed by and construction overseen by a Professional Engineer in accordance with Condition 19 of this Operating Permit.
- 19. Individual waste disposal cell (active cell) construction shall be subject to the following conditions:

- a) the Operator must notify the assigned Environment Officer within five (5) days of commencement of construction of all waste cells and within five (5) days of installing any additional groundwater monitoring wells;
- b) the Operator must provide for testing of all clay liners by a qualified consultant to confirm compaction is 95% Standard Proctor Density on maximum lifts of 150 mm;
- c) all active areas or leachate containment developed from or with clay must be constructed to achieve a hydraulic conductivity of not more than 1x10⁻⁷ cm/s with a minimum thickness of 1 metre perpendicular to the surface. If appropriate or sufficient clay is not available an alternative proposal must be submitted to the Director for written approval prior to construction; and
- d) the active area (cell) shall be constructed to retain any flyaway loose garbage or the Operator shall install a 1.8 metre fence constructed in such a manner as to contain the solid waste around the active area upon the request of an Environment Officer.
- 20. The Operator shall arrange with the designated Environment Officer a mutually acceptable time and date for any required soil sampling between the 15th day of May and the 15th day of October of any year, unless otherwise approved by the Environment Officer.
- 21. The Operator shall, within 90 days of the completion of the construction of any component of the waste disposal ground, submit "record drawings" along with a construction report to the Director.

Composting

22. Prior to establishing any composting area, the Operator shall provide a detailed operation and maintenance manual focused on the compost area including, but not limited to: the design and construction of the composting, curing and storage areas, the proposed volume and type of material for compost, the type of bulking materials used, the proposed frequency and method of turning, methods of vector and odour control, and the end use of the compost. For fish carcass composting areas this manual must be provided to the Director, and a written acceptance of the proposed operations must be received prior to the construction of the composting site.

Closure of Active Cells

23. The closure of each cell shall be performed as indicated in The Plan.

Environmental Emergency Reporting

24. The Operator shall, in the event of a fire which continues in excess of thirty (30) minutes, report the fire to the Environmental Emergency Response line by calling 1-855-944-4888 and identify the type of material involved and the location of the fire, excluding any fire in accordance with Condition 25.

Burning of Combustible Waste

25. All burning shall be carried out in accordance with the attached Appendix A: Terms and Conditions for Burning at Waste Disposal Grounds.

Monitoring and Reporting Requirements

- 26. Groundwater monitoring well samples shall be collected, stored and analyzed using approved field and laboratory techniques for dissolved analysis. The analytical results shall be retained in a format acceptable to Manitoba Conservation and Water Stewardship and must show previous results and analytical trends.
- 27. The Operator shall sample the groundwater monitoring wells once per year in late summer for those parameters identified in Appendix B or selected parameters and frequency, as approved by the Director.
- 28. The Operator shall submit an annual report, in a format acceptable to the Director, detailing the results of groundwater and surface water sampling analyses, complete with previous results and trends. The report shall be submitted to the designated Environment Officer no later than December 31 annually.

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Tracey Braun, M.Sc.

Director, Environmental Approvals

APPENDIX A

TERMS and CONDITIONS for BURNING at WASTE DISPOSAL GROUNDS

Burning of certain waste materials is allowed at waste disposal grounds **only** if a condition in the permit specifically allows for the activity and all terms and conditions of this appendix have been satisfied. Timing of burning is conducted at the **operator's** discretion and subject to authorization under *The Wildfires Act*.

Siting Criteria

- A burn area is allowed only at a waste disposal ground which can meet the siting and design criteria below.
- 2. There shall be no dwellings or commercial establishments within 400 metres of the burn area.
- 3. The burn area shall be located a minimum of **50** metres from the active waste cell or any area utilized for the collection of flammable materials.

Design Criteria

- 4. The burning area shall be constructed of 2 or more separate cells or an enclosed metal burn containment vessel. These cells shall have containment on 3 sides and each side shall be not less than 1.8 metres in height.
- A chain link fence, not less than 1.5 metres in height and with mesh size no greater than 5.5 cm, shall be constructed on top of the berms to contain windblown scatter at the written request of the designated Environment Officer.
- 6. The base of the burn area shall be graded to prevent the collection of water inside the burn area. In areas where groundwater contamination is a concern the base of the burn area shall be constructed of 1 metre of compacted clay with hydraulic conductivity less than of 10⁻⁷ cm/s or equivalent upon the written approval of the Environment Officer.

Operating Criteria

- 7. Burning shall take place within the confines of a trench, in a berm-confined area or within a burn vessel and not on or above the prevailing grade.
- 8. Only separated and readily combustible materials such as boughs, leaves, loose straw, paper products, cardboard, non-salvageable untreated wood, and packing materials derived from wood may be burned, and only when there is an appropriate volume of this material to burn. Plywood, composite board or other materials constructed with glues, finishes or preservatives must not be burned.
- Burning of any other product or material is prohibited, including but not limited to plastics, composites, rubber, manures, chemically treated fabrics, mattresses, finished furniture, or manmade synthetics.
- Burning is to occur only when weather conditions are favourable, taking into consideration wind direction and velocity, so that nuisance to any neighbouring resident and / or highway does not occur.
- 11. Burning shall be under constant supervision.
- 12. Burning is restricted to daylight hours only.
- 13. If burning is started as a result of vandalism or natural cause, the fire is to be extinguished as quickly as possible by the most appropriate means; and the regional Environment Officer must be notified of the occurrence and actions taken.
- 14. Ashes, when completely extinguished, shall be removed from the burn area regularly and deposited at the active cell.
- **15.** The site supervisor shall keep a record of all controlled burns indicating the date of each burn; volume of waste burned and types of wastes burned on each occasion. Upon request by the Director or an Environment Officer, the records must be provided.

Appendix B Ground Water Chemistry Parameters

	Chemistry Farameters				
Chemical Parameters					
In	organics				
Alkalinity – Total	Magnesium – Dissolved				
Ammonia – Total	Manganese - Dissolved				
Arsenic – Total	Mercury - Dissolved				
Barium - Dissolved	Nitrate - Reported as N				
Boron Dissolved	Nitrite - Reported as N				
Cadmium - Dissolved	Total Kjeldahl Nitrogen – Reported as N				
Calcium – Dissolved	рН				
Calcium Carbonate	Total Phosphorous				
Chloride	Potassium – Dissolved				
Chromium - Dissolved	Silicon – Dissolved				
Conductivity	Sodium - Dissolved				
Copper - Dissolved	Total Dissolved Solids (TDS)				
Iron - Dissolved	Sulphate				
Lead - Dissolved	Uranium – Dissolved				
	Zinc – Dissolved				
Volatile Organic	Compounds (VOC's)				
BTEX					
Othe	er Organics				
Biological Oxygen Demand (BOD)	Chemical Oxygen Demand (COD)				
Dissolved Organic Carbon (DOC)					
Field	Parameters				
pH	Groundwater Elevation				
Conductivity	Dissolved Oxygen				
Temperature					
	-1				

Note: All metals (except Arsenic) are to be sampled for dissolved analysis.

Dissolved samples should be filtered in the field and preserved in the field at time of sampling. If dissolved samples are not to be filtered and preserved in the field then Conservation and Water Stewardship and the Laboratory must be notified prior to sampling.

Crown Lands & Property Agency - Lands Branch, March 9, 2011 Email Correspondence

From: "Little, Karen (CLP)" < Karen.Little@gov.mb.ca>
Subject: RE: LGD of Mystery Lake WDF - Mineral Rights

Sent date: 03/09/2011 09:21:07 AM

To: "Brett McCormac" < bmccormac@jrcc.ca>

Cc: "Armitt, Ernest (IEM)" < Ernest.Armitt@gov.mb.ca>

Good Morning Brett, according to our records this date, Her Majesty the Queen in Right of the Province of Manitoba owns the Mines & Minerals and Sand & Gravel in NW 18, S 1/2 & NW 19 in 77-3 WPM and in SE 24-77-4 WPM.

You may want to contact Mr. Ernie Armitt of Mines Branch to determine if any mineral dispositions are affected.

Karen Little
Supervisor of Crown Lands Registry
Crown Lands and Property Agency
308 - 25 Tupper Street North
Portage la Prairie MB R1N 3K1
P (204) 239-3805 F (204) 239-3560
Toll Free 1-866-210-9589
karen.little@gov.mb.ca
An Agency of MB Infrastructure and Transportation

----Original Message----

From: Brett McCormac [mailto:bmccormac@jrcc.ca]

Sent: Tuesday, March 08, 2011 9:53 AM

To: Little, Karen (CLP)

Subject: LGD of Mystery Lake WDF - Mineral Rights

Hello Karen,

J.R. Cousin Consultants Ltd. (JRCC) is preparing an Environmental Submission on behalf of the LGD of Mystery Lake, for a proposed solid waste disposal facility upgrade and expansion. The WDF site is located approximately 4 km south of the City of Thompson located on Part NW $\frac{1}{4}$ 18, S $\frac{1}{2}$ and NW $\frac{1}{4}$ 19 in TWP 77-3 WPM and in Part SE $\frac{1}{4}$ 24-77-4 WPM. The site can be seen in the attached plan.

The land is Crown Land leased to the LGD of Mystery Lake under Crown Land Permit No. GP 50804.

Would you please provide information regarding who owns the Mineral Rights underneath the WDF site?

Thank you,

Brett McCormac, E.I.T. Environmental Engineer-in-Training

J.R. Cousin Consultants Ltd. Phone: (204) 489-0474 Fax: (204) 489-0487 http://www.jrcc.ca

Table 1:	Population and Waste Generation Projections — City of Thompson Waste Disposal Ground

TABLE 1 POPULATION AND WASTE GENERATION PROJECTIONS City of Thompson Waste Disposal Ground

Column 1	Column 2	Column 3	Column 4	Column 5	Column 6	Column 7	Column 8	Column 9	Column 10	Column 11
CALENDAR YEAR	PROJECT YEAR	CITY OF THOMPSON	LGD OF MYSTERY LAKE	TOTAL WASTE FROM CITY OF THOMPSON AND LGD OF MYSTERY LAKE	TOTAL WASTE FROM WUSKWATIM, KEEYASK AND PAINT LAKE	TOTAL WASTE TO DISPOSAL SITE	ACTUAL WASTE TO DISPOSAL SITE from weigh scale	TOTAL WASTE TO DISPOSAL SITE	CAPACITY REMAINING AT END OF YEAR	CAPACITY REMAINING AT END OF YEAR
		(people)	(people)	2.0 kg/person/day	(tonnes / year)					
		0.52% annual growth	0.52% annual growth	(tonnes / year)	0.0% annual growth	(tonnes / year)	(tonnes / year)	(m³/year)	(tonnes)	(m³)
2010	0	13,188	10	9,634	614	10,248	12,008	25,280	344,604	725,482
2011	0	13,123	10	9,587	614	10,201	12,389	26,082	332,215	699,400
2012	0	13,191	10	9,637	614	10,251	10,525	22,158	321,690	677,242
2013	0	13,260	10	9,687	614	10,301	9,873	20,785	311,817	656,457
2014	0	13,329	10	9,737	614	10,351	9,800	20,632	302,017	635,825
2015	0	13,398	10	9,788	614	10,402	10,420	21,937	291,597	613,888
2016	0	13,468	10	9,839	614	10,453		22,006	281,144	591,882
2017	1	13,538	10	9,890	614	10,504		22,114	270,640	569,768
2018	2	13,608	10	9,942	614	10,556		22,222	260,084	547,546
2019	3	13,679	10	9,993	614	10,607		22,331	249,477	525,215
2020	4	13,750	10	10,045	614	10,659		22,440	238,818	502,774
2021	5	13,822	11	10,097	614	10,711		22,550	228,106	480,224
2022	6	13,893	11	10,150	614	10,764		22,661	217,342	457,563
2023	7	13,966	11	10,203	614	10,817		22,772	206,526	434,791
2024	8	14,038	11	10,256	614	10,870		22,884	195,656	411,907
2025	9	14,111	11	10,309	614	10,923		22,996	184,733	388,911
2026	10	14,185	11	10,363	614	10,977		23,109	173,756	365,802
2027	11	14,258	11	10,417	614	11,031		23,222	162,725	342,580
2028	12	14,333	11	10,471	614	11,085		23,336	151,641	319,244
2029	13	14,407	11	10,525	614	11,139		23,451	140,501	295,793
2030	14	14,482	11	10,580	614	11,194		23,566	129,308	272,226
2031	15	14,557	11	10,635	614	11,249		23,682	118,059	248,544
2032	16	14,633	11	10,690	614	11,304		23,798	106,754	224,746
2033	17	14,709	11	10,746	614	11,360		23,916	95,394	200,830
2034	18	14,786	11	10,802	614	11,416		24,033	83,979	176,797
2035	19	14,863	11	10,858	614	11,472		24,151	72,507	152,646
2036	20	14,940	11	10,914	614	11,528		24,270	60,978	128,376
2037	21	15,017	11	10,971	614	11,585		24,390	49,393	103,986
2038	22	15,096	12	11,028	614	11,642		24,510	37,751	79,476
2039	23	15,174	12	11,086	614	11,700		24,631	26,052	54,845
2040	24	15,253	12	11,143	614	11,757		24,752	14,294	30,093
2041	25	15,332	12	11,201	614	11,815		24,874	2,479	5,219

Appendix B

LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report, AECOM 2008

LGD of Mystery Lake Waste Geotechnical and Topographic Investigation for the Waste Disposal Ground, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works, JR Cousin Consultants Ltd., 2011

LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Scope Change #2 – Additional Test Holes, JR Cousin Consultants Ltd., 2012

Phase I Construction Works - Hydraulic Conductivity Test Results, NTL, September 14, 2012

Phase II Construction Works – Hydraulic Conductivity Test Results, NTL, October 29, 2013

Phase III Construction Works - Hydraulic Conductivity Test Results, Stantec, October 23, 2014

LGD of Mystery Lake Existing Waste Disposal Facility Assessment and Closure Report, AECOM 2008	

The Manitoba Water Services Board
Local Government District of Mystery Lake
Existing Waste Disposal Facility
Assessment and Closure Report

Prepared by: UMA Engineering Ltd. 1479 Buffalo Place Winnipeg, MB, R3T 1L7

UMA Project No.: 0326 060 00 03 (4.6.1)

Mr. David Shwaluk, P.Eng. The Manitoba Water Services Board 2022 Currie Boulevard Box 22080 Brandon, Manitoba R7A 6Y9

Dear Mr. Shwaluk:

Re: LGD of Mystery Lake Existing Waste Disposal Facility
Assessment and Closure Report

UMA Engineering Ltd. (UMA) is pleased to submit our report summarizing the engineering assessment for the closure of the existing waste disposal facility on behalf of the Local Government District of Mystery Lake and the City of Thompson.

Should you have any questions or require additional information, please contact Mr. Clifton Samoiloff, B.Sc. directly at (204) 284-0580.

Yours truly,

UMA Engineering Ltd.

Ron Typliski, P.Eng. Regional Manager Earth and Environmental

cc: Ken Allard, City of Thompson Carol Taylor, LGD of Mystery Lake

Disclaimer

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1.0 Introduction

The Local Government District (LGD) of Mystery Lake currently operates a Class I Waste Disposal Facility (WDF) servicing the LGD and the City of Thompson, under Manitoba Conservation Permit N-02 (issued March 26, 1992). The existing WDF is located on Part NW ¼ 18, S ½ & NW ¼ 19 in TWP 77-3 WPM and in Part SE ½ 24-77-4 WPM, approximately 4 km south of the City of Thompson (Figure 01).

UMA Engineering Ltd. (UMA) was retained by The Manitoba Water Services Board to complete an engineering assessment and to develop a Closure Plan for the existing WDF. According to the Request for Proposal dated April 7, 2005, local officials estimate that the WDF will reach the end of its useful life within five years. As such the municipalities are anxious to develop a new Class I facility to replace the existing WDF before it reaches its capacity. Closure of the existing facility would occur once the new facility is operational. To prepare for landfill closure, a Closure Plan is required in accordance with Manitoba Regulation 150/91, Waste Disposal Ground Regulation.

The existing WDF is owned and operated by the LGD of Mystery Lake under Crown Land Permit No. GP 50804 issued by Manitoba Conservation, dated February 22, 2005. A copy of the Permit is provided in Appendix A. Waste sources include commercial and residential waste from the LGD and the City of Thompson. Operations include compaction of the wastes, placement of cover soils and preparation of new cells.

Access to the site is via a gravel road west off of PTH 6. The WDF is approximately 24 ha in size. The site is generally covered in grasses and the surrounding area consists primarily of forested land, with the exception of a Manitoba Hydro transmission line and PTH 6, which border the site to the east.

The following report provides documentation on the existing WDF in support of a submission to Manitoba Conservation as per Manitoba Regulation 150/91. The study was completed based on the work program outlined in our initial proposal submission dated April 27, 2005. The work program involved: an assessment of the landfill, including site surveys, geotechnical and hydrogeological investigations; an assessment of remaining capacity; and recommendations for closure, including cost estimates.

2.0 Site Development and Remaining Capacity

2.1 Site Layout

In general, the site is composed of a reception/operations area, former and active waste areas, a used oil filter/container Eco-Centre, a recycling depot, and designated areas for burning, asbestos material, clay stockpile, metals, tires, white goods, and automobiles. The facility also includes a sewage treatment plant sludge drying pit and soil remediation area. The site is unfenced, however, the entrance to the facility is gated. The general layout of the WDF is depicted on Figure 02. Photographs of the overall site are provided in Appendix B. Individual photographs relating to specific site features are referenced below.

The hours of operation for the WDF are 8 am to 6 pm Monday to Saturday. The entrance to the waste and stockpile areas is manned at all times when the facility is open. The site access gate is locked when the facility is closed.

The following are observations noted during the site investigation:

- The surfaces of the WDF are fairly well drained other than in the vicinity of the soil remediation area (Photo 1). There are no defined drainage ditches along the perimeter of the WDF other than on the north side. At the time of the site investigation, ponded water was observed in the north ditch and along the western border of the facility (Photos 2, 3 and 4). The south and east perimeter of the facility is well drained due to the slope of the land.
- In the active area, refuse is not confined with berms (Photos 5 and 6). Refuse from the active area is in contact with water in the north ditch. Blown refuse litters the trees on the north, east and west borders of the site (Photos 7, 8 and 9). The former waste cells have been covered with clay and vegetation has been established in these areas (Photo 10).
- Two above ground petroleum storage tanks were observed in the reception/operations area (Photo 11).
- Unburied plastic bags containing asbestos material were observed within the asbestos material area (Photo 12).
- A pile of sludge, approximately 20 m³ in volume, was observed within the asbestos material area (Photo 13). According to municipal officials, the sludge is from the City of Thompson sewage treatment plant. A small pond of water was observed adjacent to the pile of sludge (Photo 14).

2.2 Above and Below Grade Development

The existing limits of above grade development are shown on Figure 02. The height of the former and active waste disposal areas is an average of approximately 5 m above the existing grade elevation. The maximum elevation of the waste mound is 7 m from grade.

According to the current operator at the WDF, the past and present waste cells were developed below grade. This was confirmed by the absence of the surficial layer of native high plastic soil (that was observed in the test holes surrounding the site) in the test holes completed within the former waste cells (refer to Section 4.3).

2.3 Remaining Capacity

An assessment of the remaining capacity at the existing WDF was conducted to determine whether the facility can accommodate wastes from the LGD and the City until a new WDF can be constructed.

The existing WDF property is approximately 58 ha in size. Of this land, approximately 34 ha remain undeveloped. However, the land located to the west of the developed area is not ideal for expansion of the facility as a good portion of it is low-lying and wet. Therefore, for the purposes of this study, the remaining capacity of the WDF is considered to be limited to the available area within the previously developed and current active areas. If development of the low lying area to the west is considered in the future, detailed geotechnical and hydrogeological investigations would be required to confirm its suitability.

The remaining capacity of the existing WDF is dependant on the available area, fill height, waste generation rate and compaction density. As a general guideline, waste generation rates are in the order of 1.5 to 3.0 kg/person/day. This rate is dependent on the level of industrial development in the region. More industry typically relates to higher generation rates. Waste generation estimates provided by the City of Thompson and the LGD of Mystery Lake indicate that the current waste generation rate is estimated at 5.5 kg/person/day. This includes both the residential and commercial waste streams. As this value is significantly greater than typical waste generation rates, there is a concern as to the accuracy of the figure reported. Therefore, the upper end of the range of typical waste generation rates, 3.0 kg/person/day, is assumed for this study.

Based on Canada Census information, the population of the City of Thompson was 13,256 in 2001. Assuming an annual growth rate of 1.0% since 2001, based on the current economic development within the region, the 2006 population of the City would be approximately 13,932. According to the LGD of Mystery Lake, the 2006 population of the LGD is only 5 people. The current combined population is therefore estimated to be 13,937 people. Based on a waste generation rate of 3.0 kg/person/day and assuming a compacted density of 350 kg/m³ of waste, this equates to an estimated volume of approximately 44,000 m³ of waste being deposited in the WDF in 2006.

Currently, the active area is approximately 22,500 m² in size. The height of this area is an average of approximately 3 m below the final elevations of the older portions of the facility. If the active area is only built up to the elevation of the former waste disposal areas, the WDF would only have sufficient capacity for approximately one more year. To provide sufficient time to design, obtain an environmental licence and construct the new WDF, the existing WDF must remain in operation for approximately 2 to 3 years. To accommodate 2 to 3 years of wastes from the LGD of Mystery Lake and the City of Thompson, the WDF would have to be built up to an elevation above that of the former waste disposal areas.

An area of approximately 100,000 m² is available within the active and the former waste disposal areas for further above grade development. Based on this area and a waste generation rate of 44,000 m³/year over three years, the waste would have to be built up approximately 1.3 m, not including monthly and final cover material. Assuming a requirement of approximately 65,000 m³ for monthly and final cover material (refer to Section 5.2), the final elevation of this area would be approximately 2.0 m above the existing grades. Further above grade development would result in sections of the waste disposal areas being above the elevation of PTH 6.

3.0 Geological and Hydrogeological Setting

3.1 Physiography

The physiography of the Thompson area is a reflection of the underlying bedrock terrain and the various glacial deposits formed during the last Ice Age. The terrain is undulating and is characterized by bedrock ridges and knolls interspaced with till plains and poorly drained areas of organics.

3.2 Bedrock Geology

The regional bedrock geology is consists of bedrock outcrops consisting of Precambrian felsic migmatite, gneiss, granofels, and mafic granulite.

3.3 Surficial Geology

The surficial soils in the area typically consist of clay with thicknesses ranging from a thin veneer to up to 30 m forming extensive former lake plains. Where the drift thickness is thin the overlying topography generally mirrors the underlying bedrock surface. Water well driller's records in the area indicated that the general soil profile consists of clay underlain by till with silt and sand overtop of bedrock.

3.4 Hydrogeology

Water Resources Branch water well records indicate little groundwater development in the Thompson area other than within the City itself. There are no domestic groundwater wells in use within a distance of at least 2.0 km of the existing WDF site.

There is no information available on the regional groundwater flow system. Based on conditions in similar environments, the regional groundwater flow is likely towards the surrounding lakes with localized discharge in topographic lows.

4.0 Site Investigation

4.1 General

A topographic survey, geotechnical investigation, hydrogeological investigation, and groundwater quality analysis were conducted at the existing WDF to determine the extent of leachate contamination at the facility and provide technical data for closure of the site.

4.2 Topography

Within the former and active waste disposal areas, the WDF site is generally flat with a gentle slope to the west. A bedrock outcrop rises to an elevation of approximately 8 m along the eastern border of the site, parallel to PTH 6. The area surrounding the WDF is an undulating downward slope toward the west.

Level surveys were performed to establish ground elevations within and surrounding the WDF. Ground elevations based on the survey are depicted on Figure 03. A level survey of the ground surface and top of the PVC pipe at each of the monitoring well locations was also completed. The results of the monitoring well survey are summarized on Table 3.1 below.

4.3 Geotechnical Investigation

A total of eleven (11) 127 mm diameter test holes were completed at the existing WDF on October 5, 2005. Eight (8) of the test holes (TH401, TH401A, TH402, TH403, TH403A and TH405 to TH407) were drilled along the perimeter of the facility to determine the soil conditions underlying the site and three (3) test holes (TH408 to TH410) were drilled within former waste cells to determine the depth of the waste. The locations of the test holes are shown on Figure 03. Several test holes were completed as monitoring wells. These holes are labelled as MW rather than TH (for example, TH401 is labelled as MW401 on Figure 03).

The depth of the test holes ranged from 3.0 m to 10.7 m. All test holes were visually logged in the field for soil type, moisture content, consistency, density and visual evidence of impact (i.e. staining discolouration, odour). Test hole logs are provided in Appendix C.

Soil Stratigraphy

The soil stratigraphy encountered in the test holes completed along the perimeter of the site generally consists of a 1.0 m to 2.1 m thick layer of high plastic clay overlying a layer of varved clay which ranges from 1.0 m to 4.0 m in thickness. Along the bedrock outcrop that runs along the east end of the site, the varved clay is underlain by sand to auger refusal. Beyond the bedrock outcrop, the varved clay is underlain by a layer of varved silt which ranged from 3.7 m to 7.6 m in thickness. In TH403A, the material encountered consisted of 2.1 m of clay fill and 0.6 m of waste underlain by varved clay. Auger refusal was encountered in MW401, TH401A, MW402 and MW407. The refusal depth ranged from 3.0 m to 7.3 m below the surface.

Soils encountered in TH408 consisted of clay fill to the end of the test hole (4.6 m). The test hole was completed near a clay stockpile in the centre of the WDF. The depth of clay fill in this test hole indicates that this location may have been a former clay stockpile area. In TH409, the material encountered consisted of 0.3 m of clay fill underlain by a 2.7 m thick layer of waste, 1.5 m of clay fill, and another 1.5 m thick layer of waste followed by native soils composed of high plastic clay varved with clayey silt.

Similarly, the material encountered in TH410 consisted of 0.3 m of clay fill underlain by a 2.4 m thick layer of waste followed by native varved clay soils.

4.4 Hydrogeological Investigation

Monitoring wells were installed around the perimeter of the WDF to determine the depth of the water table, the horizontal gradient and flow direction within the overburden.

Overburden Monitoring Wells

Monitoring wells were installed in the overburden soils at six (6) test hole locations, MW401, MW402, MW403, MW405, MW406 and MW407. Wells MW401 and MW407 were installed upgradient of the site. Wells MW402 and MW406 were installed cross-gradient to the site. Wells MW403 and MW405 were installed down-gradient from the site. The piezometers were completed as 50 mm diameter PVC wells complete with a 1.5 metre slotted screen. The annular space around the intake was backfilled with silica sand followed by bentonite pellets to surface. Construction details for the monitoring wells are shown on the corresponding test hole logs presented in Appendix C. The intake screens for MW401, MW402 and MW407 were installed within a layer of sand. The remainder of the monitoring well screens were installed in a varved silt layer.

Following installation of the overburden monitoring wells, groundwater level measurements were recorded at each well to determine equilibrium water levels. All water level measurements were made using an electric sounding line referenced to the top of the well casing. The results are summarized on Table 3.1.

Table 3.1 – Summary of Monitoring Details

	MW401	MW402	MW403	MW405	MW406	MW407
Installation Details	Installation Details					
Top of PVC Pipe	227.859	218.559	208.623	212.411	214.583	219.088
Ground Elevation	226.763	217.952	207.884	211.471	213.685	218.285
Top of Screen	225.263	215.662	201.784	205.371	207.585	212.495
Bottom of Screen	223.763	214.142	200.264	203.851	206.065	210.965
Static Water Level						
November 21, 2005	225.119	217.079	208.073	210.511	211.333	Dry

Groundwater Table

The groundwater levels recorded in the overburden monitoring wells on November 21, 2005 range from 0.87 m to 2.35 m below ground surface, with the exception of MW403, in which the water level was 0.19 m above ground. Based on these water levels, the direction of flow within the overburden is towards the west-southwest. This direction corresponds with the general slope of the topography in this area. The magnitude of the horizontal gradient within the overburden soils (change in water elevation with distance)

is about 0.069 m/m. The groundwater level measurements and inferred flow direction are illustrated on Figure 04.

Hydraulic Conductivity Testing

On November 21, 2005, single well hydraulic conductivity tests (bail tests) were conducted on the five (5) monitoring wells at the site that contained water. The data was analyzed with AqtesolveTM software, using the Bouwer and Rice (1976) method. The results are included in Appendix D. The measured hydraulic conductivity values ranged from 1.2×10^{-4} cm/s to 4.5×10^{-5} cm/s in the monitoring wells installed within the sand (MW401 and MW402), and from 1.3×10^{-6} cm/s to 2.8×10^{-7} cm/s in the monitoring wells installed within the varved silt (MW403, MW405 and MW406).

Contaminant Migration

To evaluate the potential impact of leachate from the WDF on the underlying groundwater, an assessment of the vertical and lateral migration of contaminants from the proposed landfill site was conducted based on the following:

- leachate movement by advection,
- no natural attenuation of leachate,
- an average hydraulic conductivity of 2.0 x 10⁻⁶ cm/sec for the varved clay soils, and 8.3 x 10⁻⁵ cm/sec for the sand soils,
- a downward (vertical) gradient of 0.3 m/m,
- an average effective porosity of 0.10,
- the vertical and horizontal rate of migration (average linear velocity) calculated using Darcy's Law:

 $q = Ki/n_e$, where: q = average linear velocity

K = average hydraulic conductivity

i = average hydraulic gradient

n_e = average effective porosity of the clay

Using the above parameters, a vertical rate of migration of about 0.19 m/year is estimated for the varved clay layer, and 78.5 m/year for the sand layer. Based on the siting guidelines, a continuous layer of varved clay, ranging from 1 m to 4 m in thickness, with a vertical rate of migration rate of 0.19 m/year corresponds to a high geological sensitivity rating for the site. Based on the rate of vertical migration through the sand layer, it would not have a significant effect on the geological sensitivity rating of the site given the influence of the varved clay layer.

4.5 Groundwater Quality Assessment

Water samples were recovered from the monitoring wells to determine whether leachate from the site may be impacting the local groundwater.

Groundwater Sampling and Discussion of Water Quality Results

Monitoring wells MW401, MW402, MW403, MW405 and MW406 were sampled on November 4, 2005. MW407 was reported dry. The samples were submitted to Enviro-Test Laboratories in Winnipeg, Manitoba for chemical analysis.

The samples were analyzed for a range of parameters including; trace organics (benzene, toluene, ethylbenzene, and xylenes (BTEX)), total volatile hydrocarbons (TVH) and total extractable hydrocarbons (TEH), inorganics and total metals. As a result of limited recovery, MW-401 was only sampled for select inorganics and total metals. The test parameters included in the laboratory analyses were stipulated in the Siting Guidelines for Class II and Class III Waste Disposal Grounds. Although these analyses were originally intended for new waste disposal sites, they are also appropriate for use in monitoring existing and closed waste disposal sites. The laboratory analytical results are presented in Table 1, in Appendix E along with a copy of the laboratory report.

Analytical results have been compared with the Canadian Council of Ministers of the Environment (CCME) Canadian Environmental Quality Guidelines (CEQG) for Community Water, (updated December 2004). The appropriate Community Water quality guidelines are noted on Table 1.

Concentrations of all trace organic parameters were non-detect and below the applicable CCME guidelines. All metal and inorganic parameters analysed were below the selected CEQG, with the exception of aluminium in all wells, iron in one gradient and two down-gradient wells, manganese, selenium and sodium in down-gradient wells, and turbidity and total dissolved solids in almost all of the wells. The aluminum concentrations exceeded the CEQG by magnitudes ranging from 1.4 to 4.0. Iron concentrations exceeded the CEQG by magnitudes ranging from 1.4 to 2.0. Manganese concentrations exceeded the CEQG by magnitudes of 2.8 to 7.7. Selenium and sodium values exceeded the CEQG by factors of 1.2 and 1.3, respectively. Turbidity values well exceeded the CEQG and the measured total dissolved solids values were generally twice the CEQG.

Although there is insufficient data to define specific trends, results of the analysis indicate that the greatest impact on water quality appears to be in monitoring wells MW403 and MW405, located down-gradient of the existing active area. The least amount of impact appears to be in well MW406 to the north and cross gradient from the existing active area. Further groundwater sampling is required to ascertain whether leachate from the WDF is impacting the underlying groundwater.

In most cases, values that exceeded the CCME limit will affect the aesthetic water quality and do not pose a risk to human health or the environment. On this basis, there is currently no risk to local groundwater users. The following is a brief interpretation on those parameters which exceeded the CEQG.

Turbidity

Turbidity in drinking water should not exceed 1 unit. Levels exceeding this value may make water unpleasing or may protect micro-organisms against the effects of a disinfection agent. Elevated levels were noted at all sampled locations. Turbid samples are common from newly installed wells and typically diminishes after periodic development and resampling of the wells.

Total Dissolved Solids

This is a measure of the dissolved minerals in the water. As a general rule, greater than 500 mg/L (aesthetic objective) is considered unsatisfactory. Levels higher than this are not necessarily a problem as it depends on the specific minerals present. Elevated levels were noted in the cross-gradient wells (MW402 and MW406). Levels were approximately twice as high in the down-gradient wells (MW403 and MW405).

Aluminum -Total

Aluminum is the third most common element in the earth's crust and is naturally present in soils and water. The total aluminum concentrations noted in all wells exceeded the CEQG. These values may, however be a result of suspended sediment in the water from drilling activities or may be indicative of natural groundwater concentrations in the area.

Iron – Total

If the concentration of iron is above 0.3 mg/L, it will cause staining of laundry and fixtures. Higher concentrations will produce a metallic taste and may produce a yellow precipitate. If the concentration of iron is above 0.5 mg/L, it may interfere with zeolite water softening. As illustrated in Table 1, elevated levels of iron were noted at three of the five points sampled including one upgradient well (MW401) and the two down-gradient wells (MW403 and MW405). Elevated iron is common in groundwater in Manitoba and the results may indicate natural background conditions

Manganese - Total

Manganese is undesirable in domestic water supplies because it causes unpleasant tastes, deposits on food during cooking, stains or discolours laundry and plumbing fixtures and fosters the growth of some micro-organisms in reservoirs, filters, and distribution systems. The guideline limit for these aesthetic considerations is 0.5 mg/L. Elevated levels were noted at downstream wells in comparison to the upgradient point MW401. This may be indicative of impacts to the underlying groundwater from the WDF.

Selenuim - Total

The concentration of selenium exceeded the CEQG in one of the downgradient sampling points. The reported concentration at MW405 was however only slightly above the guideline value. Although the CEQG are based on health risk, most toxic effects of selenium appear to be associated with the consumption at high concentrations in food rather then water.

Sodium -Total

Most soils contain sodium in the range of 0.1 to 1 percent. Because of the high solubility of sodium minerals, sodium is ubiquitous in the water environment. Elevated sodium concentrations were noted in both of the downgradient wells, with reported values in MW403 and MW405 slightly above and slightly below the CEQG. These elevated concentrations may be indicative of impacts to the shallow groundwater regime below the site.

Quality Control Program

To ensure a high level of quality throughout the sampling and analytical stages of the project, a number of controls and procedures were followed.

Dedicated disposable bailers were used to collect all water samples. The collected samples were placed in laboratory supplied sample bottles with no headspace and stored on ice in a cooler. All samples were shipped to the lab and analyzed within the accepted holding times.

One blind field duplicate (labelled MW999) was collected from monitoring well MW403 during the November 4, 2005 sampling event. The laboratory analysis results are provided in Table 2 of Appendix E. Generally, the results of the laboratory analyses for the field duplicate sample collected are within Enviro-Test Laboratories target analysis error range for sample concentrations greater than 10 times the detection limit. The duplicate analysis also provides a check of the integrity of the field sample collection and handling procedures. The above duplicate results validate the current field protocols.

5.0 End Use Development / Site Closure Plan

5.1 Proposed End Use Development Plan

The proposed End Use Development Plan for the site is to restore the area to a natural green space. The surface of the WDF will be graded and seeded to establish rough natural grasses. This proposed end use represents a low-cost, low-impact and low maintenance approach to site development. The final landfill footprint and proposed grading are shown in plan view in Figure 05.

5.2 Cover Material

An assessment was completed to determine the volume of clay soil required for monthly and final cover to achieve the final landfill configuration. This assessment was based on the Manitoba Waste Disposal Grounds Regulation 150/91, which stipulate that wastes must be covered with 0.15 m of clay per month and 0.5 m of clay upon termination of use of an active area.

Based on the available surface area for above grade development at the WDF (refer to Section 2.3), the surface area which would require final cover is approximately 100,000 m2. Given a final cover thickness of 0.5 m, this area would require approximately 50,000 m3 of final cover material. Assuming a waste to soil ratio of 10:1 to determine the volume available for refuse placement and monthly cover, the disposal volume would consist of approximately 132,000 m3 of refuse and 15,000 m3 of monthly cover. Therefore, the total volume of cover material required, monthly and final, would be approximately 65,000 m3. Additional cover material will also be required to cover portions of the WDF that do not have at least 0.5 m of cover material. Test pits/holes should be completed throughout the WDF to identify sections that do not have sufficient cover.

Clay cover could likely be obtained from the land owned by the LGD directly west of the existing WDF. Clay cover material for the active area is currently obtained from a borrow pit located within the proposed WDF site on the adjacent land to the north. Borrow activities should be discontinued in this area so it can be filled with compacted clay in preparation for the new WDF.

5.3 Drainage

Ditching should be constructed around the entire facility to prevent surface water run-on into the WDF and direct all surface water runoff away from the site. Proposed and existing drainage features are shown on Figure 05.

5.4 Site Grading

Figure 05 highlights the limits of the development based on the proposed end use plan. Grading of the final cover material is required to minimize leachate production by minimizing surface infiltration and promoting positive surface runoff. The final surface of the cap of the WDF should be graded at approximately 4% with the exception of the outer slopes which should be completed at a slope of 5H:1V. The construction of steeper slopes will have a lower factor of safety and may include an element of risk related to satisfactory slope performance. An even greater risk can be expected if proper quality control and compaction standards are not followed during construction activities.

5.5 Landscaping

Based on the proposed end use development plan, site landscaping will consist of rough grass areas to be seeded with a mix of hearty ground cover supported by a growing medium consisting of a thin layer peat moss and sand tilled into the clay cap.

5.6 Signage

Upon closure of the site, a sign should be posted at the gate indicating that the site is closed and the location of the new facility should be provided.

5.7 Site Specific Closure Requirements

Several items were identified during the site investigation that would require attention prior to completing closure of the site. These items include containment of the active waste disposal area, fencing, and decommissioning of onsite facilities.

Active Waste Disposal Area

- Berms must be constructed around the active area to contain the wastes and any leachate generated within the wastes. The top of the berms should be at least 0.5 m higher than the proposed height of the wastes.
- Clearing of litter from the trees around the perimeter of the WDF is required. Temporary fencing is recommended to minimize the amount of blown litter from the active area.

Fencing

According to current regulations, active waste disposal facilities must be fenced. A fence should be
erected around the entire WDF as it will remain in operation until a new facility is developed. The
fencing will prevent access to the site once it is closed.

Decommissioning of Onsite Facilities

 The existing WDF has several facilities that will require decommissioning as part of closure of the site. These include the soil remediation area, sludge drying pit, recycling depot, and all other buildings onsite.

Other items include the following:

- The existing burning area must be levelled, compacted and covered with 0.5 m of clay,
- Stockpiles of metals, tires, white goods, etc. must be removed from the site,
- The pile of sludge in the asbestos area should be sampled and tested to determine if treatment of the sludge is required prior to it's disposal in the active area of the WDF,
- Ponding water in the asbestos area should be removed using a vac-truck and disposed of at the City
 of Thompson sewage treatment plant, and
- Exposed bags of asbestos material should be buried on-site in the designated area.

6.0 Post Closure Monitoring and Maintenance

6.1 Site Maintenance

Cover Soils

The cover soils play an integral role in the minimization of leachate generation by reducing the amount of surface infiltration. It is therefore important to monitor the integrity of this layer and complete remedial works in areas where the cover has deteriorated. Cover deterioration can occur due to erosion, desiccation cracking, frost heave and cracking resulting from waste settlement. A regular inspection of the cover will identify problem areas and allow maintenance actions to be taken before the problem results in significant adverse effects. Maintenance could include adding additional fill soils, re-grading or revegetating exposed or eroded areas.

Monitoring should be completed monthly, from April to November, during the initial two years of post closure care. Subsequent monitoring can be conducted on a semi-annual basis in the spring and fall. Post closure monitoring and maintenance of this nature generally continues for a minimum period of 20 years following landfill closure.

Landscaping

The proposed landscaping is very low maintenance except during the initial establishment period of two to three years. During the seed establishment period, additional mowing and some chemical control may be required, along with re-seeding or over-seeding to obtain acceptable growth covers. The rough grass areas should be mowed annually or managed by controlled burning every three years.

6.2 Environmental Monitoring

It is generally accepted practice to provide post-closure environmental monitoring of a landfill site for a minimum of 20 years following closure. The purpose of the environmental monitoring plan is to provide a background database, meet regulatory requirements and demonstrate the environmental integrity of the landfill. The following program has been developed to meet these needs. The monitoring program includes surface water, groundwater, leachate and methane gas. Specific details on each program are provided below.

Surface Water

Surface water surrounding the landfill site should be monitored on an annual basis to evaluate any potential impacts on water quality from the landfill operations. Monitoring will involve the sampling of two points including the discharge point of the perimeter ditches located in the southwest corner of the WDF and of the surface water body (marsh) located immediately southwest of the facility as shown on Figure 02.

In addition, specific samples should be collected in areas adjacent to localized leachate breakouts, if any occur.

Surface water samples should be analyzed for common major and minor inorganic constituents. Analyzing for organic contaminants and EPA priority pollutants should be kept to a minimum. Analytical targets should be based on the results of detailed samples of landfill leachate. Grab samples should be collected at each sampling location during late spring. Any significant amount of suspended matter should be separated by decanting and/or filtering. Samples should be filtered using disposable in-line units. The solids residue should be recorded and also analyzed.

Groundwater

Monitoring of the groundwater system should be completed through routine sampling of perimeter monitoring points. Six (6) overburden monitoring wells were installed as part of the WDF site investigation in October 2005 (MW401-MW403, and MW405-MW407). The locations of the monitoring wells are shown on Figure 03. It should be noted that no domestic wells are located down-gradient of the site. Potable water wells are located up-gradient, with the closest being approximately 2 km from the site.

All points should be sampled on an annual basis, preferably in late spring. The monitoring wells should be purged prior to sampling to remove any standing water in the casing and to bring in fresh formation water. This will ensure that a representative groundwater sample is collected. A minimum of three well volumes should be evacuated before a sample is collected.

Groundwater samples should be analyzed for common major and minor inorganic constituents. Organic and EPA priority pollutant analyses should be kept to a minimum. Detailed chemical analysis of the leachate for inorganic, organic and EPA priority pollutants should be completed to establish which of these parameters can be best used for detective monitoring. Focusing on the parameters likely to be elevated by leachate contaminants will help reduce the overall cost of chemical analysis.

Piezometric levels should be recorded at each of the monitoring wells prior to each sampling event. This information should be used to monitor the horizontal flow gradients beneath the site and confirm that the vertical gradient through the overburden remains downward.

To initiate a database on the background water quality, groundwater samples have been collected from the overburden monitoring wells. A copy of the laboratory report is found in Appendix E. A summary of the results is provided on Table 1. The sampling procedure and interpretation of laboratory results is outlined in Section 4.5.

Leachate

Test holes completed within the former waste disposal areas indicate that the decomposing wastes are saturated with leachate. Therefore, a leachate monitoring program is recommended to determine the potential for the build up of leachate to "break out" of the containment area. It is recommended that eight monitoring wells be installed throughout the former waste disposal areas to assess the potential need for a leachate collection system. A detailed drilling program to determine the horizontal and vertical extent of the wastes would be required to assess the requirements for the leachate monitoring program and a leachate collection system.

Upon installation of monitoring wells within the former waste disposal area, leachate quality should be monitored to characterize the quality of leachate being generated and to identify what chemicals could potentially be used as target indicators in the ground and surface water monitoring programs. As a minimum, two leachate samples should be analyzed annually. Once a consistent data base has been developed, the number of samples and sampling frequency can be reduced. Analysis should include inorganics, organics and EPA priority pollutants.

Methane Gas

Gas is generated from the decomposition of organic material contained in the landfill. The main constituents of the produced gas are methane and carbon dioxide. The gas has the potential to migrate through the soil and collect in explosive concentrations in enclosed spaces and can damage vegetation and reduce the quality of groundwater and air.

The gas within the landfill is generally under positive pressure which causes lateral and vertical migration. The purpose of monitoring landfill gas is to determine the extent of this migration. It is proposed to allow passive venting of the landfill gas through the cover soils, therefore vertical migration would not a concern.

To assess lateral migration, it is recommended that four (4) gas probes be installed at the locations indicated in Figure 05. The points should be located near the toe of the landfill development. If and when measurable concentrations are detected, additional points can be installed near the property limits to assess the potential for off-site migration. Past experience has shown that a 30 metre buffer will generally be adequate for lateral control of gas migration. The proposed gas probes should be monitored on a quarterly basis during the initial two years of post closure monitoring to assess seasonal influences and then annually thereafter. Field monitoring should include the gas concentration, percent of the lower explosive limit (LEL), atmospheric pressure and air temperature.

The gas probes should be constructed using Schedule 80 PVC pipe. The upper 1.5 m of the installation should consist of solid pipe. The remainder of the installation should be screened and extend to the depth of the waste placement. The top of the probe should be completed with a sealed cap equipped with a quick connect coupler. The coupler can then be used to directly connect to a gas meter. Silica sand should be placed around the piezometer intake with a bentonite seal at surface. The probes should be installed with a protective steel casing.

7.0 Class C Cost Estimate

The following is a breakdown of the initial capital investments, annual monitoring costs, cost for site closure, post-closure monitoring costs, and associated costs for engineering. Annual costs to operate the existing WDF until its closure, including construction of berms around current and future active areas and monthly cover material, are not included.

7.1 Initial Capital Investment

The initial capital investment includes all costs associated with the closure of the site. This will include: placement and grading of final cover material, removal of stockpiles, decommissioning of onsite buildings, removal of sludge pile and ponded water in asbestos material area, decommissioning of sludge drying pit and soil remediation area, and fenceline and perimeter ditches for the entire site.

The cost for installation of the proposed environmental monitoring network has been included in the program. This includes eight (8) monitoring wells and four (4) gas probes installed within the waste disposal areas. Costs for a leachate collection system have not been included as monitoring is required to determine the need for and required extent of such a system. The cost of signage is included as an incidental to the fencing and gate.

ACTIVITY	UNITS	QUANTITY	RATE	COST
Borrow Pit Development (stripping, clearing/grubbing)	ha	3	\$10,000	\$30,000
Removal of Metals, Tires, White Goods, etc. Stockpiles from the Site	unit	1	\$10,000	\$10,000
0.5 m Final Cover Material and Grading	cu.m.	50,000	\$12	\$600,000
Decommissioning of Onsite Buildings	allowance	1	\$25,000	\$25,000
Removal of Sludge Pile and Ponded Water from Asbestos Material Collection Area	allowance	1	\$10,000	\$10,000
Decommissioning of Sludge Drying Pit	allowance	1	\$10,000	\$10,000
Decommissioning of Soil Remediation Area	allowance	1	\$10,000	\$10,000
Post and Wire Mesh Fence	l.m.	2,000	\$40	\$80,000
Perimeter Ditching (7.0 m ³ – 1,600 lineal m)	cu.m.	11,200	\$10.00	\$112,000
Growing Medium, Seeding, Hydro-mulching	sq.m.	100,000	\$3.00	\$300,000
Installation of Monitoring Well Network	Unit	12	\$1,000	\$12,000
Contingency (25%)				\$299,750
Total				\$1,498,750

7.2 Annual Monitoring Costs

The annual monitoring costs include the cost for surface and groundwater sampling, cover soil inspections and preparation of an annual report. Also included is an option for leachate sampling, methane gas monitoring.

ACTIVITY	UNITS	QUANTITY	RATE	COST
Surface Water Sampling	Units	2	\$500	\$1,000
Groundwater Sampling	Units	6	\$500	\$3,000
Cover Soil Inspection	Unit	1	\$500	\$500
Reporting	Unit	1	\$5,000	\$5,000
Sub-total				\$9,500
Leachate Sampling	Units	8	\$500	\$4,000
Methane Gas Monitoring	Units	4	\$125	\$500
Total				\$14,000

The unit rates provided above are inclusive of all time, equipment rental and materials to collect the samples, analyse the samples and complete any in-situ monitoring. Sampling and monitoring activities assume the use of local personnel provided that qualified personnel from the City are available at the time of these activities.

7.3 Post-Closure Monitoring

The cost for post closure monitoring will be comparable to the annual monitoring cost noted in Section 7.2 and would include: surface and groundwater sampling, cover soil inspection, preparation of an annual report, and potentially leachate sampling and methane gas monitoring.

7.4 Engineering

Engineering costs will include: preparation of a Closure Plan; preparation of technical specifications; tender award; contract administration; and the preparation of as-builts with respect to the closed facility. The costs associated with installation of the monitoring well network and any sampling/monitoring are inclusive and include the cost of engineering. Contract administration and inspection activities could be supplemented with the use of local personnel provided qualified personnel are available at the time of these activities.

ACTIVITY	COST
Preparation of Closure Plan and Technical Specifications	\$20,000
Tender Award	\$2,000
Contract Administration (assume 4 weeks @ \$1,000/day plus 25% office admin)	\$35,000
As-builts	\$3,000
Sub-total	\$60,000

8.0 Summary

The existing LGD of Mystery Lake WDF property is approximately 58 ha in size. Of this land, approximately 34 ha remain undeveloped. However, the land is not ideal for further development of the facility as a good portion of it is low-lying and wet. Therefore, for the purpose of this study, the remaining capacity of the WDF is considered to be limited to the available area within the previously developed and current active areas. To provide sufficient time to design, obtain an environmental licence and construct the new WDF, the existing WDF must remain in operation for approximately 2 to 3 years. The existing WDF can accommodate wastes for this period of time if the active and former waste disposal areas are further developed above grade.

Geotechnical and hydrogeological assessments conducted at the WDF indicate that the site has a high geological sensitivity rating based on the ratings in the Manitoba Conservation waste disposal grounds siting guidelines.

Clay cover material for the active area is currently obtained from a borrow pit located within the proposed WDF site. Borrow activities should be discontinued in this area so it can be filled with compacted clay in preparation for the new WDF. Additional cover material will be required on portions of the WDF that do not have at least 0.5 m of final cover material. Test pits/holes should be completed throughout the WDF to identify sections that do not have sufficient cover. Suitable cover material could likely be obtained from the land owned by the LGD directly west of the existing WDF. A geotechnical investigation would be required in this area to confirm the suitability of the soils for cover material and that sufficient quantities of the material exist.

A groundwater quality assessment consisting of the sampling of monitoring wells installed around the perimeter of the WDF indicates that concentrations of manganese, selenium and sodium are more elevated in the downstream wells as compared to the upstream wells. This may be an indication that the WDF is impacting the underlying groundwater. Continued groundwater monitoring is recommended to ascertain whether leachate from the WDF is impacting the underlying groundwater.

The proposed End Use Development Plan for the site is to complete the area as a natural green space. Specific closure requirements identified during the site inspection include the following:

- Construction of berms to contain the wastes in the active area,
- Construction of perimeter ditching and fencing,
- Placement of 0.5 m of final cover cap and site grading,
- Clearing of blown litter from the trees around the perimeter of the WDF,
- Levelling and compaction of wastes in the existing burning area and placement of cover material in this location,
- Removal of stockpiles of recyclable material from the site,
- Sampling and testing of the pile of sludge in the asbestos area to determine if treatment of the sludge is required prior to it's disposal in the active area of the WDF,

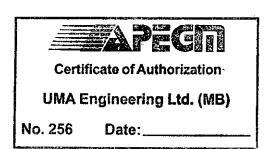
- Removal of the pond of water in the asbestos area using a vac-truck, and disposal of the liquid at the City of Thompson sewage treatment plant,
- Burial of exposed bags of asbestos material in the designated area, and
- Decommissioning of onsite soil remediation area, sludge drying pit, recycling depot, and all other onsite buildings.

Design and implementation of an environmental monitoring program is required to demonstrate the long-term performance of the environmental control measures. The following parameters should be included in the monitoring program:

- surface and groundwater quality;
- leachate production, levels and quality;
- landfill gas; and
- cover integrity.

A "Class C" cost estimate has been developed for the proposed closure requirements. The estimate includes capital investment, annual monitoring costs, closure costs and post closure costs.

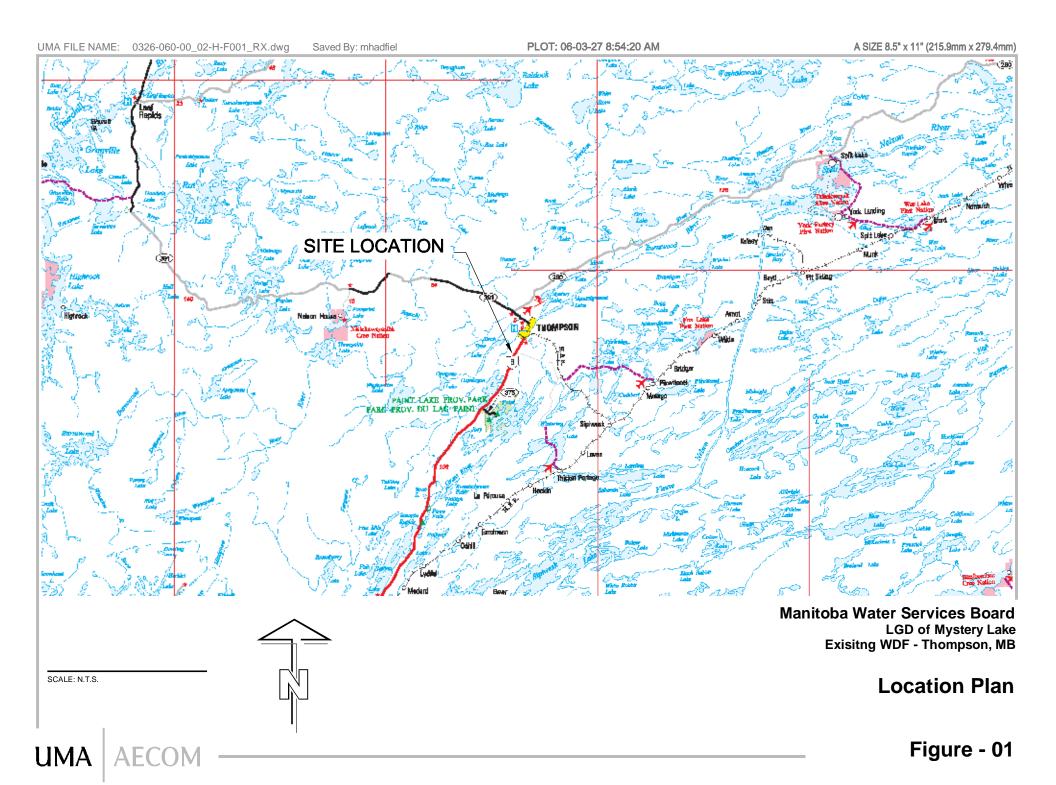
Respectfully submitted,	
UMA Engineering Ltd.	Reviewed By:
Peter Bohonos, P.Eng. Project Manager Earth and Environmental	Steve Wiecek, P.Eng., P.Geo. Senior Hydrogeologist Earth and Environmental
Revised By:	Reviewed By:
Clifton Samoiloff, B.Sc.	Ron Typliski, P.Eng.



9.0 References

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- Manitoba Conservation Guidelines for the Siting, Design, Construction, Operation, Performance Monitoring, and Closure of a Class 1 Waste Disposal Ground in Manitoba, 1994.
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- Manitoba Energy and Mines, Mineral Resource Division, 1981: Surficial Geology Map of Manitoba, Map 81-1, Scale 1:1,000,000.
- Manitoba Energy Mines and Resources, Surveys and Mapping Branch, 1980: Thompson Mystery Lake Local Government District, Manitoba, West of Principal Meridian, 63P/12 Edition 3, Scale 1:50,000.
- Manitoba Industry, Trades and Mines, Manitoba Geological Survey, 2001: Geology of the Ospwagan Lake west (63O/9 west half) and Thompson east (63P/12 west half) area, Scale 1:50,000.





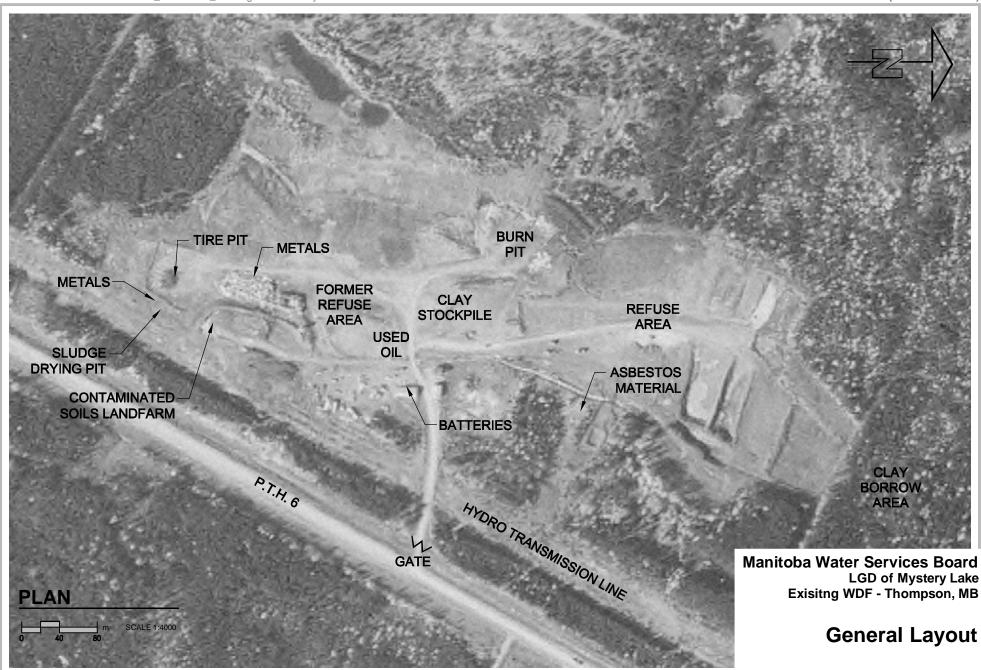




Figure - 03

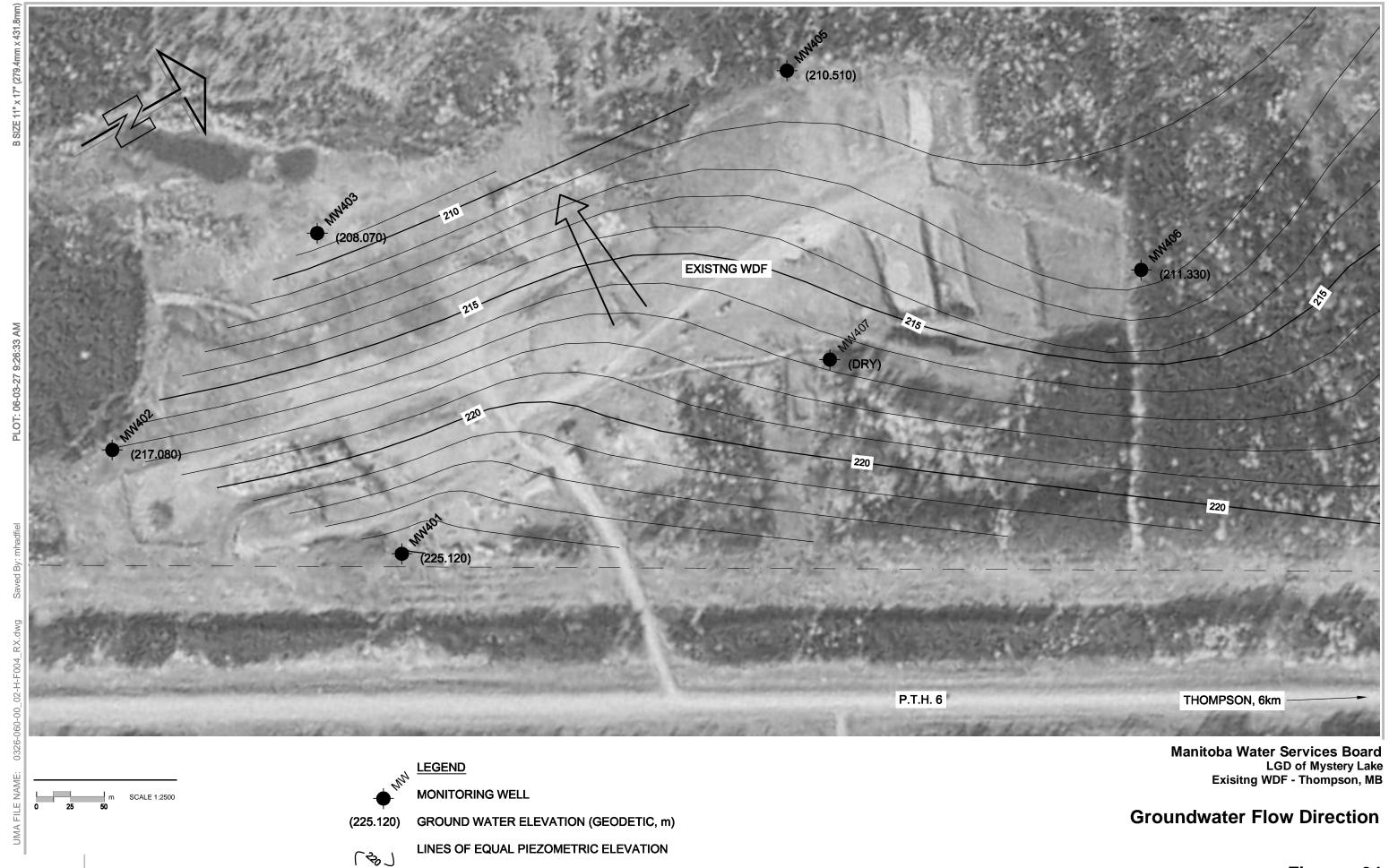


Figure - 04

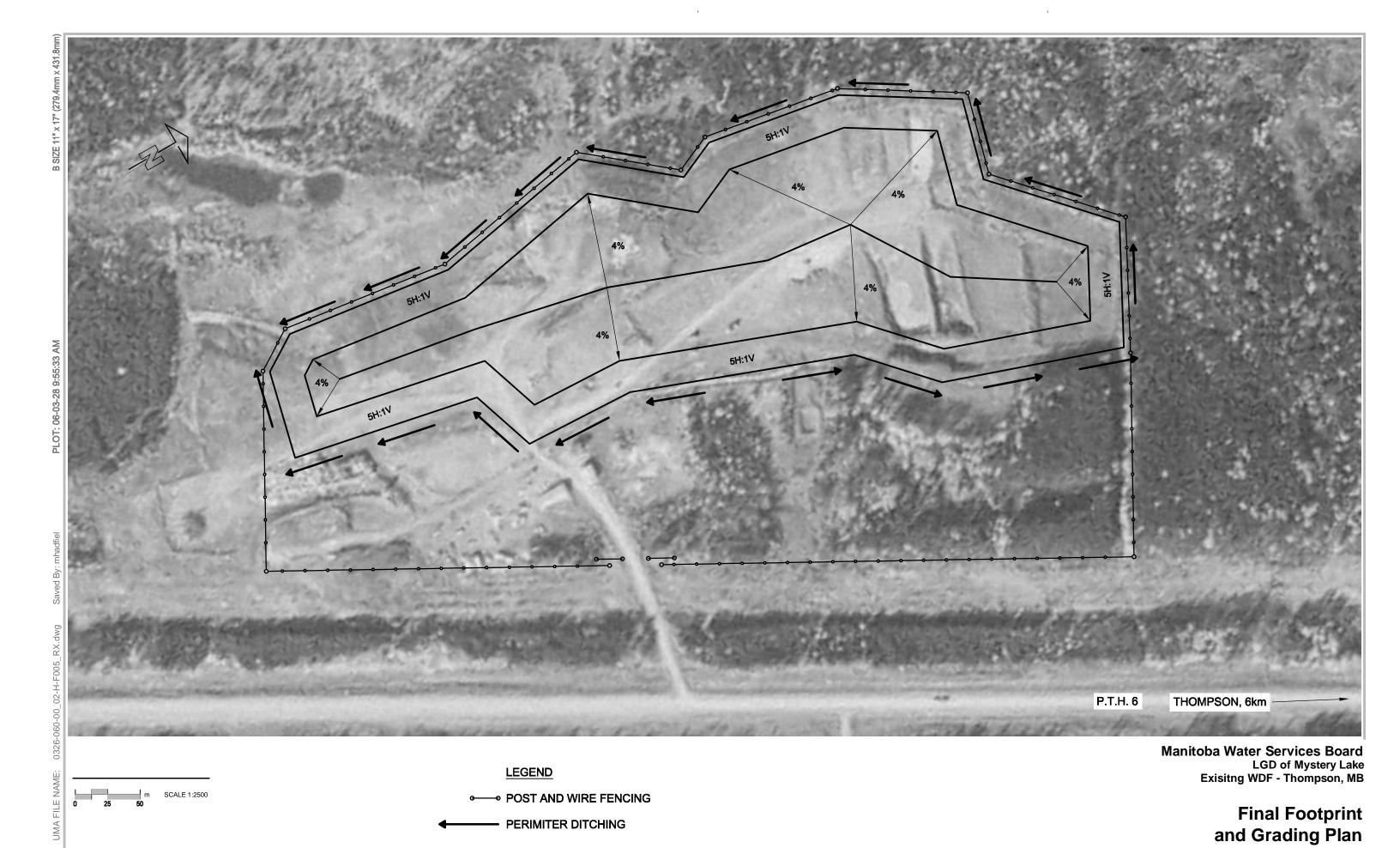


Figure - 05

Appendix A Crown Land Permit

P.O. BOX 189 THOMPSON, MB R8N 1N1 PHONE (204) 677-4075 e-mail: lgdmystlake@mts.net

FAX (204)778-7642

C.A.O.: Carol Taylor



-01/
CUR

To: Marie Elliott, Deputy Minister	
Intergovernmental Affairs	From: Carol Taylor
Fax:1-204-945-5255	Pages:
Phone:	Date: March 23,2005
Re:	CC:
☐ Urgent ☐ For Review ☐ Please Comment • Comments:	t □ Please Reply □ Please Recycle
Good Morning:	
Please find attached a copy of our permit for the lan signing it or would you like to sign it? It must be in New	dfill. Do you have any problems with my epewa by April 22,2005.
Carol Taylor	

Manitoba



Conservation

Lands Branch

Box 20000, 123 Main Street W Neepawa Mb. R0J 1H0 CANADA Tel: (204)-476-7060 Fax: (204)-476-7539

February 22, 2005

Local Government District of Mystery Lake

Attention: Louise Hodder

Box 730

Thompson, Mb. R8N 1N5

Dear Madam:

Re: Site in Part NW1/4 18, S1/2 & NW1/4 19 in Twp 77-3 WPM and in Part SE1/4 24-77-4 WPM as

shown on a sketch on file at Lands Branch.

waste disposal site

Crown Land Permit No. GP 50804

I am pleased to advise that your Crown Land Permit application for the above noted land has been conditionally approved under the terms and conditions outlined in the enclosed Schedule A.

Please review Schedule A. If the terms and conditions are acceptable to you, please sign and date both copies where indicated and have your Witness sign and date both copies where indicated.

Return one copy of the signed Schedule A to this office.

If we have not received a signed copy of Schedule A by April 22, 2005, we will assume that you are no longer interested in this property and your application will be cancelled. Any new application received after that date will be dealt with in accordance with the policies and regulations in effect at that time.

Your permit will be issued upon receipt of the signed copy of Schedule A.

If you have any questions concerning Permit No. GP 50804, please contact Larry Krakowka, Land Administrator at (204) 476-7515.

Yours truly,

Harley Johasson

Director

/km

Copy: Brian Barton, Regional Land Manager

PROVINCE OF MANITOBA MANITOBA CONSERVATION

SCHEDULE "A" TO CROWN LAND PERMIT NO. GP 50804 ("the Permit")

ISSUED BY:

HER MAJESTY THE QUEEN IN RIGHT OF THE PROVINCE OF MANITOBA represented herein by the Honourable Minister of Conservation

("Manitoba")

ISSUED TO:

Local Government District of Mystery Lake

(the "Permittee")

pursuant to The Crown Lands Act as amended from time to time.

WHEREAS:

- A) The Permittee has made an application to Manitoba for a Crown Land Permit for the Land (as described further in this Schedule);
- B) The Permittee is eligible for a Crown Land Permit for the Land and the Land has been determined by Manitoba to be suitable for the use and purpose as described in this Schedule; and
- C) Manitoba agrees to issue a Crown Land Permit to the Permittee, subject to the terms and conditions set out in this Schedule, which is Schedule "A" to the Permit, and the Standard Conditions attached to the Permit, for the land described as follows and as substantially similar to that set out on the map attached as Schedule A1:

Site in Part NW $\frac{1}{4}$ 18, S $\frac{1}{2}$ & NW $\frac{1}{4}$ 19 in Twp 77-3 WPM and in Part SE $\frac{1}{4}$ 24-77-4 WPM as shown on a sketch on file at Lands Branch.

Area: 136.38 acres (1,800 ft. x 3,300 ft.)

(the "Land")

THE PERMIT IS SUBJECT TO THE FOLLOWING TERMS AND CONDITIONS:

1.00 TERM AND RIGHT TO USE AND OCCUPY THE LAND

- 1.01 The Permit shall be effective from the date it is issued by Manitoba until December 31, 2005, subject to termination or extension under section 7.
- 1.02 Subject to the terms and conditions of the Permit, Manitoba grants to the Permittee the right to use and occupy the Land.

2.00 PAYMENT OF FEES AND TAXES

- 2.01 The Permittee shall pay to Manitoba rent equal to the annual fee prescribed from time to time by the Regulations under *The Crown Lands Act*, in accordance with such Regulations and the Permit, within 30 days of receipt of an invoice from Manitoba. The Permittee acknowledges that the current annual fee is \$0.00, as per Item No. 4 of an Agreement dated December 16, 1966 and signed by Manitoba, the International Nickel Company of Canada Limited, the Local Governmet District of Mystery Lake, the School District of Mystery Lake No. 2355, the Town of Thompson and the Resident Administrator of the Local Government District of Mystery Lake.
- 2.02 The Permittee acknowledges that an application for renewal and administration fee in relation to the Permit shall be paid by the Permittee, as prescribed by the Land Administration Fees Regulation (M.R. 216/89) and as amended from time to time.
- 2.03 Payments of the annual fee and the administration fees shall be made in accordance with the directions contained in the invoice from Manitoba.
- 2.04 Manitoba may establish a new annual fee rate where there is a change in one or more of the following factors in order to reflect these changes:
 - a) the appraised value of the Land as determined by Manitoba;
 - b) the appraised value of the buildings and improvements owned by Manitoba;
 - c) the policy of Manitoba as set out in an Act of the Legislature or a Regulation relating to the determination of annual fee; or
 - d) the use of the buildings, infrastructure or Land.

- 2.05 Manitoba shall give notice to the Permittee 30 days prior to the effective date of an increase in the annual fee.
- 2.06 The Permittee shall pay all taxes, rates, duties and assessments whatsoever, whether municipal or otherwise, now or hereafter charged on the Land or in respect of the Permittee's use and occupation thereof.
- 2.07 The Permittee shall pay interest to Manitoba on any arrears of annual fee or administration fees at rate equal to the rate fixed from time to time by the Minister of Finance of Manitoba under section 25(1) of *The Financial Administration Act*. Failing such rate being fixed, interest shall be payable thereon at a rate equal to the rate fixed from time to time by Manitoba.
- 2.08 The Permittee shall pay to Manitoba an amount equal to any and all goods and services taxes now or hereafter imposed on, or collectible by Manitoba with respect to any amounts payable by the Permittee to Manitoba hereunder, whether characterized as a goods and services tax, sales tax, value added tax or otherwise ("Sales Taxes"). The intention of the parties is that Manitoba shall be fully reimbursed by the Permittee with respect to any and all Sales Taxes payable or collectible by Manitoba now or in the future.
- 2.09 The Permittee is responsible for and shall pay any and all costs, charges, impositions and expenses related to the Land, including, without limitation, all water, sewer, gas, telephone, or electric power charges.
- 2.10 If the Permittee fails to pay any and all taxes or water, sewer, gas, telephone, or electric power charges as required, Manitoba may pay them or any of them and charge those payments to the Permittee who shall reimburse Manitoba forthwith and Manitoba may take the same steps for the recovery of those payments as it would be for the recovery of rent arrears.
- 2.11 The Permittee shall pay all amounts payable to Manitoba hereunder without any deduction or setoff whatsoever.

3.00 USE OF THE LAND

- 3.01 The Permittee shall use the Land for a waste disposal site and for no other purpose, including non-use, without prior permission in writing from Manitoba.
- 3.02 The Permittee agrees that the following structures and improvements on the Land are authorized under the Permit: 1 office building (35 ft. x 20 ft.).
- 3.03 Other than those developments and uses permitted under paragraphs 3.01 and 3.02 of this Schedule, the Permittee shall not construct, erect or alter any other buildings or structures on the Land or effect any change in use of the Land without prior permission in writing from Manitoba.
- 3.04 The Permittee agrees to notify Manitoba of any building destroyed, demolished, or removed from the Land within 30 days of that occurrence; and to rebuild, replace or reinstate the building within 24 months of that occurrence.
- 3.05 It is the responsibility of the Permittee to place and maintain all buildings within the boundaries of the Land, and to obtain any Surveyor's Certificates necessary to effect or verify this condition.
- 3.06 Manitoba has no obligation to survey or resurvey the Land, and the Permit shall create no such obligation on Manitoba to survey or resurvey the Land.
- 3.07 The Permittee agrees that removal or relocation of any existing Manitoba Hydro facilities shall be at his/her expense.
- 3.08 The Permittee and its officers, directors, agents, invitees and employees, as applicable, shall be bound by the rules, regulations and guidelines made by Manitoba from time to time. All such rules, regulations and guidelines will be deemed to be incorporated into and form part of the Permit. Some form of advance public notice shall be provided for changes in these rules, regulations and guidelines.
- 3.09 The Permittee shall comply with all federal, provincial and municipal laws and regulations, and obtain all licences and permits necessary for the lawful use of the Land, which, without restricting the generality of the foregoing, includes obtaining a work permit from the local District Resource Officer before cutting any trees or commencing any work on the Land, obtaining a building permit from the Department of Labour before constructing any structures, as may be authorized by Manitoba, in accordance with the Manitoba Building Code and applicable Municipal By-laws and regulations. The Permittee shall provide Manitoba with a copy of work permits or building permits obtained at the request of Manitoba.

- 3.10 The Permittee understands and agrees that the issuance of this Permit in no way implies that either Manitoba or the local government authority shall provide any services.
- 3.11 The Land is contained in the "Burntwood River Water Power Reserve" and this Permit is issued subject to *The Water Power Act* and Regulations thereunder.
- 3.12 The Permittee acknowledges that the Land is affected by Mineral Lease Nos. M4795, M4796, M4798, M4801, M4802, M4804 and M4805 and the leases are in good standing under *The Mines and Minerals Act*. These leases are held in the name of Inco Ltd, and this company retains the right to travel across the Land and to mine thereunder.
- 3.13 The Permittee acknowledges that the operation of the waste disposal site on the Land is governed by Operating Permit #N-02. Any expansion of the Land would require an Environment Act Licence which would require the filing of a proposal for a Class 2 development.
- 3.14 The Permittee acknowledges that a Manitoba Telephone System fibre optic cable is situated within the Hydro Right-of-Way paralleling Provincial Trunk Highway #6 or immediately adjacent to that Hydro faciltiy. The Permittee understands and agrees to contact the Manitoba Telephone System before any excavation occurs near this area.

4.00 MAINTENANCE OF LAND

- 4.01 The Permittee agrees:
 - a) to keep the Land, and all buildings and structures thereon, in a clean and sanitary condition free from inflammable materials, other than those contained in containers approved by the Canadian Standards Association;
 - b) to comply with all federal, provincial and municipal by-laws, Acts and regulations relating to the Permittee and/or the Land including, but not limited to, *The Crown Lands Act* and Regulations, *The Dangerous Goods Handling and Transportation Act* and Regulations and *The Environment Act* and Regulations, all as amended, replaced or substituted from time to time;
 - c) not to commit waste or damage the Land;
 - d) to keep the Land, and all buildings and structures thereon, in good and safe repair; and in a proper and neat condition and to repair in accordance with any notice from Manitoba;
 - e) to allow a person or persons on behalf of Manitoba to enter the Land, including all buildings and structures, at all reasonable times to examine the state of repair;
 - f) not to cut or remove any trees without prior written consent of Manitoba
 - g) any shoreline development to be minimal on Crown land adjacent to lakes or rivers and limited only to facilities or uses approved in writing by Manitoba. Natural vegetation and features should have minimal disturbance, and a vegetative riparian zone should be maintained or encouraged.
- 4.02 The Permittee shall not release upon the Land or any part thereof any Pollutants (as defined in paragraph 4.05), but if Permittee does release any Pollutants, the Permittee shall
 - a) at his/her expense, immediately give Manitoba notice of the release; remove the Pollutants from the Land in a manner which conforms with all laws and regulations covering the handling, removal and management of the Pollutants and as may be directed or ordered by an Environment Officer or Director of the Environmental Approvals Branch, or such successor as appropriate, as soon as reasonably practicable; and
 - b) obtain from an independent Qualified Environmental Consultant, a report verifying the complete and proper removal thereof from the Land, if requested by Manitoba, otherwise the Permittee shall report as to the extent and nature of any failure to comply with this Section.
- 4.03 Any Pollutants noted in paragraph 4.02 shall not become the property of Manitoba notwithstanding any rule of the law to the contrary (save and except where such Pollutants are brought or created upon the Land by Manitoba or its servants, employees or agents, and provided such person is not the Permittee or an officer, director, agent or employee of the Permittee). At the option of Manitoba, any substance contaminated by such Pollutants shall become the property of the Permittee and at the Permittee's expense, the Permittee or, at Manitoba's option, Manitoba, shall remove the contaminated substance from the Land and make good any damage done in so doing.
- 4.04 The Permittee shall indemnify and save harmless Manitoba from all costs or expenses, liabilities, losses, claims, damages (including consequential damages, interest, penalties, fines or monetary sanctions), legal costs or fees on a solicitor and own client basis, and fees or expenses of professional consultants incurred by Manitoba by reason of Pollutants being present on the Land and resulting from the Permittee's use or occupation of the Land or the breach of any warranty or covenant of the Permittee in this Section.

- 4.05 In this Section, "Pollutants" means any product, solid, liquid, gas, smoke, odour, waste, radiation or organism, or any combination of these, that is foreign to or in excess of the natural constituents of the environment on the Land and that:
 - a) has affected, is affecting or may affect the natural, physical, chemical or biological quality of the air, land and water; or
 - b) is, or is likely to be, injurious or damaging to the health or safety of a person(s), or injurious or damaging to property or to plant or animal life.

5.00 NO ASSIGNMENT OF PERMIT WITHOUT CONSENT

- 5.01 The Permittee shall not assign the Permit without the prior written consent of Manitoba, that consent not be unreasonably withheld. If the Permittee is a corporation, any change in ownership or control of the Permittee is deemed to be a proposed assignment.
- 5.02 Manitoba shall not unreasonably withhold consent to the assignment of the Permit for collateral (financing and security) purposes.
- 5.03 The Permittee shall submit an application on a form specified by Manitoba for approval to assign the Permit or any interest in the Permit.
- 5.04 Notwithstanding paragraphs 5.01 or 5.02, Manitoba may, in its sole discretion, refuse to assign the Permit if:
 - a) the Permittee has not paid any and all outstanding rent and taxes in respect of the Land and improvements, or
 - b) the proposed assignee is not eligible to hold a Permit in accordance with then current laws, regulations and policies of Manitoba.
- 5.05 The Permittee shall not sublet or rent out the Land.
- 5.06 The Permit shall be binding upon the executors, administrators, heirs, successors and any permitted assigns of the Permittee.

6.00 RESPONSIBILITY AND INSURANCE

- 6.01 Nothing contained in the Permit shall create any liability on the part of Manitoba or Manitoba Hydro for any damages caused or purported to be caused in respect to the Land by raising or lowering waters bordering upon or adjacent to the Land.
- 6.02 The Permittee shall use due care in the occupation of the Land to ensure that no person is injured, no property is damaged or lost and no rights are infringed.
- 6.03 The Permittee shall be solely responsible for and indemnify and save harmless Manitoba, its officers, employees and agents from and against all claims, liabilities and demands with respect to:
 - a) any injury to persons (including death), damage or loss to property caused by, or related to the occupation of the Land or the performance of the Permit or the breach of any term or condition of the Permit by the Permittee, any agent, invitee, officer, director or employee of the Permittee or any other person authorized by the Permittee to occupy the Land, and
 - any omission or wrongful or negligent act of the Permittee, any agent, invitee, officer, director or employee of the Permittee or of any other person authorized by the Permittee to occupy the Land;
 - unless such claims, liabilities, and demands arise out of the acts or omissions of Manitoba, its officers, employees or agents, and provided such person is not the Permittee or an officer, director, agent or employee of the Permittee.
- It is the responsibility of the Permittee to discuss his/her insurance requirements with his/her insurance adviser/broker and to arrange for his/her own insurance coverage(s). However, at a minimum, the Permittee shall purchase and maintain comprehensive general liability insurance with a minimum limit of \$1,000,000 per occurrence or claim. Manitoba reserves the right to require the Permittee to purchase and maintain a different minimum amount of liability insurance as specified by Manitoba from time to time by providing at least 180 days notice in writing of the change in the minimum amount to the Permittee. Evidence of insurance in the form of a Certificate of Insurance shall be provided by the Permittee upon request.

- 6.05 Notwithstanding paragraph 6.03, the Permittee agrees that any buildings, including any buildings existing at the issuance of the Permit, on the Land shall be maintained entirely at the Permittee's own risk, and the Permittee agrees to assume full responsibility for any damage or injury to persons or property situated on the Land resulting from flooding, erosion, ice damage, or temporary or permanent loss of Land accessibility. The Permittee agrees not to institute any action or make any claim against Manitoba or any employee or agent of Manitoba, including Manitoba Hydro, in respect to any personal injury caused by or related to flooding, whether or not the damage was occasioned by flooding resulting from the regulation or control of the adjacent waterway by Manitoba or Manitoba Hydro.
- 6.06 Notwithstanding paragraph 6.03, the Permittee agrees to indemnify and save harmless Manitoba and all employees and agents of Manitoba, including Manitoba Hydro, from and against all claims, liabilities and demands in respect of any damage to property or injury to persons located on the Land, which has been caused by flooding, erosion, ice damage, or temporary or permanent loss to Land accessibility.
- 6.07 The Permittee agrees not to institute any action or make any claim against the local government authority with respect to damage to any building or personal property or any injury to persons located on the Land that may be caused by flooding, erosion, ice damage, or temporary or permanent loss of land accessibility, as described herein and the Permittee agrees to enter into a written Agreement with the local government authority if the local government authority deems it necessary.

7.00 TERMINATION AND EXTENSION

- 7.01 The Permittee acknowledges that the Permit does not operate to prevent the sale or lease of the Land at any time during its term and is subject to the condition that Manitoba may give the Permittee notice of the cancellation thereof; and at the expiration of 30 days from the service of the notice, the Permit shall be cancelled.
- 7.02 Subject to 7.01 and provided that there has been no uncured default by the Permittee, including payment of rent, Manitoba may, in its discretion, automatically renew the Permit for a 1 year term on an annual basis and in accordance with then current laws, regulations or policies respecting rental rates and rental property of this type, unless otherwise notified by the Permittee.
- 7.03 Without restricting any other remedies available, Manitoba may, at its sole option, immediately terminate the Permit in writing if:
 - the Permittee has failed to make any payment due hereunder, has misrepresented any fact on the application for the Crown Land Permit, or has failed to comply with anyterm or condition of the Permit and has not remedied that failure to comply within 30 days of receipt of notice in writing from Manitoba;
 - b) the Permittee makes an assignment for the benefit of creditors, becomes bankrupt or insolvent, takes the benefit of, or becomes subject to, any statutes that may be in force relating to bankrupt or insolvent debtors (the appointment of a receiver or receiver and manager of the assets of the Permittee being conclusive evidence of insolvency), or if any certificate or order is made or granted for the winding-up or dissolution of the Permittee, voluntarily or otherwise;
 - c) the Permittee suffers a lien under *The Builders' Lien Act* (Manitoba) or any similar or successor legislation registered against the Land or Manitoba's interest therein and does not contest the validity or the amount of the lien and do all things necessary to obtain and register a discharge forthwith after the lien has come to the notice of the Permittee.
- 7.04 Where the Permittee terminates the Permit under paragraph 7.02 or Manitoba terminates the Permit in accordance with paragraph 7.01 or 7.03, or upon the expiration of the term or any renewal term of the Permit:
 - a) the Permittee shall deliver up possession of the Land to Manitoba and shall not remain in possession of the Land following the date of expiration or termination of the Permit; and
 - b) at the option of Manitoba:
 - (i) the Permittee and Manitoba may agree on the fair market value of the buildings or structures added to the Land by the Permittee and Manitoba may purchase such buildings or structures by paying to the Permittee that fair market value. If they fail to reach an agreement regarding the fair market value within 180 days of notice of termination being given by Manitoba, such value shall be determined by reference to the Land Value Appraisal Commission, or such other body as may hereafter be substituted therefor from time to time, or

- (ii) the Permittee shall remove all buildings and structures added to the Land by he Permittee within six months of such expiry or termination, or such other term as agreed to by Manitoba, and where those buildings and structures are not removed within six months or the term agreed to by Manitoba, they shall become the property of Manitoba. At the end of such six months or term agreed to by Manitoba, any assets left on the property as at such date shall vest in Manitoba, and the Permittee shall be deemed to have released and quit-claimed any interest therein to and in favour of Manitoba. No compensation or payment whatsoever shall be payable therefor by Manitoba to the Permittee in such event.
- 7.05 Where Manitoba terminates the Permit in accordance with paragraph 7.01 in instances where the Permittee is entering into a purchase or lease Agreement in respect of the Landwith Manitoba, all buildings and structures added to the Land by the Permittee shall be dealt with in accordance with the terms of that Agreement.
- 7.06 Where Manitoba terminates the Permit in accordance with paragraph 7.01 and 7.03 in instances where collateral assignments are recorded, it shall provide notice in writing of such termination to the holder of such collateral assignments (the "Security Holder"). The Security Holder:
 - a) shall then be allowed a reasonable time frame of not less than 30 days as stipulated in the notice, to cure defaults of the Permittee, and upon doing so the Permit shall be deemed not to have terminated;
 - b) shall not be obligated to go into possession; and
 - c) shall be allowed to assign the Permittee's interest in the Permit to a third party purchaser, subject to the prior written consent of Manitoba being required, but which shall not be unreasonably withheld; provided that as a condition of any such assignment, such subsequent assignee shall execute such documentation as Manitoba considers reasonable to bind the assignee directly to Manitoba on the terms and conditions as contained in the Permit, and all defaults of the Permittee shall be cured and brought to good standing. In the event of such permitted assignment, the Permit shall be deemed not to have terminated.

8.00 ENTIRE PERMIT

- 8.01 The Permit, including this Schedule and any Standard Conditions attached to the Permit, constitutes the entire Permit. There are no undertakings, representations, warranties, covenants, guarantees, agreements or promises, express or implied, verbal or otherwise, other than those contained in the Permit.
- 8.02 No amendment or change to, or modification of, the Permit shall be valid unless it is in writing.

9.00 APPLICABLE LAW

9.01 The Permit shall be governed by, interpreted, performed and enforced in accordance with the laws of Manitoba.

10.00 NOTICES

- 10.01 Any notice or other communication to Manitoba under the Permit shall be in writing and shall be delivered or sent by mail, postage prepaid to: Manitoba Conservation, Lands Branch, Attention: Director, Box 20,000, 123 Main Street West, Neepawa, Mb., R0J 1H0.
- 10.02 Any notice or other communication to the Permittee under the Permit shall be in writing and shall be delivered personally to the Permittee or an officer, director or employee of the Permittee or sent by mail, postage prepaid, to: Box 730, Thompson, Mb., R8N 1N5.
- Any notice or communication sent by mail shall be deemed to have been received on the third business day following the date of mailing. If mail service is disrupted by labour controversy, notice shall be delivered personally.
- 10.04 Either party may provide notice of change of address to the other in writing and thereafter all notices or communications shall be provided to the new address.
- 10.05 Any notice or other communication signed by any employee, officer or minister of Manitoba acting in that capacity shall be deemed for the purposes of the Permit to be a notice or other communication executed by Manitoba.
- 10.06 Notwithstanding paragraphs 10.02 and 10.03 any written notice to be served or given by Manitoba to the Permittee under the Permit shall be effectively given or served by posting the same in a conspicuous place on the Land.

11.00 ADDITIONAL PROVISIONS

11.01 Time shall be of the essence of the Permit.

- 11.02 If any provision of the Permit is illegal or invalid or unenforceable at law it shall be deemed to be severed from the Permit and the remaining provisions shall nevertheless continue to be in full force and effect.
- 11.03 No waiver of any default under the Permit shall be binding unless acknowledged in writing by Manitoba. Any condoning, excusing or overlooking by Manitoba of any default shall not operate as a waiver of Manitoba's rights hereunder in respect of any subsequent default.
- 11.04 All headings in this Schedule are inserted for convenience of reference only and will not affect the construction and interpretation of the Permit.
- 11.05 If this Permit is issued to two or more persons as Permittee, the liability of each to pay rent and taxes and to perform all other obligations hereunder shall be joint and several. If the Permittee is a corporation, each person acknowledging the terms of the Permit on behalf of the Permittee by so signing hereby agrees to guarantee to Manitoba the performance by the Permittee of all obligations of the Permittee hereunder, and each such person shall be jointly and severally liable with the Permittee as Permittee hereunder.
- 11.06 If the Permittee remains in possession of the Land after the termination of the Permit and Manitoba accepts rent, the tenancy, in the absence of written Agreement, will be from month to month only and shall be subject to all terms of the Permit, including rent, except that the tenancy shall be from month to month.
- 11.07 The Permittee shall not be entitled to file a caveat against title to the Land respecting the Permit under *The Real Property Act* (Manitoba) as it may be amended, replaced or substituted from time to time.
- 11.08 Sections 4 and 6 shall survive the termination or expiration of the Permit

THE PERMITTEE or the Permittee's duly authorized representative, on the dates noted below, acknowledges that he/she has read and understands all the terms and conditions of the Permit and agrees to be bound by same.

WITNESS SIGNED IN THE PRESENCE OF	PERMITTEE Local Government District of Mystery Lake
Print Name of Witness	Name of Permittee
Signature of Witness	Signature of Permittee
DATE:	DATE:

Appendix B Site Photographs



Photo 1 - View of poorly drained portions of contaminated soils area.



Photo 2 - View south of ponded water on west side of waste disposal facility.



Photo 3 - View south of ponded water on north side of waste disposal facility.





Photo 5 - View south of active garbage disposal area. Note the absence of containment berms.



Photo 6 - View west of the north edge of the active garbage disposal area. Note the absence of containment berms.



Photo 7 - View of blown litter along the northern perimeter of the waste disposal facility.



Photo 8 - View of blown litter along the eastern perimeter of the waste disposal facility.



Photo 9 - View of blown litter along the western perimeter of the waste disposal facility.



Photo 10 - View of clay and vegetation covered former waste area.



Photo 11 - View of aboveground petroleum storage tanks in operations area.



Photo 12 - View of unburied plastic bags containing asbestos material within the asbestos material collection area.



Photo 13 - View of sludge pile in the asbestos material collection area.



Photo 14 - View of pond of water adjacent to the sludge pile in the asbestos material collection area.



Photo 15 - View of used oil filter/container Eco-Centre near the entrance to the waste disposal facility.



Photo 16 - View of used tire and metals stockpiles at southeast end of the waste disposal facility.



Photo 17 – View of a former waste disposal area overlooking the marsh located southwest of the waste disposal facility.



Photo 18 – View West- The burning area at the west end of the waste disposal facility is visible.



Photo 19 - View Southwest - The burning area at the west end of the waste disposal facility is visible.



Photo 20 - View North - The operator's shed, bulldozer garage, used oil filter/container Eco-Centre, two sheds and an abandoned trailer area are visible in the operations area.



Photo 21 – View South - The recycling depot and a metals stockpile in the operations area are visible.



Photo 22 - View North - Overall view of the north end of the waste disposal facility. The burning area and a portion of the former waste disposal areas are visible.



Photo 23 – View North - The active area at the north end of the waste disposal facility is visible.

Appendix C Test Hole Logs

PROJECT: Engin	eering Assessment Stud	y for a WDF CLIEN	IT: Manitoba Water Se	rvices Bo	oard						NO: MW401	
	ting LGD of Mystery Lake		ty, Thompson, MB								NO.: 0326 060 00 02	
CONTRACTOR:	Paddock Drilling Ltd.		OD: 127 mm solid ster								N (m): 226.76	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	■BU						COVE		
BACKFILL TYPE	BENTONITE	.∵GRAVEL		GR	OUT				CUTTII	NGS	SAND	1
DEPTH (m)		SOIL DESCRIP	TION		SAMPLE TYPE	SAMPLE #	⊗\	Vapour F (ppr	n)		COMMENTS	ELEVATION (m)
1	CLAY - silty, brown, moist, firm, hig CLAY AND SILT - silty, brown, moist, firm, hig plastic clay lenses, 5 mm in	h plastic clay, varved with ec	qual amounts of pale brown,	low							Top of PVC Casing = 227.859 m	226 -
	SAND - some silt, brown, moist, de	nse, fine grained									Water Level = 225.12 m (05/11/21)	225 -
—4 ——4	REFUSAL AT 3.0 m											223 -
5												222
-6 												220
ENVIRONMENTAL EXISTING WOG SITE GPJ UMA GDT 317/06												219
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PROJECT: Engir	neering Assessment Study	y for a WDF CLIEN	T: Manitoba Wate	r Services B	oard			TESTH	OLE	NO: MW402	
LOCATION: Exis	ting LGD of Mystery Lake	Waste Disposal Facilit	y, Thompson, MB					PROJE	ECT N	IO.: 0326 060 00 02	
CONTRACTOR:	Paddock Drilling Ltd.	METH	OD: 127 mm solid	l stem auger	S			ELEVA	TION	l (m): 217.95	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOOI	v ⊟BI	JLK			☑NO REC	OVER	Y CORE	
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	Gl	ROUT	•	8	CUTTIN	GS	SAND	
DEPTH (m) SOIL SYMBOL	CLAY	SOIL DESCRIP	TION		SAMPLE TYPE	SAMPLE #		ur Reading ⊗ (ppm) 100 1000 : Î : Î	0	COMMENTS Top of PVC Casing =	ELEVATION (m)
1	- siity, brown, moist, firm, high	ı plastic								218.559 m Water Level = 217.08 m (05/11/21)	217
-2	- silty, brown, moist, firm, high plastic clay lenses, 5 mm in the - trace fine sand lenses between		ual amounts of pale br	own, low							216
-3 -3 -3 -3 -3 -3 -3 -3	SAND - some silt, brown, moist, dens	se, fine grained									215
-4 4	REFUSAL AT 3.8 m										214
- -5 - - - -											213
- -6 											212
7											211
8											210
											209
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	ering Assessment Study f		Γ: Manitoba Water S	ervices Bo	oard				E NO: MW403	
	ng LGD of Mystery Lake V								NO.: 0326 060 00 02	
	addock Drilling Ltd.		DD: 127 mm solid st			····			N (m): 207.88	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BU				RECOVE		
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	∏ GR	OUT			JTTINGS	SAND	T
DEPTH (m)	S	OIL DESCRIPT	ΓΙΟΝ		SAMPLE TYPE		Vapour Rea (ppm) 0 100	iding ⊗	COMMENTS	ELEVATION (m)
0	CLAY								Top of PVC Casing =	
	- silty, some silt inclusions, brow	n, moist, firm, high plastic							208.623 m Water Level = 208.073 m	
									(05/11/21)	
‡. ▮ *										207 -
F'										
	CLAY AND SILT - silty, brown, moist, firm, high p	lastic clay, varved with pale	e brown, low plastic clay	enses						
	•								1	
E_2										206 -
							<u>-</u>			
F ₋₃										205 -
	SILT AND CLAY - pale gray, very moist, clayey si	It. varved with silty, brown,	moist, firm, high plastic	clay			l			
	paid gray, rolly mains, and year	· · · · · · · · · · · · · · · · · · ·	, , ,	•						
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QON	UMA AECOM			IEWED BY					LETION DEPTH: 10.67 III	1
N N	UMA ALCOM			JECT ENG		: Peter l	Bohonos			1 of 2

PROJ	ECT:	Engin	eering Assessment Stud		: Manitoba Wate		oard): MW403	
LOCA	TION:	Exis	ting LGD of Mystery Lak	ke Waste Disposal Facility	, Thompson, MB						: 0326 060 00 02	
CONT	RACT	OR:	Paddock Drilling Ltd.	METHO	D: 127 mm solic	d stem augers	AND ADDRESS OF THE PARTY OF THE				n): 207.88	
SAME	LE TY	PΕ	GRAB	SHELBY TUBE	SPLIT SP00				E	COVERY	CORE	
BACK	FILL T	YPE	BENTONITE	GRAVEL	SLOUGH	GR	OUT		CUTTII	NGS	SAND	
DEPTH (m)	SLOTTED PIEZOMETER			SOIL DESCRIPT	TION		SAMPLE TYPE	** CAMPLE #	Vapour Reading (ppm) 0 100 10	⊗	COMMENTS	ELEVATION (m)
- 10 - - - - - - - - - - - - - - - - - - -			END OF HOLE AT 10.7 m I	IN SILT AND CLAY								197
-12 -												196
-13 13 												195 —
15												193 -
-16 -16 												192 -
												190 -
ENVIRONMENTAL EXISTING WAGES ALE GET OWN. GET OF THE COLOR OF THE COLO												189 -
<u> 20</u>		-				LOGGED BY:	ED	1,,,,,,			ON DEPTH: 10.67 r	
Ş			UMA AECOM	И		REVIEWED BY	Y: PB		(ON DATE: 4/10/05	
2			mark 3 " N.C. p			PROJECT EN	GINE	R: Peter	Bohonos		Page	2 of 2

PROJECT: Engineering Assessment Study for a W	***************************************	Manitoba Wate	r Services B	Board	<u> </u>): MW405	
LOCATION: Existing LGD of Mystery Lake Waste D							F	PROJE	ECT NO.	: 0326 060 00 0	2
CONTRACTOR: Paddock Drilling Ltd.	METHOD): 127 mm solid	and the second s	s	······································	*************	1	ELEVA	TION (m	n): 211.47	
SAMPLE TYPE GRAB SI	HELBY TUBE	SPLIT SPOON					E		OVERY	CORE	****
BACKFILL TYPE BENTONITE G	RAVEL	SLOUGH	G	ROU	T			CUTTING	GS	SAND	
SOIL I	DESCRIPTI	ON		SAMPLE TYPE	SAMPLE #	⊗\	(ppn			COMMENTS	ELEVATION (m)
CLAY (Fill) - silty, brown, moist, soft, medium plastic	;								: Top	of PVC Casing = .411 m	211
CLAY AND ORGANICS - some silt, black, moist, soft, low plastic CLAY AND SILT - silty, brown, moist, firm, high plastic cla		rown, low plastic cla	y lenses							ter Level = 210.511 i /11/21)	m 210
SILT AND CLAY	d with all to be a second	aint from high att	io do:								209
- pale gray, very moist, clayey silt, varved	d with silty, brown, m	oist, firm, high plast	ic clay								208
-6											206
END OF HOLE AT 7.6 m IN SILT AND C	LAY										203
uma AECOM		RI	OGGED BY: EVIEWED BY ROJECT ENC	/: PE		eter Bo	ohonos	CON		N DEPTH: 7.62 m N DATE: 4/10/05 Page	e 1 of

ſ	PROJ	ECT:	Engir	neering Assessment Study fo	or a WDF CLIEN	T: Manitoba Wa	ter Services Bo	oard			TESTHOLE	E NO: MW406	
Ì	LOCA	TION	Exis	ting LGD of Mystery Lake W	aste Disposal Facilit	y, Thompson, MI	3				PROJECT	NO.: 0326 060 00 02	
				Paddock Drilling Ltd.		OD: 127 mm sol		S			ELEVATIO	N (m): 213.68	
Ì	SAMP	LE T	/PE	GRAB	SHELBY TUBE	SPLIT SPO					NO RECOVE	RY CORE	-
Ī	BACKI	FILL	ГҮРЕ	BENTONITE	GRAVEL	∭SLOUGH	€GF	ROUT		\square	CUTTINGS	SAND	
-	DEPTH (m)	F	SOIL SYMBOL	SO	OIL DESCRIP	TION		SAMPLE TYPE	SAMPLE #	(pr	Reading ⊗ om) 00 1000	COMMENTS	ELEVATION (m)
	- 0 			CLAY - silty, brown, moist, firm, high pla	astic							Top of PVC Casing = 214.583 m	213 —
	- - - - - - 2			CLAY AND SILT - silty, brown, moist, firm, high pla	astic clay, varved with pal	le brown, low plastic	clay lenses					Water Level = 211.333 m	212 -
	- - -3											(05/11/21)	211
	- - - 4			SILT AND CLAY	1 70 - 70 - 10 - 10 - 10 - 10	and the state of							210
	- - - - - - - - 5			- pale gray, very moist, clayey sill	, varved with silty, brown	, moist, firm, high pla	stic clay						209 —
	-6												208 -
7/06	-7 -7												207
ITE.GPJ UMA.GDT 3/1	-8			END OF HOLE AT 7.6 m IN SILT	AND CLAY		:						206
ENVIRONMENTAL EXISTING WDG SITE.GPJ UMA.GDT 3/17/06	-9 9 												204 —
ENVIRONME			<u> </u>	UMA AECOM			LOGGED BY: I REVIEWED BY PROJECT ENG	: PB	R: Pe	ter Bohono	COMPL	ETION DEPTH: 7.62 m ETION DATE: 5/10/05 Page	1 of 1

	ineering Assessment Stud		CLIENT: Manitoba W	·····	Board	<u></u>		1	restholi	E NO: MW407	
	isting LGD of Mystery Lak				***************************************					NO.: 0326 060 00	02
	: Paddock Drilling Ltd.		METHOD: 127 mm s					-	Andrew Commencer and the Commencer of th	N (m): 218.28	************
SAMPLE TYPE	GRAB	SHELBY TU						*******	NO RECOVE		
BACKFILL TYPI	BENTONITE	GRAVEL	∭SLOUGH	∷ G	ROU	T	,		CUTTINGS	SAND	
DEPTH (m)	CLAY	SOIL DESC	RIPTION		SAMPLE TYPE	SAMPLE#	⊗ V 10	apour Ri (ppm 100		COMMENTS Top of PVC Casing =	
-1 -2 -3 -4 -4	- silty, brown, moist, firm, hig CLAY AND SILT - silty, brown, moist, firm, hig SAND - some silt, moist, dense, fine	nh plastic clay, varved v	with pale brown, low plast	c clay lenses						219.088 m	2 2 2 2 2 2
-6	REFUSAL AT 7.3 m										2 2 20
10	UMA AECOM			LOGGED BY: E	: PB					TION DEPTH: 7.32 m TION DATE: 4/10/05	
	ŧ			PROJECT ENG	INEE	R: P	eter Boh	onos		Page	9 1 (

CLAY (Fiti) - silly, brown, moist, stiff, high plastic - silly, brown, moist, stiff, high plastic clay, varved with equal amounts of pale brown, low plastic day tensors, 5 mm in thickness - some medium grained sand - REFUSAL AT 4.0 m	PROJECT:	Engineering Assessment Stud	ly for a WDF CL	IENT: Manitoba W	ater Services B	oard	1		ESTHOLE	NO: TH401A	
SAMPLE TYPE GRAB SOIL DESCRIPTION SOIL DESCRIPTION CLAY (Fill) - sity, brown, most, stiff, high plastic CLAY (Fill) - sity, brown, most, stiff, high plastic CLAY SAS SAT -	LOCATION	: Existing LGD of Mystery Lake	e Waste Disposal Fa	cility, Thompson, f	ИΒ			F	ROJECT	NO.: 0326 060 00 02	2
SOIL DESCRIPTION CLAY [FII]	CONTRAC	TOR: Paddock Drilling Ltd.									VV
CLAY (Fill) - silly, trown, most, silf, high plastic CLAY AND SILTsilly, trown, most, firm, high plastic day, varved with equal amounts of pale brown, few plastic day lenses, 5 mm in thickness REFUSAL AT 4 C m LOGGED BY: ED COMPLETION DEPTH: 3.56 m LUMA AECOMI REVIEWED BY: PB COMPLETION DEPTH: 3.56 m	SAMPLE T	YPE GRAB	∭SHELBY TUBI	SPLIT SP	DON BR	JLK			O RECOVE	RY CORE	
CLAY (Fill) - stilly, brown, moist, stilf, high plastic CLAY AND SILT - stilly, brown, moist, firm, high plastic city, varved with equal amounts of pale brown, low plastic city lenses, 5 mm in thickness - some medium grained sand - some medium grained sand REFUSAL AT 4.0 m LOGSED BY: ED COMPLETION DEPTH: 3.96 m REVIEWED BY: FB COMPLETION DEPTH: 3.96 m	DEPTH (m) SOIL SYMBOL	S	OIL DESCRIF	TION		SAMPLE TYPE	SAMPLE #	(ppm)	COMMENTS	DEDTH (m)
LOGGED BY: ED COMPLETION DEPTH: 3.96 m UMA AECOM REVIEWED BY: PB COMPLETION DATE: 4/10/05	-1 -2 -3 -4 -5 -6 -7	- silty, brown, moist, stiff, high plastic CLAY AND SILT - silty, brown, moist, firm, high plastic lenses, 5 mm in thickness - some medium grained sand		amounts of pale brown	n, low plastic clay						5 6 7 7 8 8 9
	10	UMA AECOM			REVIEWED BY:	PB				TION DATE: 4/10/05	

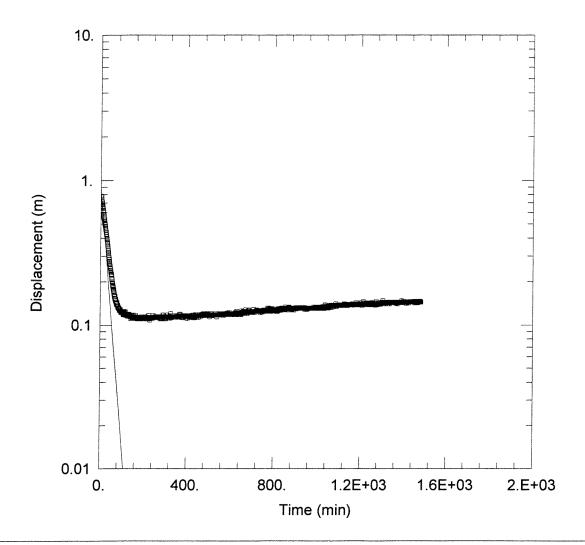
PROJ	ECT:	Engineering Assessment Study for a WDF	es Boar	ď	Т	ESTHOLE	NO: TH403A	**************************************
LOCA	TION	: Existing LGD of Mystery Lake Waste Disposal Facility, Thompson, MB			Р	ROJECT	NO.: 0326 060 00 02	
		TOR: Paddock Drilling Ltd. METHOD: 127 mm solid stem a				LEVATIO		
SAMP	LE T	YPE GRAB SHELBY TUBE SPLIT SPOON	BULK		N	O RECOVE	RY CORE	
DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	⊗Vapour Re (ppm) 10 100	ading⊗ 1000	COMMENTS	DEPTH (m)
ENVIRONMENTAL EXISTING WDG SITE.GPJ UMA.GDT 3/17/06 C		CLAY (Fill) - silty, brown, moist, soft, high plastic - some garbage GARBAGE CLAY AND SILT - silty, brown, moist, firm, high plastic clay, varved with pale brown, low plastic clay lenses END OF HOLE AT 4.3 m IN CLAY						3- 3- 3- 3-
ENVIRONME	I.	UMA AECOM LOGGED E REVIEWED PROJECT	BY: PE		Peter Bohonos		TION DEPTH: 4.27 m TION DATE: 4/10/05 Page	1 of 1

PRO	JECT: Eng	ineering Assessment Stu	•	NT: Manitoba Wa		oard	1			NO: TH408	
LOCA	ATION: Ex	isting LGD of Mystery Lak	e Waste Disposal Facili	ity, Thompson, M	В					O.: 0326 060 00 02	
		: Paddock Drilling Ltd.	METH	HOD: 127 mm so	lid stem augers				EVATION		
	PLE TYPE		SHELBY TUBE	SPLIT SPO	ON B BL	JLK		⊠ N(RECOVER'	Y CORE	
DEPTH (m)	SOIL SYMBOL	S	OIL DESCRIPT	ION		SAMPLE TYPE	SAMPLE#	⊗Vapour Re. (ppm) 10 100	ading ⊗	COMMENTS	DEPTH (m)
-3	- si	AY (Fill) Ity, dark brown, some metals an	d paper, moist, soft, high pla	stic				10 100	1000		3-
ENVIRONMENTAL EXISTING WING SHE, GP. UMA, GD. 3/7/08					LOGGED BY:	F.			COMPLE	TION DEPTH: 4.57 m	8 -
NVIKONIN		UMA AECOM			REVIEWED BY PROJECT ENG	r: Pl		Peter Bohonos		TION DATE: 4/10/05	1 of 1

PROJ	ECT:	Engineering Assessment Stu	•	Ր: Manitoba Water Տ	ervices Bo	ard				NO: TH409	
LOCA	TION:	Existing LGD of Mystery La	ce Waste Disposal Facility	, Thompson, MB						NO.: 0326 060 00 02	
		OR: Paddock Drilling Ltd.	METHO	DD: 127 mm solid st					ELEVATIO		
SAMP			SHELBY TUBE	SPLIT SPOON	■BU	LK	······································		NO RECOVE	RY CORE	т
ОЕРТН (m)	SOIL SYMBOL		SOIL DESCRIPTION	ON		SAMPLE TYPE	SAMPLE #	⊗ Vapour I (pp 10 10	m)	COMMENTS	DEPTH (m)
ENVIRONMENTAL, EXISTING WOG SITE GPJ. UMA GDT 3/17/06		CLAY (Fill) - silty, brown, moist, firm, high place GARBAGE CLAY (Fill) - silty, brown, moist, firm, high place GARBAGE CLAY AND SILT - silty, brown, moist, firm, high place END OF HOLE AT 7.6 m IN CLAY	stic	lenses				10 11	00 1000		1- 2- 3- 4- 5-
ENTAL EXISTING W											
RONME		UMA AECON	7	RE	GGED BY: I	: P			COMPL	LETION DEPTH: 7.62 m LETION DATE: 4/10/05	
N.		The second secon		PR	DJECT ENG	SINE	ER:	Peter Bohon	os	Page	1 of

PROJ	ECT:	Engineering Assessment Stu	idy for a WDF CL	IENT: Manitoba Wa		oard				NO: TH410			
LOCATION: Existing LGD of Mystery Lake Waste Disposal Facility, Thompson, MB								PROJECT NO.: 0326 060 00 02					
CONTRACTOR: Paddock Drilling Ltd. METHOD: 127 mm solid SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON									ELEVATION (m): NO RECOVERY CORE				
SAMP	LE T	YPE GRAB	∭ SHETRA LORE	: XISPLIT SPC	ON BRO	JLK 		∠ NO	RECOVE	Kr [II]CO	KE	Т	
DEPTH (m)	SOIL SYMBOL			SAMPLE TYPE	SAMPLE #	⊗Vapour Reac (ppm) 10 100	ling⊗ 1000	. СОММЕ	NTS	DEPTH (m)			
0 1 1 2 3 4 4 5 5 6 7 7 8 6 7 7 8 6 7 7 8 7 9 9 7 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		CLAY (Fill) - silty, brown, moist, firm, high place GARBAGE CLAY AND SILT - silty, brown, moist, firm, high place END OF HOLE AT 4.6 m IN CLAY	stic clay, varved with low p	lastic clay lenses								1 · · · · · · · · · · · · · · · · · · ·	
- - - 10		#			LOGGED BY: E					ETION DEPTH:			
						REVIEWED BY: PB				COMPLETION DATE: 4/10/05			
i						PROJECT ENGINEER: Peter Bohonos				Page 1 of			

Appendix D Hydrograph Plots



WELL TEST ANALYSIS

Data Set: P:\0326\060-00\4 Development\4 Test Results and Analysis\MW401.aqt

Date: 01/20/06 Time: 14:28:39

PROJECT INFORMATION

Company: UMA Engineering Ltd.

Client: City of Thompson Project: 326 060 00

Test Location: Thompson, MB

Test Well: MW401

Test Date: November 3, 2005

AQUIFER DATA

Saturated Thickness: 0.9 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW401)

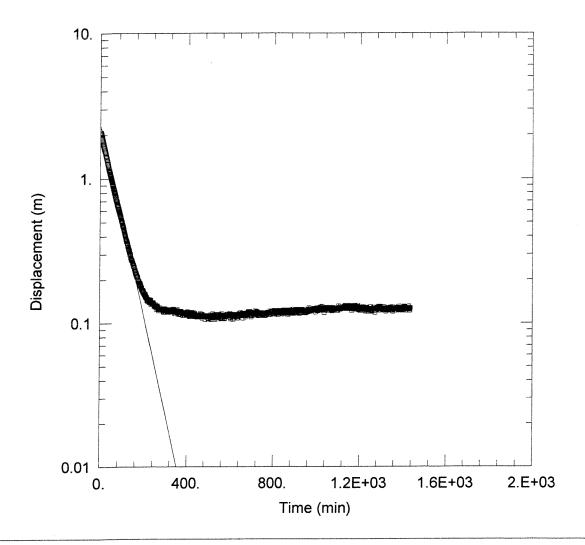
Initial Displacement: 0.78 m Casing Radius: 0.05 m Wellbore Radius: 0.075 m Well Skin Radius: 0.125 m

Screen Length: 1.5 m Total Well Penetration Depth: 1.45 m Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: <u>Unconfined</u> Solution Method: <u>Bouwer-Rice</u>

K = 0.000122 cm/sec y0 = 0.8268 m



WELL TEST ANALYSIS

Data Set: P:\0326\060-00\4 Development\4 Test Results and Analysis\MW402.aqt

Date: 01/20/06 Time: 14:29:17

PROJECT INFORMATION

Company: UMA Engineering Ltd

Client: City of Thompson Project: 326 060 00

Test Location: Thompson, MB

Test Well: MW402

Test Date: November 3, 2005

AQUIFER DATA

Saturated Thickness: 1.2 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW402)

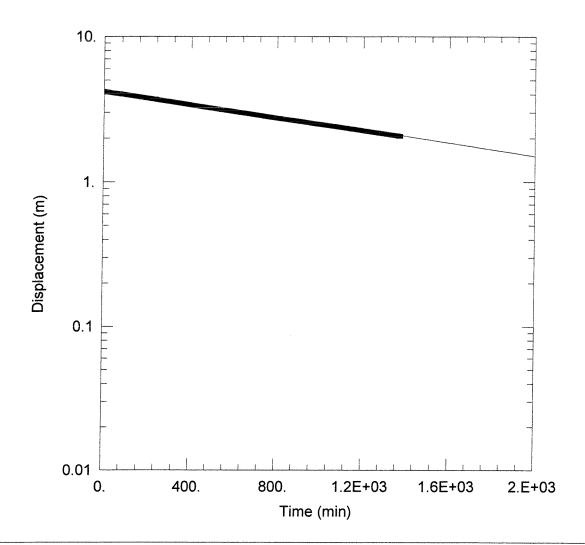
Initial Displacement: 2.08 m Casing Radius: 0.05 m Wellbore Radius: 0.075 m Well Skin Radius: 0.125 m

Screen Length: 1.5 m Total Well Penetration Depth: 1.2 m Gravel Pack Porosity: 0.3

SOLUTION

Aguifer Model: Unconfined Solution Method: Bouwer-Rice

K = 4.452E-05 cm/sec y0 = 2.311 m



WELL TEST ANALYSIS

Data Set: P:\0326\060-00\4 Development\4 Test Results and Analysis\MW403.agt

Date: 01/20/06 Time: 14:29:59

PROJECT INFORMATION

Company: UMA Engineering Ltd.

Client: City of Thompson Project: 0326 060 00

Test Location: Thompson, MB

Test Well: MW403

Test Date: November 3, 2005

AQUIFER DATA

Saturated Thickness: 11.05 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW403)

Initial Displacement: 4.18 m

Wellbore Radius: 0.075 m

Casing Radius: 0.05 m

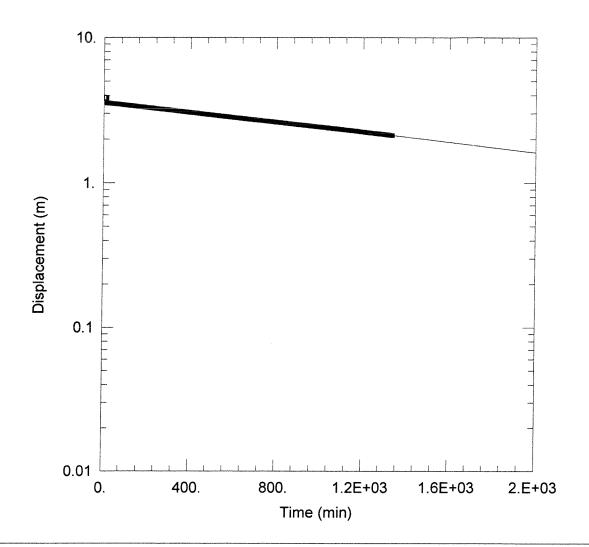
Well Skin Radius: 0.125 m

Screen Length: 1.5 m Total Well Penetration Depth: 1.5 m Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined Solution Method: Bouwer-Rice

K = 1.315E-06 cm/sec y0 = 4.313 m



WELL TEST ANALYSIS

Data Set: P:\0326\060-00\4 Development\4 Test Results and Analysis\MW405.agt

Date: 01/20/06 Time: 14:30:23

PROJECT INFORMATION

Company: UMA Engineering Ltd.

Client: City of Thompson Project: 0326 060 00

Test Location: Thompson, MB

Test Well: MW405

Test Date: November 3, 2005

AQUIFER DATA

Saturated Thickness: 6.64 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW405)

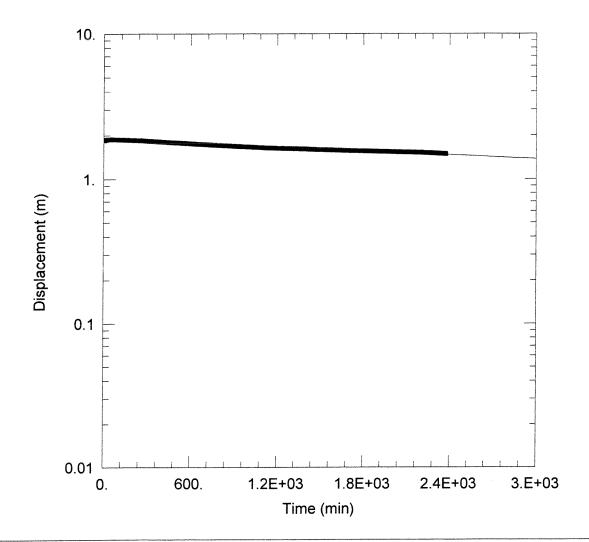
Initial Displacement: 3.87 m Casing Radius: 0.05 m
Wellbore Radius: 0.075 m Well Skin Radius: 0.125 m

Screen Length: 1.5 m Total Well Penetration Depth: 1.5 m Gravel Pack Porosity: 0.3

SOLUTION

Aquifer Model: Unconfined Solution Method: Bouwer-Rice

K = 1.048E-06 cm/sec y0 = 3.683 m



WELL TEST ANALYSIS

Data Set: P:\0326\060-00\4 Development\4 Test Results and Analysis\MW406.aqt

Date: 01/20/06 Time: 14:30:54

PROJECT INFORMATION

Company: UMA Engineering Ltd.

Client: City of Thompson Project: 0326 060 00

Test Location: Thompson, MB

Test Well: MW406

Test Date: November 2, 2005

AQUIFER DATA

Anisotropy Ratio (Kz/Kr): 1. Saturated Thickness: 5.24 m

WELL DATA (MW406)

Casing Radius: 0.05 m Initial Displacement: 1.85 m Well Skin Radius: 0.125 m Wellbore Radius: 0.075 m

Total Well Penetration Depth: 1.5 m Screen Length: 1.5 m Gravel Pack Porosity: 0.3

SOLUTION

Solution Method: Bouwer-Rice Aquifer Model: Unconfined

y0 = 1.918 mK = 2.842E-07 cm/sec

Appendix E Laboratory Data

Table 1. Summary of Analytical Results - November 2005 Existing Waste Disposal Facility - Local Government District of Mystery Lake

		CCME	MW401	MW402	MW403	MVV405	MW406
Parameter	MDL	Guidelines					
		Community Water	05/11/04	05/11/04	05/11/04	05/11/04	05/11/04
Trace Organincs		,	_				
Benzene	0.0005	0.005		< 0.0005	< 0.0005	< 0.0005	< 0.0005
Toluene	0.0005	0.024	•	< 0.0005	< 0.0005	< 0.0005	< 0.0005
Ethylbenzene Xylenes	0.0005	0.0024	-	< 0.0005 < 0.0005	< 0.0005 < 0.0005	< 0.0005 < 0.0005	< 0.0005 < 0.0005
TVH	0.0000		<u> </u>	< 0.1	< 0.1	< 0.1	< 0.1
TEH	0.1		•	< 0.1	< 0.1	< 0.1	< 0.1
Inorganics							
Alkalinity - Total (as CaCO ₃)	1		597	469	521	505	106
Ammonia (NH ₃)	0.01	-		0.06	0.64	0.05	0.06
Bicarbonate (HCO ₃) Carbonate (CO ₃)	0.6		728	572	636	617	129
Chemical Oxygen Demand	8		< 0.6	< 0.6 < 8	< 0.6 < 8	< 0.6	< 0.6 < 8
Chloride	9	250*	< 9	26	33	21	20
Conductivity	0.4	_	1330	1050	1790	1830	316
Cyanide - Free	0.01	0.2	-	< 0.01	< 0.01	< 0.01	< 0.01
Hardness (as CaCO ₃)	0.2	-	858	516	432	590	76.7
Hydroxide (OH)	0.4		< 0.4	< 0.4	< 0.4	< 0.4	< 0.4
Kjeldahl Nitrogen - Total	0.2			< 0.2	0.8	0.2	0.3
Nitrate+Nitrite-N pH	0.01	6.5-8.5*	0.50	1.46	0.32	0.01	0.15
Phospohrus - Total	0.01	0.5-8.5	7.32	7.41 0.032	7.80 0.145	7.65 0.148	8.11 0.052
Sulphate	9	500*	241	92	481	9	27
Turbidity	0.05	1	-	70	190	190	8.7
Total Dissolved Solids	5	500*	921	660	1300	1300	190
Total Solids	5		-	870	1600	1600	210
Total Suspended Solids	5			180	300	200	14
Metals (Total)		1	F				
Aluminum	0.02 0.001	0.1 0.006	0.47	0.14	0.29	0.49	0.24
Antimony Arsenic	0.0005	0.006	< 0.001 < 0.0005	< 0.001 < 0.0005	< 0.001 0.0054	< 0.001 0.0016	0.001 < 0.0005
Barium	0.0003	1	0.115	0.0889	0.0755	0.115	0.0121
Beryllium	0.001		< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
Bismuth	0.0001	**	< 0.0001	< 0.0001	< 0.0001	< 0.0001	< 0.0001
Boron	0.03	5	< 0.03	0.15	0.23	0.05	< 0.03
Cadmium	0.0002	0.005	0.0008	0.0021	0.0002	0.0019	0.0012
Calcium	0.1		245	121	90.6	147	23.1
Cesium Chromium	0.0001 0.001	0.05	< 0.0001 0.004	< 0.0001 0.006	< 0.0001 0.002	< 0.0001 0.002	< 0.0001
Cobalt	0.0002	0.05	0.004	0.0004	0.002	0.0009	0.001 0.0004
Copper	0.001	1*	0.012	0.004	0.007	0.0003	0.010
Iron	0.05	0.3*	0.61	0.18	0.41	0.63	0.23
Lead	0.0005	0.01	0.0048	0.0041	0.0011	0.0017	0.0014
Lithium	0.01		0.02	0.02	0.05	0.03	< 0.01
Magnesium	0.01		60.0	52.1	49.9	54.2	4.61
Manganese Molybdenum	0.0003	0.05*	0.0341 < 0.0002	0.0110	0.384	0.143	0.0346
Nickel				0.0012	0.0119	0.0077	< 0.0002
Phosphorus	0.002		0.041 0.15	0.015 0.11	0.005 0.14	0.048 0.13	0.010 0.10
Potassium	0.1		1.3	3.8	8.1	4.2	1.2
Rubidium	0.0002		0.0022	0.0008	0.0033	0.0030	0.0010
Selenium	0.001	0.01	0.004	0.004	0.006	0.012	0.003
Silver	0.001		< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
Sodium	0.03	200*	13.5	19.0	262	196	3.05
Strontium	0.0001 0.001		0.319	0.412	0.629	0.582	0.0389
Tellurium Thallium	0.0001		< 0.001 0.0001	< 0.001 < 0.0001	< 0.001 0.0001	< 0.001 < 0.0001	< 0.001 < 0.0001
Tin	0.0001	**	< 0.0001	0.0011	< 0.0001	0.0008	0.0047
Titanium	0.0009		0.0252	0.0097	0.0189	0.0222	0.0047
Tungsten	0.0002	-	< 0.0002	< 0.0002	< 0.0002	< 0.0002	< 0.0002
Uranium	0.0001	0.02	0.0041	0.0109	0.0161	0.0144	0.0001
Vanadium	0.001	_	0.002	< 0.001	0.004	0.002	< 0.001
Zinc	0.01	5*	0.05	0.02	0.02	0.04	0.17
Zirconium	0.0004		0.0015	0.0005	0.0012	0.0014	< 0.0004

- All units in mg/L expect the following (conductivity, umho/cm; pH, pH units; turbidity, NTU)

 1. Canadian Environmental Quality Guidelines, Canadian Council of Ministers of the Environment, (updated 2004).

 1. Canadian Environmental Quality Guidelines, Canadian Council of Ministers of the Environment, (updated 2004).

 1. Indicates concentration is less than the method detection limit (MDL).

 1. Bolded and shaded areas exceed CCME Community Water guideline.

 1. Indicates aesthetic objective only.

- indicates no guideline established
 indicates analysis not conducted

Table 2. QA/QC Results - November 2005 Existing Waste Disposal Facility - Local Government District of Mystery Lake

		MW403	MW99	RPD
Parameter	MDL			
7.7				
Alkalinity - Total (as CaCO ₃)		05/11/04	05/11/04	. 7
Bicarbonate (HCO ₃)	1	521	507	0.7
	2	636	618	0.7
Carbonate (CO ₃)	0.6	< 0.6	< 0.6	0.0
Chloride	9	33	34	0.7
Conductivity	0.4	1790	1790	0.0
Hardness (as CaCO ₃)	0.2	432	465	1.8
Hydroxide (OH)	0.4	< 0.4	< 0.4	0,0
Nitrate+Nitrite-N	0.01	0.32	0.31	0.8
pH	0.01	7.80	7.89	0.3
Sulphate	9	481	454	1.4
Total Dissolved Solids	5	1300	1230	1.4
Aluminum	0.02	0.29	0.92	26.0
Antimony	0.001	< 0.001	< 0.001	0.0
Arsenic	0.0005	0.0054	0.0055	0.5
Barium	0.0003	0.0755	0.083	2.4
Beryllium	0.001	< 0.001	< 0.001	0.0
Bismuth	0.0001	< 0.0001	< 0.0001	0.0
Boron	0.03	0.23	0.27	4.0
Cadmium	0.0002	0.0002	0.0411	49.5
Calcium	0.1	90.6	100	2.5
Cesium	0.0001	< 0.0001	0.0001	0.0
Chromium	0.001	0.002	0.003	10.0
Cobalt	0.0002	0.0012	0.0022	14.7
Copper	0.001	0.007	0.009	6.3
Iron	0.05	0.41	1.45	28.0
Lead	0.0005	0.0011	0.0035	26.1
Lithium	0.01	0,05	0.04	5.6
Magnesium	0.01	49.9	52.3	1.2
Manganese	0.0003	0.384	0.428	2.7
Molybdenum	0.0002	0.0119	0.0101	4.1
Nickel	0.002	0.005	0.015	25.0
Phosphorus	0.05	0.14	0.24	13.2
Potassium	0.1	8.1	8.3	0.6
Rubidium	0.0002	0.0033	0.0048	9.3
Selenium	0.001	0.006	0.004	10.0
Silver	0.001	< 0.001	< 0.001	0.0
Sodium	0.03	262	273	1.0
Strontium	0.0001	0.629	0.632	0.1
Tellurium	0.001	< 0.001	< 0.001	0.0
Thallium	0.0001	0.0001	< 0.0001	0.0
Tin	0.0006	< 0.0006	0.0009	0.0
Titanium	0.0009	0.0189	0.0533	23.8
Tungsten	0.0002	< 0.0002	< 0.0002	0.0
Uranium	0.0001	0.0161	0.0158	0.5
Vanadium	0.001	0.004	0.005	5.6
Zinc	0.01	0.02	0.03	10.0
Zirconium	0.0004	0.0012	0.002	12.5

Notes:
All units in mg/L expect the following (conductivity, umho/cm; pH, pH units; turbidity, NTU)
"RPD" indicates Relative Percent Difference.
"NA" indicates variability not availale as the sample concentration is not ten times the detection

limit.

Variability of duplicate samples with identical concentrations or below detection limits indicated as zero.



DATE:

17-NOV-05

ANALYTICAL REPORT

UMA ENGINEERING

ATTN: PETER BOHONOS

1479 BUFFALO PLACE WINNIPEG MB R3T 1L7

Lab Work Order #: L338009

Sampled By: MA

Date Received: 07-NOV-05

Project P.O. #:

Project Reference:

Comments: The portion of the sample for metals analysis was preserved by the client prior to submission.

APPROVED BY: Paul Necolas

PAUL NICOLAS

Project Manager

THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN AUTHORITY OF THE LABORATORY. ALL SAMPLES WILL BE DISPOSED OF AFTER 30 DAYS FOLLOWING ANALYSIS. PLEASE CONTACT THE LAB IF YOU REQUIRE ADDITIONAL SAMPLE STORAGE TIME.

Sample Details/Parameters	Result	Qualifie	er U.L	'Units	Extract	ed Analyze	d By	Bato
.338009-1 MW 401								
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								-
Routine Soluble + Metal scan			-					
pH								
PH	7.32		0.01	pH uni		00 100		
TDS calculated			0.01	pri di li	19	08-NOV-0	05 DX	N R3443
TDS (Calculated)	921		5	mg/L		10-NOV-0	.=	
Sulphate Soluble				mg/L		10-100-0	15	
Sulphate (SO4) - Soluble	241		9	mg/L		07-NOV-0	5 0	
Nitrate + Nitrite Soluble				5.2		0,-1000-0	5 CLI	M R3440
Nitrate+Nitrite-N	0.50	RAMB	0.01	mg/L		07-NOV-0	5 CLI	M R3440
Metal scan						07-110-0	CLI	vi 13440
Silver (Ag)-Total	<0.001		0.001	mg/L	09-NOV-	05 10-NOV-0	5 DAG	3 R3449
Aluminum (AI)-Total	0.47		0.02	mg/L		05 10-NOV-0		
Arsenic (As)-Total	<0.0005		0.0005		09-NOV-	05 10-NOV-0	5 DAG	
Boron (B)-Total	<0.03		0.03	mg/L		05 10-NOV-0		1
Barium (Ba)-Total	0.115		0.0003	1		05 10-NOV-0		
Beryllium (Be)-Total	<0.001		0.001	mg/L		05 10-NOV-0		1
Bismuth (Bi)-Total	<0.0001		0.0001	mg/L		05 10-NOV-05		
Calcium (Ca)-Total	245		0.1	mg/L		05 10-NOV-05		1
Cadmium (Cd)-Total	0.0008		0.0002	mg/L	09-NOV-	05 10-NOV-05	DAG	
Cobalt (Co)-Total	0.0010		0.0002	mg/L	09-NOV-0	5 10-NOV-05	DAG	í
Chromium (Cr)-Total	0.004		0.001	mg/L		5 10-NOV-05		
Cesium (Cs)-Total	<0.0001		0.0001	mg/L		5 10-NOV-05		
Copper (Cu)-Total	0.012		0.001	mg/L		5 10-NOV-05		1
Iron (Fe)-Total	0.61		0.05	mg/L		5 10-NOV-05		1
Potassium (K)-Total	1.3		0.1	mg/L		5 10-NOV-05	DAG	1
Lithium (Li)-Total	0.02		0.01	mg/L		5 10-NOV-05	DAG	
Magnesium (Mg)-Total	60.0		0.01	mg/L		5 10-NOV-05	DAG	
Manganese (Mn)-Total	0.0341		0.0003	mg/L		5 10-NOV-05	DAG	R34497
Molybdenum (Mo)-Total	<0.0002	C	.0002	mg/L	09-NOV-0	5 10-NOV-05	DAG	R34497
Sodium (Na)-Total	13.5		0.03	mg/L		5 10-NOV-05	DAG	R34497
Nickel (Ni)-Total	0.041	(0.002	mg/L		10-NOV-05	DAG	R34497
Phosphorus (P)-Total	0.15		0.05	mg/L	09-NOV-0	10-NOV-05	DAG	R34497
Lead (Pb)-Total	0.0048	0	.0005	mg/L	09-NOV-0	10-NOV-05	DAG	R34497
Rubidium (Rb)-Total	0.0022	0	.0002	mg/L	09-NOV-08	10-NOV-05	DAG	R34497
Antimony (Sb)-Total	<0.001	0).001	mg/L		10-NOV-05		R34497
Selenium (Se)-Total Tin (Sn)-Total	0.004	i	.001	mg/L		10-NOV-05	DAG	1
	<0.0006	1	.0006	mg/L		10-NOV-05	DAG	R34497
Strontium (Sr)-Total Tellurium (Te)-Total	0.319	ļ	0001	mg/L		10-NOV-05	DAG	R34497
Titanium (Ti)-Total	<0.001	f f	.001	mg/L	09-NOV-05		DAG	R344974
Thallium (TI)-Total	0.0252	1	0009	mg/L	09-NOV-05		DAG	R344974
Uranium (U)-Total	0.0001	1	0001	mg/L	09-NOV-05	10-NOV-05	DAG	R344974
Vanadium (V)-Total	0.0041	i	0001	mg/L	09-NOV-05		DAG	R344974
Tungsten (W)-Total	0.002	- 1	001		09-NOV-05		DAG	R344974
	<0.0002	i	0002		09-NOV-05		1	R344974
Zinc (Zn)-Total Zirconium (Zr)-Total	0.05	1	.01		09-NOV-05		DAG	R344974
	0.0015	0.0	0004	mg/L	09-NOV-05	10-NOV-05		R344974
ardness Calculated Hardness (as CaCO3)	858		.3	ma/l		10 NOV 05		
onductivity		0		mg/L		10-NOV-05		
Conductivity	1330	0	.4 u	mhos/cm	k	08-NOV-05	DXN F	R344368
hloride Soluble			1	1	ſ			

Sample Details/Parameters	Result	Qualif	ier D.L	Units	Extracted	Analyze	d By	Batch
L338009-1 MW 401								And the second
Sample Date: 04-NOV-05 08:00							***************************************	
Matrix: WATER							***	
Routine Soluble + Metal scan								
Chloride Soluble								
Chloride (CI) - Soluble	<9		9	mg/L		07-NOV-0	5 CLN	A R344055
Alkalinity								
Alkalinity, Total (as CaCO3) Bicarbonate (HCO3)	597		1	mg/L		08-NOV-0		N R344368
Carbonate (CO3)	728 <0.6		2	mg/L		08-NOV-0		
Hydroxide (OH)	<0.4		0.6	mg/L		08-NOV-0		
338009-2 MW 402	10.4	-	0.4	mg/L		08-NOV-0	5 DXN	R344368
ample Date: 04-NOV-05 08:00								
atrix: WATER								
WDG Monitoring Well								
Sulphate Dissolved								
Sulphate (SO4) - Dissolved	92		9	mg/L	07-NOV-04	07-NOV-05	CLM	D244055
Nitrate + Nitrite Dissolved				9/	J. 110 V-0.	J140 V-05	CLIM	R344055
Nitrate+Nitrite-N - Dissolved	1.46	RAMB	0.01	mg/L	07-NOV-05	07-NOV-05	CLM	R344055
Chloride Dissolved								
Chloride (Cl) - Dissolved	26		9	mg/L	07-NOV-05	07-NOV-05	CLM	R344055
Ammonia Dissolved Ammonia (NH3) - Dissolved	0.00							
Phosphorus, Total	0.06		0.01	mg/L	07-NOV-05	07-NOV-05	CLM	R344055
Total Phosphorous	0.032	RAMB	0.001	ma/l		40 1101 405		
рН	0.002	10 11110	0.001	mg/L		10-NOV-05	MEB	R345178
PH	7.41		0.01	pH units		07-NOV-05	DXN	R344056
Turbidity						0	DAN	1344030
Turbidity	70		0.05	NTU		07-NOV-05	DXN	R343905
Total Suspended Solids								
Total Suspended Solids Total Solids	180		5	mg/L		07-NOV-05	LVP	R344261
Total Solids	870		_					
Total Kjeldahl Nitrogen	870		5	mg/L		07-NOV-05	LVP	R344261
Total Kjeldahl Nitrogen	<0.2		0.2	mg/L	09-NOV-05	15-NOV-05	CLM	R346542
Total Dissolved Solids			0.2	9/2	05-140-05	10-140-05	CLIM	K346542
Total Dissolved Solids	660		5	mg/L		07-NOV-05	LVP	R344261
Hardness Calculated								11011201
Hardness (as CaCO3)	516	ĺ	0.2	mg/L		7-NOV-05		
Cyanide, Free Cyanide, Free	.0.04	-						
Conductivity	<0.01		0.01	mg/L		7-NOV-05	MB	R343922
Conductivity	1050		0.4	umhos/cm		7 NOV 05	5)4.	50.440.50
Chemical Oxygen Demand	1000		U. 4	umnos/cm		7-NOV-05	DXN	R344056
Chemical Oxygen Demand	<8	-	8	mg/L	o	8-NOV-05	SXG	R344384
BTEX and TVH (C5-C10)	**************************************		-				UNG	11074304
Benzene	<0.0005	C	0.0005	mg/L	o	8-NOV-05	TJJ	R344763
Toluene	<0.0005	C	0.0005	mg/L	0	8-NOV-05	1	R344763
Ethylbenzene	<0.0005		.0005	mg/L	0	3-NOV-05	- 1	R344763
m+p-xylenes	<0.0005	1	.0005	mg/L	i i	3-NOV-05	1	R344763
o-xylene	<0.0005	0	.0005	mg/L	1	3-NOV-05	TJJ I	R344763
Total Volatiles	<0.1		0.1	mg/L	1	3-NOV-05	1	R344763
Xylenes	<0.0005	0	.0005	mg/L	08	-NOV-05	TJJ F	R344763
Alkalinity Alkalinity, Total (as CaCO3)	469							
Annamity, Total (as CaCCS)	409		1	mg/L	07	-NOV-05	DXN F	R344056

Sample Details/Parameters	Result	Qualifier	D.L.	Units	Extracte	d Analyze	d By	Bat
L338009-2 MW 402								
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								
WDG Monitoring Well								
Alkalinity								
Bicarbonate (HCO3)	572					22 11014 2		
Carbonate (CO3)	<0.6		2	mg/L	i	07-NOV-0		
Hydroxide (OH)	<0.4		0.6	mg/L	1	07-NOV-0	1	
try arosina (e. i)	~0.4		0.4	mg/L		07-NOV-0	5 DX	N R344
Total Volatiles	-0.4							
TEH (C11-C30)	<0.1		0.1	mg/L		08-NOV-0		J R344
•	<0.1		0.1	mg/L	08-NOV	05 09-NOV-0	5 HD	T R344
Metal scan Silver (Ag)-Total								
Aluminum (AI)-Total	<0.001		0.001	mg/L		05 10-NOV-0		3 R344
	0.14		0.02	mg/L		05 10-NOV-0		R344
Arsenic (As)-Total	<0.0005		0.0005	mg/L		05 10-NOV-0		R344
Boron (B)-Total	0.15		0.03	mg/L		05 10-NOV-05		R344
Barium (Ba)-Total Beryllium (Be)-Total	0.0889	1	0.0003	mg/L		05 10-NOV-05		R344
	<0.001	į.	0.001	mg/L	1	05 10-NOV-05	,	R344
Bismuth (Bi)-Total	<0.0001	(0.0001	mg/L		05 10-NOV-05		R344
Calcium (Ca)-Total	121		0.1	mg/L		05 10-NOV-05		R344
Cadmium (Cd)-Total	0.0021	1	0.0002	mg/L		05 10-NOV-05		R3449
Cobalt (Co)-Total	0.0004	C	0.0002	mg/L		05 10-NOV-05		R3449
Chromium (Cr)-Total	0.006	1	0.001	mg/L	09-NOV-0	5 10-NOV-05	DAG	ı
Cesium (Cs)-Total	<0.0001	0	0.0001	mg/L	09-NOV-0	5 10-NOV-05	DAG	1
Copper (Cu)-Total	0.004	(0.001	mg/L		5 10-NOV-05		1
iron (Fe)-Total	0.18		0.05	mg/L		5 10-NOV-05	DAG	
Potassium (K)-Total	3.8		0.1	mg/L		5 10-NOV-05	DAG	1
Lithium (Li)-Total	0.02		0.01	mg/L		5 10-NOV-05	DAG	
Magnesium (Mg)-Total	52.1	1	0.01	mg/L		5 10-NOV-05	DAG	R3449
Manganese (Mn)-Total	0.0110	0.	.0003	mg/L		5 10-NOV-05	DAG	R3449
Molybdenum (Mo)-Total	0.0012	0.	.0002	mg/L		5 10-NOV-05	DAG	R3449
Sodium (Na)-Total	19.0	1	0.03	mg/L	1	5 10-NOV-05	DAG	R3449
Nickel (Ni)-Total	0.015	1	0.002	mg/L		5 10-NOV-05	DAG	R3449
Phosphorus (P)-Total	0.11	ł .	0.05	mg/L		5 10-NOV-05	DAG	1
Lead (Pb)-Total	0.0041	1	0005	mg/L		10-NOV-05		R3449
Rubidium (Rb)-Total	0.0008		0002	mg/L		10-NOV-05	DAG	R3449
Antimony (Sb)-Total	<0.001	i	.001	mg/L		10-NOV-05	DAG	1
Selenium (Se)-Total	0.004	į	.001			10-NOV-05		R3449
Tin (Sn)-Total	0.0011	1	0006	mg/L	3	1 1		R34497
Strontium (Sr)-Total	0.412	1	0000	mg/L		10-NOV-05		R34497
Tellurium (Te)-Total	<0.001	1	i	mg/L		10-NOV-05	DAG	R34497
Titanium (Ti)-Total	0.0097	i i	.001	mg/L		10-NOV-05	DAG	R34497
Thallium (TI)-Total	{	1	0009	mg/L		10-NOV-05	DAG	R34497
Uranium (U)-Total	<0.0001	1	0001	mg/L		10-NOV-05	DAG	R34497
Vanadium (V)-Total	0.0109	1	0001	mg/L		10-NOV-05	DAG	R34497
Tungsten (W)-Total	<0.001		001	mg/L		10-NOV-05	DAG	R34497
	<0.0002	i i	0002	mg/L	09-NOV-05		DAG	R34497
Zinc (Zn)-Total	0.02	f	.01	mg/L	09-NOV-05	10-NOV-05	DAG	R344974
Zirconium (Zr)-Total	0.0005	0.0	004	mg/L	09-NOV-05	10-NOV-05	DAG	R344974
009-3 MW 403								
ole Date: 04-NOV-05 08:00						***************************************	and the same	
x: WATER	The state of the s		1				-	
VDG Monitoring Well			- Appelling			***************************************		
Sulphate Dissolved								
Sulphate (SO4) - Dissolved	481	_		ma/l	07.8004.05	NO NOV		20115
	701	9	,	mg/L	07-NOV-05	70-NUV-05	ALW	344388

Sample Details/Parameters	Result	Qualif	ier D.L.	Units	Extracte	d Analyze	d By	Batch
L338009-3 MW 403								
Sample Date: 04-NOV-05 08:00							-	
Matrix: WATER								
WDG Monitoring Well			-					
Nitrate + Nitrite Dissolved								1
Nitrate+Nitrite-N - Dissolved	0.32	RAMB	0.01	mg/L	07-NOV	-05 07-NOV-0	5 CL	M R344055
Chloride Dissolved								11044000
Chloride (CI) - Dissolved	33		9	mg/L	07-NOV	-05 07-NOV-0	5 CLI	M R344055
Ammonia Dissolved								
Ammonia (NH3) - Dissolved	0.64		0.01	mg/L	07-NOV-	05 07-NOV-0	5 CLI	M R344055
Phosphorus, Total Total Phosphorous	0.445	5446						-
pH	0.145	RAMB	0.001	mg/L		10-NOV-0	5 ME	B R345178
PH	7.80		0.04	m1114.				
Turbidity	7.00		0.01	pH units	3	07-NOV-0	5 DXI	N R344056
Turbidity	190		0.05	NTU		07 NOV 0		
Total Suspended Solids	100		0.05	NIO		07-NOV-0	DXI	N R343905
Total Suspended Solids	300		5	mg/L		07-NOV-05		D044004
Total Solids				g/ =		07-140-00	LVF	R344261
Total Solids	1600		5	mg/L		07-NOV-05	LVP	R344261
Total Kjeldahl Nitrogen								11344201
Total Kjeldahl Nitrogen	0.8		0.2	mg/L	09-NOV-0	5 15-NOV-05	CLM	R346542
Total Dissolved Solids								
Total Dissolved Solids	1300		5	mg/L		07-NOV-05	LVP	R344261
Hardness Calculated								
Hardness (as CaCO3) Cyanide, Free	432		0.2	mg/L		07-NOV-05		
Cyanide, Free	<0.01		201					
Conductivity	\0.01		0.01	mg/L		07-NOV-05	МВ	R343922
Conductivity	1790		0.4	umhos/cm		07-NOV-05	5	
Chemical Oxygen Demand			0.4	Gillios/Gil	']	07-140-05	DXN	R344056
Chemical Oxygen Demand	<8		8	mg/L		08-NOV-05	SXG	R344384
BTEX and TVH (C5-C10)			_			001101-00	376	K344364
Benzene	<0.0005		0.0005	mg/L		08-NOV-05	TJJ	R344763
Toluene	<0.0005		0.0005	mg/L		08-NOV-05	TJJ	R344763
Ethylbenzene	<0.0005		0.0005	mg/L		08-NOV-05	TJJ	R344763
m+p-xylenes	<0.0005		0.0005	mg/L		08-NOV-05	TJJ	R344763
o-xylene	<0.0005	1	0.0005	mg/L		08-NOV-05	TJJ	R344763
Total Volatiles	<0.1		0.1	mg/L		08-NOV-05	TJJ	R344763
Xylenes	<0.0005		0.0005	mg/L		08-NOV-05	TJJ	R344763
Alkalinity Alkalinity, Total (as CaCO3)	504	1						
Bicarbonate (HCO3)	521		1	mg/L		07-NOV-05	DXN	R344056
Carbonate (CO3)	636 <0.6	-	2	mg/L	f	07-NOV-05		R344056
Hydroxide (OH)	<0.4		0.6	mg/L	1	07-NOV-05		R344056
	-0.4		0.4	mg/L		07-NOV-05	DXN	R344056
Total Volatiles	<0.1	- 1	0.1	ma/l		00 1101/05		-
TEH (C11-C30)	<0.1		0.1	mg/L	ı	08-NOV-05	1	R344763
Metal scan	-0.1		0.1	mg/L	08-NOV-05	09-NOV-05	HDT	R344530
Silver (Ag)-Total	<0.001		0.001	mg/L	09-NOV-05	10-NOV 05	DAG	D244074
Aluminum (Al)-Total	0.29	i	0.02	- 1	09-NOV-05		1	R344974
Arsenic (As)-Total	0.0054	ì	.0005		09-NOV-05		1	R344974
Boron (B)-Total	0.23	1	0.03		09-NOV-05		ţ	R344974
Barium (Ba)-Total	0.0755	- 1	.0003		09-NOV-05 1		1	R344974
Beryllium (Be)-Total	<0.001	- 1	.0003	1	09-NOV-05 1		1	R344974
						5 110 V-05	ו טאט	R344974
		-	1	I	1	1	ļ	ĺ

Sample Details/Parameters	Result	Qua	ilifier D.	L. Units	Extract	ed Analyzo	ed By	Batch
L338009-3 MW 403								Data
Sample Date: 04-NOV-05 08:00 Matrix: WATER								
Maux. VVATER								
Metal scan								The same of the sa
Bismuth (Bi)-Total	<0.0001		0.00	04				
Calcium (Ca)-Total	90.6		0.00			/-05 10-NOV-		, , , , , , , , , , , , , , , , , , , ,
Cadmium (Cd)-Total	0.0002		0.1	-		/-05 10-NOV-	1	1 1 1 1 1 1 1 1
Cobalt (Co)-Total	0.0012		0.00			-05 10-NOV-0		1
Chromium (Cr)-Total	0.002		0.00	1 -		-05 10-NOV-0		
Cesium (Cs)-Total	<0.0001		0.00	1		'-05 10-NOV-('-05 10-NOV-(1
Copper (Cu)-Total	0.007		0.00	, .		-05 10-NOV-0		
Iron (Fe)-Total	0.41		0.08	_		-05 10-NOV-0		1
Potassium (K)-Total	8.1		0.1			-05 10-NOV-0	i	
Lithium (Li)-Total	0.05		0.01	1		-05 10-NOV-0		
Magnesium (Mg)-Total	49.9		0.01	1		05 10-NOV-0		
Manganese (Mn)-Total	0.384		0.000	, -		05 10-NOV-0		1
Molybdenum (Mo)-Total	0.0119		0.000	_		05 10-NOV-0		1
Sodium (Na)-Total	262		0.03	, -		05 10-NOV-0		1
Nickel (Ni)-Total	0.005		0.002	2 mg/L		05 10-NOV-0		1
Phosphorus (P)-Total	0.14		0.05	mg/L		05 10-NOV-0		1
Lead (Pb)-Total	0.0011		0.000	5 mg/L		05 10-NOV-05		
Rubidium (Rb)-Total	0.0033		0.000	2 mg/L		05 10-NOV-05		1
Antimony (Sb)-Total Selenium (Se)-Total	<0.001		0.001	-		05 10-NOV-05		ı
Tin (Sn)-Total	0.006		0.001	-		05 10-NOV-05		1
Strontium (Sr)-Total	<0.0006		0.0006	,		05 10-NOV-05		R344974
Tellurium (Te)-Total	0.629		0.000	1		05 10-NOV-05		R344974
Titanium (Ti)-Total	<0.001 0.0189		0.001	, ,		05 10-NOV-05	DAG	R344974
Thallium (TI)-Total	0.0189		0.0009			5 10-NOV-05	DAG	R344974
Uranium (U)-Total	0.0161		0.0001	1		5 10-NOV-05	DAG	
Vanadium (V)-Total	0.004		0.0001	1		5 10-NOV-05	DAG	1
Tungsten (W)-Total	<0.0002		0.0001	mg/L mg/L		5 10-NOV-05	DAG	
Zinc (Zn)-Total	0.02		0.0002	mg/L		5 10-NOV-05 5 10-NOV-05	DAG	R344974
Zirconium (Zr)-Total	0.0012		0.0004	4		5 10-NOV-05	DAG	R344974
338009-4 MW 405			0.0004	mg/L	03-140-0	0-10-100	DAG	R344974
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								
WDG Monitoring Well								
Sulphate Dissolved								
Sulphate (SO4) - Dissolved	9		9	mg/L	07.NOV 06	07-NOV-05		
Nitrate + Nitrite Dissolved				mg/L	07-140-05	07-1400-05	CLM	R344055
Nitrate+Nitrite-N - Dissolved	0.01	RAMB	0.01	mg/L	07-NOV-05	07-NOV-05	CLM	D2440EE
Chloride Dissolved			0.01	1119/2	01-140-03	07-1400-05	CLM	R344055
Chloride (CI) - Dissolved	21		9	mg/L	07-NOV-05	07-NOV-05	CLM	R344055
Ammonia Dissolved					0. 1101 00	o, 110 V-05	CLIVI	K344033
Ammonia (NH3) - Dissolved	0.05		0.01	mg/L	07-NOV-05	07-NOV-05	CLM	R344055
Phosphorus, Total				•			OLIVI	11344033
Total Phosphorous	0.148	RAMB	0.001	mg/L		10-NOV-05	MEB	R345178
pH				_				
PH	7.65		0.01	pH units		07-NOV-05	DXN	R344056
Turbidity								
Turbidity	190		0.05	NTU		07-NOV-05	DXN	R343905
Total Suspended Solids Total Suspended Solids	000		_					
rotal ouspended Sullus	200		5	mg/L		07-NOV-05	LVP I	R344261

Sample Details/Parameters	Result	Qualifier D.L.	Units	Extracted	Analyze	i By	Batch
L338009-4 MW 405							
Sample Date: 04-NOV-05 08:00						-	
Matrix: WATER			***			Ì	
WDG Monitoring Well							
Total Solids							
Total Solids	1600	5	mg/L		07-NOV-0	5 LVF	R34426
Total Kjeldahl Nitrogen			3-		0. 11010		134420
Total Kjeldahl Nitrogen	0.2	0.2	mg/L	09-NOV-0	5 15-NOV-0	5 CLN	R34654
Total Dissolved Solids							
Total Dissolved Solids	1300	5	mg/L		07-NOV-0	5 LVF	R34426
Hardness Calculated		****					
Hardness (as CaCO3)	590	0.2	mg/L		07-NOV-0	5	
Cyanide, Free		į					
Cyanide, Free	<0.01	0.01	mg/L		07-NOV-05	MB	R343922
Conductivity Conductivity							
	1830	0.4	umhos/cn	1	07-NOV-05	DXN	R344056
Chemical Oxygen Demand Chemical Oxygen Demand	24			i.i.d. i.i.			
BTEX and TVH (C5-C10)	24	8	mg/L		08-NOV-05	SXG	R344384
Benzene	<0.0005	0.0005					
Toluene	<0.0005	0.0005	mg/L		08-NOV-05	1	R344763
Ethylbenzene	<0.0005	0.0005	mg/L		08-NOV-05	1	R344763
m+p-xylenes	<0.0005	0.0005 0.0005	mg/L		08-NOV-05	1	R344763
o-xylene	<0.0005	0.0005	mg/L		08-NOV-05		R344763
Total Volatiles	<0.0003		mg/L		08-NOV-05	TJJ	R344763
Xylenes	<0.0005	0.1	mg/L		08-NOV-05	TJJ	R344763
Alkalinity	40.0005	0.0005	mg/L		08-NOV-05	TJJ	R344763
Alkalinity, Total (as CaCO3)	505	1	mg/L		07-NOV-05	DV	D044050
Bicarbonate (HCO3)	617	2	mg/L	§ .	07-NOV-05	DXN	R344056
Carbonate (CO3)	<0.6	0.6	mg/L	[]	07-NOV-05	DXN	R344056
Hydroxide (OH)	<0.4	0.4	mg/L	1 1	07-NOV-05	DXN DXN	R344056 R344056
Total Volatiles	<0.1	0.1	mg/L		00 NOV 05	· · · · ·	
TEH (C11-C30)	<0.1	0.1	-	1	08-NOV-05	TJJ	R344763
Metal scan	70.1	0.1	mg/L	08-NOV-05	U9-NOV-05	HDT	R344530
Silver (Ag)-Total	<0.001	0.001	mg/L	09-NOV-05	10 NOV 05	240	
Aluminum (AI)-Total	0.49	0.001	mg/L	09-NOV-05		DAG	R344974
Arsenic (As)-Total	0.0016	0.0005	mg/L	09-NOV-05			R344974
Boron (B)-Total	0.05	0.03	mg/L	09-NOV-05 1		DAG	R344974
Barium (Ba)-Total	0.115	0.0003	-	09-NOV-05 1		DAG	R344974
Beryllium (Be)-Total	<0.001	0.001	-	09-NOV-05 1	1	DAG DAG	R344974
Bismuth (Bi)-Total	<0.0001	0.0001		09-NOV-05 1		1	R344974
Calcium (Ca)-Total	147	0.1		09-NOV-05 1		1	R344974 R344974
Cadmium (Cd)-Total	0.0019	0.0002		09-NOV-05 1			R344974
Cobalt (Co)-Total	0.0009	0.0002		09-NOV-05 1		ł	R344974
Chromium (Cr)-Total	0.002	0.001		09-NOV-05 1		1	R344974
Cesium (Cs)-Total	<0.0001	0.0001	j	09-NOV-05 1	,	i	R344974
Copper (Cu)-Totai	0.011	0.001	- 1	09-NOV-05 1	Į.		R344974
iron (Fe)-Total	0.63	0.05	- 1	09-NOV-05 1		1	R344974 R344974
Potassium (K)-Total	4.2	0.1		9-NOV-05 10		,	R344974
Lithium (Li)-Total	0.03	0.01		9-NOV-05 10		1	R344974
Magnesium (Mg)-Total	54.2	0.01		9-NOV-05 10			3449 74 344974
Manganese (Mn)-Total	0.143	0.0003		9-NOV-05 10		i	344974 344974
Molybdenum (Mo)-Total	0.0077	0.0002		9-NOV-05 10			R344974
Sodium (Na)-Total	196	0.03	- 1	9-NOV-05 10		DAG I	1077014

Sample Details/Parameters	Result	Qualif	ier D.L.	Units	Extracte	d Analyze	d By	Batch	
L338009-4 MW 405									
Sample Date: 04-NOV-05 08:00									
Matrix: WATER									
Metal scan									
Nickel (Ni)-Total	0.048		0.002	mg/L	09. NOV	05 10-NOV-0		0 0044074	
Phosphorus (P)-Total	0.13		0.002	9	1	05 10-NOV-0	- 1 1		
Lead (Pb)-Total	0.0017		0.000			05 10-NOV-0			
Rubidium (Rb)-Total	0.0030		0.000	- 1		05 10-NOV-0		1	
Antimony (Sb)-Total	<0.001		0.001			05 10-NOV-0			
Selenium (Se)-Total	0.012		0.001	, -		05 10-NOV-0		_	
Tin (Sn)-Total	0.0008		0.0006			05 10-NOV-0		1.10.10.1	i
Strontium (Sr)-Total	0.582		0.0001			05 10-NOV-0	- 1	1	
Tellurium (Te)-Total	<0.001		0.001			05 10-NOV-0			
Titanium (Ti)-Total	0.0222		0.0009	1		5 10-NOV-0		1.10.10.1	
Thallium (TI)-Total	<0.0001		0.0001			05 10-NOV-0		1	-
Uranium (U)-Total	0.0144		0.0001			5 10-NOV-0		1	-
Vanadium (V)-Total	0.002		0.001	mg/L		5 10-NOV-0		1	
Tungsten (W)-Total	<0.0002		0.0002	_	1	5 10-NOV-0	1		
Zinc (Zn)-Total	0.04		0.01	mg/L		5 10-NOV-0		1	
Zirconium (Zr)-Total	0.0014		0.0004	, -	1	5 10-NOV-05	1	1	
.338009-5 MW 406							+		-
Sample Date: 04-NOV-05 08:00									
Matrix: WATER									
WDG Monitoring Well									
Sulphate Dissolved									
Sulphate (SO4) - Dissolved	27		9	mg/L	07-NOV-0	5 07-NOV-05	CLM	R344055	
Nitrate + Nitrite Dissolved Nitrate+Nitrite-N - Dissolved	0.15	RAMB	0.01	mg/L	07 NOV 0	07 NOV 05			
Chloride Dissolved	0.10	10.00	0.01	mg/L	07-1400-0	07-NOV-05	CLM	R344055	
Chloride (CI) - Dissolved	20		9	mg/L	07-NOV-0	07-NOV-05	CLM	R344055	
Ammonia Dissolved							-	11011000	
Ammonia (NH3) - Dissolved	0.06		0.01	mg/L	07-NOV-0	07-NOV-05	CLM	R344055	
Phosphorus, Total								1.00	
Total Phosphorous	0.052	RAMB	0.001	mg/L		10-NOV-05	MEB	R345178	
pH									
PH	8.11		0.01	pH units		07-NOV-05	DXN	R344056	
Turbidity									
Turbidity	8.7		0.05	NTU		07-NOV-05	DXN	R343905	
Total Suspended Solids									
Total Suspended Solids	14		5	mg/L		07-NOV-05	LVP	R344261	
Total Solids									
Total Solids	210		5	mg/L		07-NOV-05	LVP	R344261	
Total Kjeldahl Nitrogen								William property	
Total Kjeldahl Nitrogen	0.3		0.2	mg/L	09-NOV-05	15-NOV-05	CLM	R346542	
Total Dissolved Solids								VA	
Total Dissolved Solids	190		5	mg/L		07-NOV-05	LVP	R344261	
Hardness Calculated		***************************************							
Hardness (as CaCO3)	76.7		0.2	mg/L		07-NOV-05		th companying.	
Cyanide, Free									
Cyanide, Free	<0.01		0.01	mg/L		07-NOV-05	MB	R343922	
Conductivity								-	
Conductivity	316		0.4	umhos/cm	(7-NOV-05	DXN	R344056	
Chemical Oxygen Demand			_		- The state of the		-		
Chemical Oxygen Demand	<8		8	mg/L	C	18-NOV-05	SXG	R344384	

Sample Details/Parameters	Result	Qualifier D.L.	Units	Extracted	Analyzed	By By	Batch
L338009-5 MW 406							
Sample Date: 04-NOV-05 08:00		Line and the second sec					
Matrix: WATER							
WDG Monitoring Well							
BTEX and TVH (C5-C10)				er e			
Benzene	<0.0005	0.0005	mg/L		08-NOV-05	TJJ	R344763
Toluene	<0.0005	0.0005	mg/L		08-NOV-05	5 TJJ	
Ethylbenzene	<0.0005	0.0005	mg/L		08-NOV-05	TJJ	R344763
m+p-xylenes	<0.0005	0.0005	mg/L		08-NOV-05	i TJJ	R344763
o-xylene	<0.0005	0.0005	mg/L		08-NOV-05	TJJ	R344763
Total Volatiles	<0.1	0.1	mg/L		08-NOV-05	TJJ	R344763
Xylenes	<0.0005	0.0005	mg/L		08-NOV-05	TJJ	R344763
Alkalinity							
Alkalinity, Total (as CaCO3)	106	1	mg/L		07-NOV-05		R344056
Bicarbonate (HCO3)	129	2	mg/L	1	07-NOV-05		R344056
Carbonate (CO3)	<0.6	0.6	mg/L		07-NOV-05	DXN	R344056
Hydroxide (OH)	<0.4	0.4	mg/L		07-NOV-05	DXN	R344056
Total Volatiles	<0.1	0.1	mg/L		08-NOV-05		2044700
TEH (C11-C30)	<0.1	0.1	mg/L	08-NOV-05		TJJ	R344763
Metal scan	0	0.1	mg/L	00-140-05	09-140-05	HDT	R344530
Silver (Ag)-Total	<0.001	0.001	mg/L	09-NOV-05	10-NOV-05	DAG	R344974
Aluminum (AI)-Total	0.24	0.02	mg/L	09-NOV-05		DAG	R344974
Arsenic (As)-Total	<0.0005	0.0005	mg/L	09-NOV-05		DAG	R344974
Boron (B)-Total	<0.03	0.03	mg/L	09-NOV-05		DAG	R344974
Barium (Ba)-Total	0.0121	0.0003	mg/L	09-NOV-05		DAG	R344974
Beryllium (Be)-Total	<0.001	0.001	mg/L	09-NOV-05		DAG	R344974
Bismuth (Bi)-Total	<0.0001	0.0001	mg/L	09-NOV-05		DAG	R344974
Calcium (Ca)-Total	23.1	0.1	mg/L	09-NOV-05		DAG	R344974
Cadmium (Cd)-Total	0.0012	0.0002	mg/L	09-NOV-05		DAG	R344974
Cobalt (Co)-Total	0.0004	0.0002	mg/L	09-NOV-05		DAG	R344974
Chromium (Cr)-Total	0.001	0.001	mg/L	09-NOV-05		DAG	R344974
Cesium (Cs)-Total	<0.0001	0.0001	mg/L	09-NOV-05		DAG	R344974
Copper (Cu)-Total	0.010	0.001	mg/L	09-NOV-05	1	DAG	R344974
Iron (Fe)-Total	0.23	0.05	mg/L	09-NOV-05 1	1	DAG	R344974
Potassium (K)-Total	1.2	0.1	mg/L	09-NOV-05 1	0-NOV-05	DAG	R344974
Lithium (Li)-Total	<0.01	0.01	mg/L	09-NOV-05 1		DAG	R344974
Magnesium (Mg)-Total	4.61	0.01	mg/L	09-NOV-05 1	0-NOV-05		R344974
Manganese (Mn)-Total	0.0346	0.0003	mg/L	09-NOV-05 1	0-NOV-05	DAG	R344974
Molybdenum (Mo)-Total	<0.0002	0.0002	mg/L	09-NOV-05 1	0-NOV-05		R344974
Sodium (Na)-Total	3.05	0.03	mg/L	09-NOV-05 1	0-NOV-05		R344974
Nickel (Ni)-Total	0.010	0.002	mg/L	09-NOV-05 1	0-NOV-05		R344974
Phosphorus (P)-Total	0.10	0.05	mg/L	09-NOV-05 1	0-NOV-05		R344974
Lead (Pb)-Total	0.0014	0.0005	mg/L	09-NOV-05 1	0-NOV-05	-	R344974
Rubidium (Rb)-Total	0.0010	0.0002	mg/L	09-NOV-05 10	D-NOV-05	1	R344974
Antimony (Sb)-Total	0.001	0.001	mg/L	09-NOV-05 10	D-NOV-05	1	R344974
Selenium (Se)-Total	0.003	0.001	mg/L	09-NOV-05 10)-NOV-05	DAG	R344974
Tin (Sn)-Total	0.0047	0.0006	mg/L	09-NOV-05 10	-NOV-05	1	R344974
Strontium (Sr)-Total	0.0389	0.0001	mg/L	09-NOV-05 10	-NOV-05	DAG	R344974
Tellurium (Te)-Total	<0.001	0.001	mg/L	09-NOV-05 10	-NOV-05		R344974
Titanium (Ti)-Total	0.0060	0.0009	ł	09-NOV-05 10	-NOV-05		R344974
Thallium (TI)-Total	<0.0001	0.0001	1	09-NOV-05 10	-NOV-05	1	R344974
Uranium (U)-Total	0.0001	0.0001	-	09-NOV-05 10	1	į.	R344974
Vanadium (V)-Total	<0.001	0.001	- 1	09-NOV-05 10		T I	R344974
Tungsten (W)-Total	<0.0002	0.0002	- 1	09-NOV-05 10	1	1	R344974

Sample Details/Parameters	Result	Qualifie	or D.L.	Units	Extracted	Analyzed	Ву	Batch
L338009-5 MW 406								
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								
Mauric. WATER								
Metal scan								
Zinc (Zn)-Total	0.17		0.01	mg/L	09-NOV-04	5 10-NOV-0	DAC	R344974
Zirconium (Zr)-Total	<0.0004		0.0004	1	1	10-NOV-0		1
L338009-6 MW 999			-	-			-	7 11011011
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								
THOUSE THE TAXABLE PROPERTY OF THE PARTY OF								
Routine Soluble + Metal scan								
pH								
PH	7.89		0.01	pH units		07-NOV-05	DXN	R344056
TDS calculated								
TDS (Calculated)	1230		5	mg/L	- Andrews	14-NOV-05		
Sulphate Soluble								
Sulphate (SO4) - Soluble	454		9	mg/L		08-NOV-05	ALW	R344388
Nitrate + Nitrite Soluble Nitrate+Nitrite-N	0.04	DALLED						
Metal scan	0.31	RAMB	0.01	mg/L		07-NOV-05	CLM	R344055
Silver (Ag)-Total	<0.001		0.001	ma/l	10 NOV 05	40 11014 05		
Aluminum (Al)-Total	0.92		0.001	mg/L mg/L	10-NOV-05 10-NOV-05		DAG	1
Arsenic (As)-Total	0.0055		0.005	mg/L	10-NOV-05		DAG	R345886
Boron (B)-Total	0.27		0.003	mg/L	10-NOV-05		DAG DAG	R345886 R345886
Barium (Ba)-Total	0.0830		0.0003	mg/L	10-NOV-05		DAG	1
Beryllium (Be)-Total	<0.001		0.001	mg/L	10-NOV-05		DAG	R345886
Bismuth (Bi)-Total	<0.0001		0.0001	mg/L	10-NOV-05		DAG	R345886
Calcium (Ca)-Total	100		0.1	mg/L	10-NOV-05		DAG	R345886
Cadmium (Cd)-Total	0.0411		0.0002	mg/L	10-NOV-05		DAG	R345886
Cobalt (Co)-Total	0.0022		0.0002	mg/L	10-NOV-05	10-NOV-05	DAG	R345886
Chromium (Cr)-Total	0.003		0.001	mg/L	10-NOV-05	10-NOV-05	DAG	R345886
Cesium (Cs)-Total	0.0001		0.0001	mg/L	10-NOV-05	10-NOV-05	DAG	R345886
Copper (Cu)-Total	0.009		0.001	mg/L	10-NOV-05	10-NOV-05	DAG	R345886
Iron (Fe)-Total	1.45		0.05	mg/L	10-NOV-05 1		DAG	R345886
Potassium (K)-Total	8.3		0.1	mg/L	10-NOV-05 1	1	DAG	R345886
Lithium (Li)-Total Magnesium (Mg)-Total	0.04		0.01	mg/L	10-NOV-05 1		DAG	R345886
Manganese (Mn)-Total	52.3 0.428		0.01	mg/L	10-NOV-05 1		DAG	R345886
Molybdenum (Mo)-Total	0.0101	1	0.0003	mg/L	10-NOV-05 1		DAG	R345886
Sodium (Na)-Total	273	1	0.0002	mg/L	10-NOV-05 1 10-NOV-05 1		DAG	R345886
Nickel (Ni)-Total	0.015	· ·	0.002	mg/L mg/L	10-NOV-05 1			R345886 R345886
Phosphorus (P)-Total	0.24		0.05	mg/L	10-NOV-05 1	1		R345886
Lead (Pb)-Total	0.0035	10	0.0005	- ;	10-NOV-05 1		i	R345886
Rubidium (Rb)-Total	0.0048	1	0.0002		10-NOV-05 1	1	1	R345886
Antimony (Sb)-Total	<0.001	- 1	0.001		10-NOV-05 10		1	R345886
Selenium (Se)-Total	0.004		0.001		10-NOV-05 10		1	R345886
Tin (Sn)-Total	0.0009	i	.0006		10-NOV-05 10		f	R345886
Strontium (Sr)-Total	0.632		.0001	- }	10-NOV-05 10	3	i	R345886
Tellurium (Te)-Total	<0.001	ł	0.001		10-NOV-05 10		1	R345886
Titanium (Ti)-Total	0.0533	1	.0009		10-NOV-05 10	- 1	1	R345886
Thallium (TI)-Total	<0.0001	0	.0001	mg/L	10-NOV-05 10	-NOV-05	í	R345886
Uranium (U)-Total	0.0158	0.	.0001		10-NOV-05 10		,	R345886
Vanadium (V)-Total	0.005	0	.001		10-NOV-05 10		1	R345886
Tungsten (W)-Total	<0.0002	0.	0002	mg/L 1	10-NOV-05 10	-NOV-05	DAG I	R345886

Sample Details/Parameters	Result	Qualifier	D.L.	Units	Extracted	Analyzed	Ву	Batch
L338009-6 MW 999	*** **********************************			Total Control of the				
Sample Date: 04-NOV-05 08:00								
Matrix: WATER								
Routine Soluble + Metal scan								
Metal scan								
Zinc (Zn)-Total	0.03		0.01	mg/L	10-NOV-05	10-NOV-05	DAG	R345886
Zirconium (Zr)-Total	0.0020		0.0004	mg/L		10-NOV-05		R345886
Hardness Calculated								
Hardness (as CaCO3)	465		0.3	mg/L		14-NOV-05		
Conductivity Conductivity								
	1790		0.4	umhos/cm		07-NOV-05	DXN	R344056
Chloride Soluble Chloride (Cl) - Soluble	0.4		_					
Alkalinity	34		9	mg/L		07-NOV-05	CLM	R344055
Alkalinity, Total (as CaCO3)	507			/I		07.1101.405		
Bicarbonate (HCO3)	618		1	mg/L		07-NOV-05		R344056
Carbonate (CO3)	<0.6		2 0.6	mg/L		07-NOV-05		R344056
Hydroxide (OH)	<0.4		0.6	mg/L mg/L		07-NOV-05 07-NOV-05		R344056
	-0.4		0.4	nig/L		U/-NUV-U5	DXN	R344056
Refer to Referenced Information for Qua	alifiers (if any) and Me	hodology						
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Reference Information

Sample Parameter Qualifier key listed:

Qualifier Description **RAMB** Result Adjusted For Method Blank Methods Listed (if applicable): **ETL Test Code** Matrix **Test Description** Preparation Method Reference(Based On) Analytical Method Reference(Based On) ALK-TOT-WP Water Alkalinity

Alkalinity of water is a measure of its acid neutralizing capacity. Alkalinity is imparted by bicarbonate, carbonate and hydroxide components of water. It is determined by titration with a standard solution of strong mineral acid to the successive HCO3- and H2CO3 endpoints indicated electrometrically.

BTX,TVH-WP

Water

BTEX and TVH (C5-C10)

EPA SW846,5030,8015

Volatile organic compounds are extracted (purged) by bubbling nitrogen through a water sample. The purged sample components are trapped in a tube containing a sorbent material. When purging is complete, the tube is heated and back flushed with helium to desorb the trapped compounds onto a gas chromatographic column. The gas chromatograph is temperature programmed to separate the method analytes which are then detected with a photoionization detector (PID) followed by a flame ionization detector (FID).

CL-DIS-WP

Water

Chloride Dissolved

APHA4500;1998/LACHAT;MAR 1997

APHA 4500B, 2510B, 2320B, 1998

Chloride - Colourimetric using Mercuric Thiocyanate CL-SOL-WP

Water

Chloride Soluble

APHA4500;1998/LACHAT;MAR 1997

Chloride - Colourimetric using Mercuric Thiocyanate

CN-FREE-WP

Water

Cyanide, Free

APHA 4500CN C E-Strong acid Dist

Colorim

COD-WP

Water

Chemical Oxygen Demand

APHA 5220 D

The Chemical Oxygen Demand (COD) test is used to estimate the amount of organic matter in the water. The sample is added to HACH brand COD tubes, which contain a premixed volume of reagents. The sample is then heated for two hours on the COD reactor with a strong oxidizing agent, potassium dichromate. The COD reagents also contain silver and mercury ions. Silver is used as a catalyst and mercury is used to complex chloride interference. Oxidizable organic compounds react, reducing the dichromate ion to green chromic ion.

For the 10 - 150 mg/L range the remaining Cr6+ is measured colormetrically and a decrease in absorbance at 420 nm is proportional to the COD. For the 100 - 1500 mg/L range the amount of Cr3+ produced is measured colormetrically and an increase in absorbance at 620 nm is proportional to the COD. Samples with concentrations > 1500 mg/L can be diluted into either linear range.

EC-WP

Water

Conductivity

APHA 4500B, 2510B, 2320B, 1998

Conductivity of an aqueous solution refers to its ability to carry an electric current. Conductance of a solution is measured between two spatially fixed and chemically inert electrodes.

ETL-HARDNESS-DIS-WP Water

Hardness Calculated

Calculated

ETL-HARDNESS-TOT-WP Water IONBALANCE-OP05-WP Water Hardness Calculated

Calculated **APHA 1030E**

MET-SCAN-TOT-LOW-

Water

Metal scan

EPA 200.8 Rev 5.4 May 1994

WP N-TOTKJ-WP

Water

Total Kieldahl Nitrogen

Quickchem method 10-107-06-2-E

Samples are digested with a sulphuric acid solution, cooled, diluted with water, and analyzed for ammonia. Total Kjeldahl nitrogen is the sum of freeammonia and organic nitrogen compounds which are converted to ammonium sulphate through this digestion process. Analysis is performed by Flow

Analysis (FIA). The pH of the digested sample is raised to a known, basic pH by neutralization with a concentrated buffer solution. This neutralization converts the ammonium cation to ammonia. The ammonia produced is heated with saliclyate and hypochlorite to produce blue colour which is proportional to the ammonia concentration

N2N3-DIS-WP N2N3-SOL-WP Water Water

Nitrate + Nitrite Dissolved

APHA4500;1998/LACHAT;MAR 1997

NH3-DIS-WP

Water

Nitrate + Nitrite Soluble Ammonia Dissolved

APHA4500;1998/LACHAT;MAR 1997 APHA4500;1998/LACHAT;MAR 1997

Ammonia - Colourimeric using Salicylate-nitroprusside and hypochlorite, in an alkaline phosphate buffer.

P-TOTAL-WP

Phosphorus, Total

APHA, 1998

Samples are digested using a sulphuric acid-persulphate mixture to convert organic phosphorous to orthophosphate. The samples are analyzed by either the Flow Injection Analysis (FIA) or the Segmented Flow Analysis (SFA) method. The absorbance measured by the instrument is proportional to the concentration of orthophosphate in the sample, and is reported as phosphorous. Samples are analyzed for total or total dissolved phosphorous depending on the sample pretreatment.

Reference Information

reference electrode.

SO4-DIS-WP

Water

Sulphate Dissolved

APHA4500;1998/LACHAT:MAR 1997

Sulphate - Turbidimetric

SO4-SOL-WP

Water

Sulphate Soluble

APHA4500;1998/LACHAT;MAR 1997

Sulphate - Turbidimetric

SOLIDS-TDS-WP

Water

Total Dissolved Solids

APHA 2540

The residue remaining in a prepared casserole after passing the sample through a 1.2 um Whatman GF/C glass microfibre filter and drying at 180 degrees C. Samples may be dried at 105 degrees C if the client specifically requests this drying temperature.

SOLIDS-TOT-WP

Water

Total Solids

APHA 2540

The sum of the homogeneous suspended and dissolved material in the sample dried at 105 degrees C in a prepared casserole.

SOLIDS-TOTSUS-WP

Water

Total Suspended Solids

APHA 2540

The residue retained by a prepared 1.5 um Whatman 934-AH glass microfibre filter dried at 105 degrees C.

TEH-WP

Water

Tot. Extr. Hydrocarbons (C11-

EPA SW846,8000A

This is the semi-quantitative determination of total extractable hydrocarbons (TEH) C11-C30 in water, soil and sediment samples. A water sample volume of 240 mLs in a 250 mL glass amber bottle is shaken with 2-4 mL hexane for one hour on a wrist action shaker, then sonicated for 5 minutes. A soil/sediment sample of 25 grams is weighed out with sodium sulphate and extracted with 10 mLs hexane/acetone for one hour on a wrist action shake then sonicated for 5 minutes. After extraction, the solvent layer is drawn off and analysed against a calibrated diesel standard on a gas chromatograph equipped with a flame ionization detector. All results are reported on a dry weight basis. By special request, the result can be calculated on C10-C24 to meet specific regulations.

TURBIDITY-WP

Water

Turbidity

APHA, 1998, 2130B

A strong light beam is sent through a transparent tube containing the sample. Light that is reflected at 90 degrees to the axis by suspended particles is detected by the photocell. The electrical response is proportional to the sample turbidity.

TVH-WP

Water

TVH (C5-C10)

EPA SW846,5030,8015

Volatile organic compounds are extracted (purged) by bubbling nitrogen through a water sample. The purged sample components are trapped in a tube containing a sorbent material. When purging is complete, the tube is heated and back flushed with helium to desorb the trapped compounds onto a gas chromatographic column. The gas chromatograph is temperature programmed to separate the method analytes which are then detected with a photoionization detector (PID) followed by a flame ionization detector (FID).

		** Laboratory Methods employed follow in-house procedures, which are generally based on nationally or internationally accepted methodologies					
Chain of Custody numbers:							
The last two letters of the ab							
THE IASI INO IEILEIS OF LITE AD	ove test code(s) indicate the laboratory	that performed analytical analysis for the	hat test. Refer to the list below:				
Laboratory Definition Code	Laboratory Location	Laboratory Definition Code	hat test. Refer to the list below: Laboratory Location				

Reference Information

GLOSSARY OF REPORT TERMS

Surr - A surrogate is an organic compound that is similar to the target analyte(s) in chemical composition and behavior but not normally detected in environmental samples. Prior to sample processing, samples are fortified with one or more surrogate compounds. The reported surrogate recovery value provides a measure of method efficiency. The Laboratory warning units are determined under column heading D.L.

mg/kg (units) - unit of concentration based on mass, parts per million mg/L (units) - unit of concentration based on volume, parts per million < - Less than

D.L. - Detection Limit

N/A - Result not available. Refer to qualifier code and definition for explanation

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

UNLESS OTHERWISE STATED, SAMPLES ARE NOT CORRECTED FOR CLIENT FIELD BLANKS.

Although test results are generated under strict QA/QC protocols, any unsigned test reports, faxes, or emails are considered preliminary.

Enviro-Test Laboratories has an extensive QA/QC program where all analytical data reported is analyzed using approved referenced procedures followed by checks and reviews by senior managers and quality assurance personnel. However, since the results are obtained from chemical measurements and thus cannot be guaranteed, Enviro-Test Laboratories assumes no liability for the use or interpretation of the results.



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Enviro-Test Quality Control Report

Workorder: L338009

Client:

UMA ENGINEERING 1479 BUFFALO PLACE WINNIPEG MB R3T 1L7

Contact:

PETER BOHONOS

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
ALK-TOT-WP	Water							
Batch R344056								
WG375519-5 CVS Alkalinity, Total (as Ca	CO3/		400		•			
,	COS		100		%		93-107	07-NOV-05
WG375519-6 DUP Alkalinity, Total (as Ca	CO3)	L338009-2 469	470		mg/L	0.16	3.8	07 101 0 0
Bicarbonate (HCO3)	•	572	573		mg/L	0.16	20	07-NOV-05
Carbonate (CO3)		<0.6	<0.6	RPD-NA	mg/L	0.10 N/A	20	07-NOV-05
Hydroxide (OH)		<0.4	<0.4	RPD-NA	mg/L	N/A	20	07-NOV-05
Batch R344368				,,,,,,	···· g·	WA	20	07-NOV-05
WG375934-5 CVS								
Alkalinity, Total (as Cat	CO3)		100		%		93-107	08-NOV-05
WG375934-6 DUP		L338009-1						
Alkalinity, Total (as Cat	CO3)	597	589		mg/L	1.3	3.8	08-NOV-05
Bicarbonate (HCO3)		728	719		mg/L	1.3	20	08-NOV-05
Carbonate (CO3)		<0.6	<0.6	RPD-NA	mg/L	N/A	20	08-NOV-05
Hydroxide (OH)		<0.4	<0.4	RPD-NA	mg/L	N/A	20	08-NOV-05
TX,TVH-WP	<u>Water</u>							
Batch R344763								
WG376384-1 CCV Benzene			89		0/			
Ethylbenzene			97		%		87-113	08-NOV-05
m+p-xylenes			96		%		87-113	08-NOV-05
o-xylene			97		%		87-113	08-NOV-05
Toluene			99		%		87-113	08-NOV-05
Total Volatiles			97		%		87-113	08-NOV-05
Xylenes			97 97		%		87-113	08-NOV-05
WG376384-2 CCV			97		%		70-130	08-NOV-05
Benzene CCV			89		%		07 449	00 NOV 05
Ethylbenzene			99		%		87-113 87-113	08-NOV-05
m+p-xylenes			98		%		87-113	08-NOV-05
o-xylene			100		%		87-113	08-NOV-05
Toluene			103		%		87-113	08-NOV-05
Total Volatiles			102		%		87-113 87-113	08-NOV-05
Xylenes			99		%		87-113 70-130	08-NOV-05
WG376384-3 CVS					,v		70-130	08-NOV-05

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Enviro-Test Quality Control Report

Test		Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
BTX,TVH-WP		Water		***************************************					
	344763								
WG376384-3 Ethylbenzene	cvs			91		%		87-113	08-NOV-05
m+p-xylenes				112		%		87-113	
o-xylene				93		%		87-113	
Toluene				95		%		87-113	
Total Volatiles				97		%		87-113	
Xylenes				102		%		70-130	08-NOV-05
WG376350-3 Benzene	DUP		L338009-4 <0.0005	<0.0005	RPD-NA	mg/L	N/A		
Ethylbenzene			<0.0005	<0.0005	RPD-NA	mg/L		12	08-NOV-05
m+p-xylenes			<0.0005	<0.0005	RPD-NA	mg/L	N/A	12	08-NOV-05
o-xylene			<0.0005	<0.0005	RPD-NA	mg/L	N/A	12	08-NOV-05
Toluene			<0.0005	<0.0005	RPD-NA	mg/L	N/A	12	08-NOV-05
Total Volatiles			<0.1	<0.1	RPD-NA	mg/L	N/A N/A	12	08-NOV-05
Xylenes			<0.0005	<0.0005	RPD-NA	mg/L		12	08-NOV-05
WG376350-1 Benzene	МВ				KED-NA	-	N/A	12	08-NOV-05
Ethylbenzene				<0.0005		mg/L		0.0005	08-NOV-05
m+p-xylenes				<0.0005		mg/L		0.0005	08-NOV-05
o-xylene				<0.0005		mg/L		0.0005	08-NOV-05
Toluene				<0.0005		mg/L		0.0005	08-NOV-05
Total Volatiles				<0.0005		mg/L		0.0005	08-NOV-05
Xylenes				<0.1		mg/L		0.1	08-NOV-05
WG376350-2				<0.0005		mg/L		0.0005	08-NOV-05
Benzene	MS		L338009-5	78	Н	%		82-117	08-NOV-05
Ethylbenzene				88		%		83-106	08-NOV-05
m+p-xylenes				108		%		86-112	08-NOV-05
o-xylene				91		%		83-110	08-NOV-05
Toluene				92		%		82-109	08-NOV-05
Total Volatiles				90		%		80-120	08-NOV-05
Xylenes				99		%		70-130	08-NOV-05
-DIS-WP		<u>Water</u>							30
atch R344	1055								
	CCV			107	Н	%		93-107	07-NOV-05
WG375512-2 (Chloride (CI) - Dis	CVS solved			106		%			
	ИВ							93-107	07-NOV-05
Chioride (Ci) - Dis	soivea			<9		mg/L		9	07-NOV-05

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Enviro-Test Quality Control Report

Test	Matrix	Reference	Result	. Qualifier	Units	RPD	Limit	Analyzed
				~~~	Amta		######################################	Analyzou
CL-SOL-WP Batch R3	<u>Water</u> 344055							
WG375512-3	CCV							
Chloride (CI) - S			107	Н	%		93-107	07-NOV-05
WG375512-2	cvs							
Chloride (Cl) - S	Soluble		106		%		93-107	07-NOV-05
WG375512-5 Chloride (Cl) - S	DUP	<b>WG375512-4</b> 131	131					
		131	131		mg/L	0.28	15	07-NOV-05
WG375512-1 Chloride (Cl) - S	<b>MB</b> Soluble		<9		mg/L		9	07-NOV-05
			-		··· <b>·</b> ••		<del>-</del>	01-140 V*00
CN-FREE-WP	<u>Water</u>							
Batch R3 WG375333-2	43922 CCV							
Cyanide, Free			97		%		87-113	07-NOV-05
WG375333-1	cvs							· ••
Cyanide, Free			98		%		87-113	07-NOV-05
WG375333-4	MB							
Cyanide, Free			<0.01		mg/L		0.01	07-NOV-05
WG375333-3	MS	L338027-1	104		· %			
Cyanide, Free			101	•	- 70		80-121	07-NOV-05
COD-WP	<u>Water</u>							
	44384							
WG375927-3 Chemical Oxyge	CCV en Demand		97		%		93-107	08-NOV-05
WG375927-2	cvs		= *		· ·		9J-10 <i>1</i>	00-140 V-00
Chemical Oxyge			95		%		93-107	08-NOV-05
WG375927-4	DUP	L336770-1						
Chemical Oxyge	en Demand	12	10	J	mg/L	2	25	08-NOV-05
WG375927-1	MB							
Chemical Oxyge	n Demand		<8		mg/L		8	08-NOV-05
C-WP	<u>Water</u>							
	4056							
WG375519-2 Conductivity	CCV		101		%		07.400	07.1014.07
-	CVE		101		/0		97-103	07-NOV-05
WG375519-1 Conductivity	cvs		100		%		93-107	07-NOV-05
•	DUP	L338009-2	•				00 101	37 110 V-00
Conductivity		1050	1040		umhos/cm	0.067	3.8	07-NOV-05
WG375519-7	DUP	L338046-1						
Conductivity		3970	3970		umhos/cm	0.14	3.8	07-NOV-05
Batch R344	4368							
WG375934-2	CCV							
Conductivity			101		%		97-103	08-NOV-05
WG375934-1	cvs							

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
EC-WP	Water							
Batch R344368 WG375934-1 CVS Conductivity			99		%		93-107	08-NOV-05
WG375934-6 DUP Conductivity		<b>L338009-1</b> 1330	1330		umhos/cm	0.023	3.8	08-NOV-05
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R344974								
WG376632-4 CCV								
Aluminum (Al)-Total			102		%		93-107	09-NOV-05
Antimony (Sb)-Total			99		%		93-107	09-NOV-05
Arsenic (As)-Total			98		%		93-107	09-NOV-05
Barium (Ba)-Total			96		%		93-107	09-NOV-05
Beryllium (Be)-Total			98		%		93-107	09-NOV-05
Bismuth (Bi)-Total			102		%		93-107	09-NOV-05
Boron (B)-Total			94		%		93-107	09-NOV-05
Cadmium (Cd)-Total			98		%		93-107	09-NOV-05
Calcium (Ca)-Total			99		%		93-107	09-NOV-05
Cesium (Cs)-Total			98		%		93-107	09-NOV-05
Chromium (Cr)-Total			101		%		93-107	09-NOV-05
Cobalt (Co)-Total			98		%		93-107	09-NOV-05
Copper (Cu)-Total			98		%		93-107	09-NOV-05
Iron (Fe)-Total			99		%		93-107	09-NOV-05
Lead (Pb)-Total			100		%		93-107	09-NOV-05
Lithium (Li)-Total			95		%		93-107	09-NOV-05
Magnesium (Mg)-Total			102		%		93-107	09-NOV-05
Manganese (Mn)-Total			98		%		93-107	09-NOV-05
Molybdenum (Mo)-Total			100		%		93-107	09-NOV-05
Nickel (Ni)-Total			99		%		93-107	09-NOV-05
Phosphorus (P)-Total			100		%		93-107	09-NOV-05
Potassium (K)-Total			98		%		93-107	09-NOV-05
Rubidium (Rb)-Total			100		%		93-107	09-NOV-05
Selenium (Se)-Total			95		%		93-107	09-NOV-05
Silver (Ag)-Total			99		%		93-107	09-NOV-05
Sodium (Na)-Total			104		%		93-107	09-NOV-05
Strontium (Sr)-Total			99		%		93-107	09-NOV-05
Tellurium (Te)-Total			99		%		93-107	09-NOV-05
Thallium (TI)-Total			102		%		93-107	09-NOV-05
Tin (Sn)-Total			99		%		93-107	09-NOV-05
Titanium (Ti)-Total			99		%		93-107	09-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R344974								
WG376632-4 CCV Tungsten (W )-Total			99	0	,			
Uranium (U)-Total			101	9			93-107	09-NOV-05
Vanadium (V)-Total			101	9			93-107	09-NOV-05
Zinc (Zn)-Total			99	9,			93-107	09-NOV-05
Zirconium (Zr)-Total			100	9/			93-107	09-NOV-05
WG376632-2 CVS			100	%	0		93-107	09-NOV-05
Aluminum (Al)-Total			94	%	,		75-125	09-NOV-05
Antimony (Sb)-Total			94	%			75-125	09-NOV-05
Arsenic (As)-Total			94	%			75-125	
Barium (Ba)-Total			94	%			75-125 75-125	09-NOV-05 09-NOV-05
Beryllium (Be)-Total			99	%			75-125 75-125	09-NOV-05
Bismuth (Bi)-Total			95	%			75-125	09-NOV-05
Boron (B)-Total			97	%			75-125	09-NOV-05
Cadmium (Cd)-Total			94	%			75-125	09-NOV-05
Calcium (Ca)-Total			93	%			75-125	09-NOV-05
Cesium (Cs)-Total			95	%			75-125	09-NOV-05
Chromium (Cr)-Total			93	%			75-125	09-NOV-05
Cobalt (Co)-Total			95	%			75-125	09-NOV-05
Copper (Cu)-Total			95	%			75-125	09-NOV-05
Iron (Fe)-Total			93	%			75-125	09-NOV-05
Lead (Pb)-Total			96	%			75-125	09-NOV-05
Lithium (Li)-Total			103	%			75-125	09-NOV-05
Magnesium (Mg)-Total			95	%			75-125	09-NOV-05
Manganese (Mn)-Total			95	%			75-125	09-NOV-05
Molybdenum (Mo)-Total			95	%			75-125	09-NOV-05
Nickel (Ni)-Total			94	%			75-125	09-NOV-05
Phosphorus (P)-Total			92	%			75-125	09-NOV-05
Potassium (K)-Total			94	%			75-125	09-NOV-05
Rubidium (Rb)-Total			96	%			75-125	09-NOV-05
Selenium (Se)-Total			95	%			75-125	09-NOV-05
Silver (Ag)-Total			99	%			75-125	09-NOV-05
Sodium (Na)-Total			94	%			75-125	09-NOV-05
Strontium (Sr)-Total			96	%			75-125	09-NOV-05
Tellurium (Te)-Total			95	%			75-125	09-NOV-05
Thallium (TI)-Total			96	%			75-125	09-NOV-05
Tin (Sn)-Total			95	%			75-125	09-NOV-05
Titanium (Ti)-Total			94	%			75-125	09-NOV-05

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# **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R344974								
WG376632-2 CVS Tungsten (W )-Total			00		Δ.			
Uranium (U)-Total			96 96		%		75-125	09-NOV-05
Vanadium (V)-Total					%		75-125	09-NOV-05
Zinc (Zn)-Total			101		%		75-125	09-NOV-05
Zirconium (Zr)-Total			92		%		75-125	09-NOV-05
• •			96		%		75-125	09-NOV-05
WG376632-3 CVS Aluminum (AI)-Total			91		%		75-125	09-NOV-05
Antimony (Sb)-Total			95		%		75-125	09-NOV-05
Arsenic (As)-Total			96		%		75-125	09-NOV-05
Barium (Ba)-Total			97		%		75-125	09-NOV-05
Beryllium (Be)-Total			105		%		75-125	09-NOV-05
Bismuth (Bi)-Total			95		%		75-125	09-NOV-05
Boron (B)-Total			98		%		75-125	09-NOV-05
Cadmium (Cd)-Total			98		%		75-125	09-NOV-05
Calcium (Ca)-Total			97		%		75-125	09-NOV-05
Cesium (Cs)-Total			92		%		75-125	09-NOV-05
Chromium (Cr)-Total			97		%		75-125	09-NOV-05
Cobalt (Co)-Total			97		%		75-125	09-NOV-05
Copper (Cu)-Total			96		%		75-125	09-NOV-05
Iron (Fe)-Total			96		%		75-125	09-NOV-05
Lead (Pb)-Total			97		%		75-125	09-NOV-05
Lithium (Li)-Total			107		%		75-125	09-NOV-05
Magnesium (Mg)-Total			97		%		75-125	09-NOV-05
Manganese (Mn)-Total			97		%		75-125	09-NOV-05
Molybdenum (Mo)-Total			101		%		75-125	09-NOV-05
Nickel (Ni)-Total			97		%		75-125	09-NOV-05
Phosphorus (P)-Total			97		%		75-125	09-NOV-05
Potassium (K)-Total			97		%		75-125	09-NOV-05
Rubidium (Rb)-Total			100		%		75-125	09-NOV-05
Selenium (Se)-Total			96		%		75-125	09-NOV-05
Silver (Ag)-Total			106		%		75-125	09-NOV-05
Sodium (Na)-Total			95		%		75-125	09-NOV-05
Strontium (Sr)-Total			100		%		75-125	09-NOV-05
Tellurium (Te)-Total			96		%		75-125	09-NOV-05
Thallium (TI)-Total			96		%		75-125	09-NOV-05
Tin (Sn)-Total			101		%		75-125	09-NOV-05
Titanium (Ti)-Total			99		%		75-125	09-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R344974								
WG376632-3 CVS Tungsten (W )-Total			99		%		75-125	09-NOV-05
Uranium (U)-Total			102		%		75-125	09-NOV-05
Vanadium (V)-Total			105		%		75-125	09-NOV-05
Zinc (Zn)-Total			94		%		75-125	09-NOV-05
Zirconium (Zr)-Total			100		%		75-125	09-NOV-05
WG376308-4 DUP		WG376308-3						001101 00
Aluminum (Al)-Total		0.24	0.24		mg/L	3.4	15	10-NOV-05
Antimony (Sb)-Total		0.001	0.001	J	mg/L	0.000	0.0031	10-NOV-05
Arsenic (As)-Total		<0.0005	<0.0005	RPD-NA	mg/L	N/A	15	10-NOV-05
Barium (Ba)-Total		0.0121	0.0144	Н	mg/L	18	15	10-NOV-05
Beryllium (Be)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Bismuth (Bi)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Boron (B)-Total		<0.03	<0.03	RPD-NA	mg/L	N/A	15	10-NOV-05
Cadmium (Cd)-Total		0.0012	0.0013	J	mg/L	0.0001	0.00061	10-NOV-05
Calcium (Ca)-Total		23.1	24.7		mg/L	6.7	15	10-NOV-05
Cesium (Cs)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Chromium (Cr)-Total		0.001	0.002	J	mg/L	0.001	0.0031	10-NOV-05
Cobalt (Co)-Total		0.0004	0.0004	J	mg/L	0.0000	0.00061	10-NOV-05
Copper (Cu)-Total		0.010	0.012		mg/L	14	15	10-NOV-05
Iron (Fe)-Total		0.23	0.23	J	mg/L	0.01	0.15	10-NOV-05
Lead (Pb)-Total		0.0014	0.0016	J	mg/L	0.0002	0.0015	10-NOV-05
Lithium (Li)-Total		<0.01	<0.01	RPD-NA	mg/L	N/A	15	10-NOV-05
Magnesium (Mg)-Total		4.61	4.86		mg/L	5.4	15	10-NOV-05
Manganese (Mn)-Total		0.0346	0.0372		mg/L	7.4	15	10-NOV-05
Molybdenum (Mo)-Total		<0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Nickel (Ni)-Total		0.010	0.010	J	mg/L	0.000	0.0061	10-NOV-05
Phosphorus (P)-Total		0.10	0.11	J	mg/L	0.02	0.15	10-NOV-05
Potassium (K)-Total		1.2	1.3		mg/L	14	15	10-NOV-05
Rubidium (Rb)-Total		0.0010	0.0013	J	mg/L	0.0003	0.00061	10-NOV-05
Selenium (Se)-Total		0.003	0.002	J	mg/L	0.000	0.0031	10-NOV-05
Silver (Ag)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Sodium (Na)-Total		3.05	3.23		mg/L	5.8	15	10-NOV-05
Strontium (Sr)-Total		0.0389	0.0416		mg/L	6.8	15	10-NOV-05
Tellurium (Te)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Thallium (TI)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Tin (Sn)-Total		0.0047	0.0053	J	mg/L	0.0006	0.0018	10-NOV-05
Titanium (Ti)-Total		0.0060	0.0093	J,H	mg/L	0.0033	0.0028	10-NOV-05

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# **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water							
Batch R344974								
WG376308-4 DUP Tungsten (W )-Total		<b>WG376308-3</b> <0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Uranium (U)-Total		0.0001	0.0001	J	mg/L	0.0000	0.00031	
Vanadium (V)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Zinc (Zn)-Total		0.17	0.20	Н	mg/L	16	15	10-NOV-05
Zirconium (Zr)-Total		<0.0004	0.0005	RPD-NA	mg/L	N/A	15	10-NOV-05
WG376308-2 LCS Aluminum (Al)-Total			102		%			
Antimony (Sb)-Total			92		%		80-120	09-NOV-05
Arsenic (As)-Total			94		%		80-120	09-NOV-05
Barium (Ba)-Total			96		%		80-120	09-NOV-05
Beryllium (Be)-Total			96		%		80-120	09-NOV-05
Bismuth (Bi)-Total			98		%		80-120	09-NOV-05
Boron (B)-Total			89		%		80-120 80-120	09-NOV-05
Cadmium (Cd)-Total			94		%		89-112	09-NOV-05 09-NOV-05
Calcium (Ca)-Total			100		%		80-112	09-NOV-05
Cesium (Cs)-Total			97		%		80-120	09-NOV-05
Chromium (Cr)-Total			97		%		80-120	09-NOV-05
Cobalt (Co)-Total			96		%		80-120	09-NOV-05
Copper (Cu)-Total			98		%		92-121	09-NOV-05
iron (Fe)-Total			96		%		80-120	09-NOV-05
Lead (Pb)-Total			98		%		91-117	09-NOV-05
Lithium (Li)-Total			91		%		80-120	09-NOV-05
Magnesium (Mg)-Total			100		%		92-120	09-NOV-05
Manganese (Mn)-Total			96		%		80-120	09-NOV-05
Molybdenum (Mo)-Total			98		%		80-120	09-NOV-05
Nickel (Ni)-Total			96		%		80-120	09-NOV-05
Phosphorus (P)-Total			105		%		73-127	09-NOV-05
Potassium (K)-Total			92		%		80-120	09-NOV-05
Rubidium (Rb)-Total			97		%		80-120	09-NOV-05
Selenium (Se)-Total			92		%		80-120	09-NOV-05
Silver (Ag)-Total			97		%		80-120	09-NOV-05
Sodium (Na)-Total			91		%		80-120	09-NOV-05
Strontium (Sr)-Total			97		%		80-120	09-NOV-05
Tellurium (Te)-Total			92		%		80-120	09-NOV-05
Thallium (TI)-Total			99		%		80-120	09-NOV-05
Tin (Sn)-Total			97		%		80-120	09-NOV-05
Titanium (Ti)-Total			99		%		80-120	09-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water							
Batch R344974								
WG376308-2 LCS Tungsten (W )-Total			97		%		80-120	09-NOV-05
Uranium (U)-Total			100		%		80-120	09-NOV-05
Vanadium (V)-Total			96		%		80-120	09-NOV-05
Zinc (Zn)-Total		•	105		%		83-126	09-NOV-05
Zirconium (Zr)-Total			96		%		80-120	09-NOV-05
WG376308-1 MB Aluminum (Al)-Total			<0.02		mg/L		0.1	09-NOV-05
Antimony (Sb)-Total			<0.001		mg/L		0.005	09-NOV-05
Arsenic (As)-Total			<0.0005		mg/L		0.0025	09-NOV-05
Barium (Ba)-Total			<0.0003		mg/L		0.0015	09-NOV-05
Beryllium (Be)-Total			<0.001		mg/L		0.005	09-NOV-05
Bismuth (Bi)-Total			<0.0001		mg/L		0.0005	09-NOV-05
Boron (B)-Total			<0.03		mg/L		0.15	09-NOV-05
Cadmium (Cd)-Total			<0.0002		mg/L		0.001	09-NOV-05
Calcium (Ca)-Total			<0.1		mg/L		0.5	09-NOV-05
Cesium (Cs)-Total			<0.0001		mg/L		0.0005	09-NOV-05
Chromium (Cr)-Total			<0.001		mg/L		0.005	09-NOV-05
Cobalt (Co)-Total			<0.0002		mg/L		0.001	09-NOV-05
Copper (Cu)-Total			<0.001		mg/L		0.005	09-NOV-05
Iron (Fe)-Total			<0.05		mg/L		0.25	09-NOV-05
Lead (Pb)-Total			<0.0005		mg/L		0.0025	09-NOV-05
Lithium (Li)-Total			<0.01		mg/L		0.05	09-NOV-05
Magnesium (Mg)-Total			<0.01		mg/L		0.05	09-NOV-05
Manganese (Mn)-Total			<0.0003		mg/L		0.0015	09-NOV-05
Molybdenum (Mo)-Total			<0.0002		mg/L		0.001	09-NOV-05
Nickel (Ni)-Total			<0.002		mg/L		0.01	09-NOV-05
Phosphorus (P)-Total			<0.05		mg/L		0.25	09-NOV-05
Potassium (K)-Total			<0.1		mg/L		0.5	09-NOV-05
Rubidium (Rb)-Total			<0.0002		mg/L		0.001	09-NOV-05
Selenium (Se)-Total			<0.001		mg/L		0.005	09-NOV-05
Silver (Ag)-Total			<0.001		mg/L		0.005	09-NOV-05
Sodium (Na)-Total			<0.03		mg/L		0.15	09-NOV-05
Strontium (Sr)-Total			<0.0001		mg/L		0.0005	09-NOV-05
Tellurium (Te)-Total			<0.001		mg/L		0.005	09-NOV-05
Thallium (TI)-Total			<0.0001		mg/L		0.0005	09-NOV-05
Tin (Sn)-Total			<0.0006		mg/L		0.003	09-NOV-05
Titanium (Ti)-Total			<0.0009		mg/L		0.0045	09-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R344974								
WG376308-1 MB Tungsten (W )-Total			<0.0002		m a /i		0.004	
Uranium (U)-Total			<0.0002		mg/L mg/L		0.001	09-NOV-05
Vanadium (V)-Total			<0.0001		-		0.0005	09-NOV-05
Zinc (Zn)-Total			<0.001		mg/L mg/L		0.005 0.05	09-NOV-05
Zirconium (Zr)-Total			<0.004		mg/L		0.00	09-NOV-05
			-0.000-4		mg/L		0.002	09-NOV-05
Batch R345886 WG377806-4 CCV								
Aluminum (AI)-Total			100		%		93-107	10-NOV-05
Antimony (Sb)-Total			98		%		93-107	10-NOV-05
Arsenic (As)-Total			98		%		93-107	10-NOV-05
Barium (Ba)-Total			98		%		93-107	10-NOV-05
Beryllium (Be)-Total			96		%		93-107	10-NOV-05
Bismuth (Bi)-Total			101		%		93-107	10-NOV-05
Boron (B)-Total			98		%		93-107	10-NOV-05
Cadmium (Cd)-Total			99		%		93-107	10-NOV-05
Calcium (Ca)-Total			100		%		93-107	10-NOV-05
Cesium (Cs)-Total			100		%		93-107	10-NOV-05
Chromium (Cr)-Total			101		%		93-107	10-NOV-05
Cobalt (Co)-Total			100		%		93-107	10-NOV-05
Copper (Cu)-Total			99		%		93-107	10-NOV-05
Iron (Fe)-Total			101		%		93-107	10-NOV-05
Lead (Pb)-Total			99		%		93-107	10-NOV-05
Lithium (Li)-Total			98		%		93-107	10-NOV-05
Magnesium (Mg)-Total			99		%		93-107	10-NOV-05
Manganese (Mn)-Total			99		%		93-107	10-NOV-05
Molybdenum (Mo)-Total			98		%		93-107	10-NOV-05
Nickel (Ni)-Total			99		%		93-107	10-NOV-05
Phosphorus (P)-Total			98		%		93-107	10-NOV-05
Potassium (K)-Total			99		%		93-107	10-NOV-05
Rubidium (Rb)-Total			97		%		93-107	10-NOV-05
Selenium (Se)-Total			99		%		93-107	10-NOV-05
Silver (Ag)-Total			98		%		93-107	10-NOV-05
Sodium (Na)-Total			101		%		93-107	10-NOV-05
Strontium (Sr)-Total			97		%		93-107	10-NOV-05
Tellurium (Te)-Total			99		%		93-107	10-NOV-05
Thallium (TI)-Total			101		%		93-107	10-NOV-05
Tin (Sn)-Total			97		%		93-107	10-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water							
Batch R345886								
WG377806-4 CCV								
Titanium (Ti)-Total			97		%		93-107	10-NOV-05
Tungsten (W )-Total			99		%		93-107	10-NOV-05
Uranium (U)-Total			100		%		93-107	10-NOV-05
Vanadium (V)-Total			99		%		93-107	10-NOV-05
Zinc (Zn)-Total			100		%		93-107	10-NOV-05
Zirconium (Zr)-Total			98		%		93-107	10-NOV-05
WG377806-2 CVS Aluminum (Al)-Total			96		%		75-125	10-NOV-05
Antimony (Sb)-Total			101		%		75-125	10-NOV-05
Arsenic (As)-Total			97		%		75-125	10-NOV-05
Barium (Ba)-Total			96		%		75-125	10-NOV-05
Beryllium (Be)-Total			99		%		75-125	10-NOV-05
Bismuth (Bi)-Total			98		%		75-125	10-NOV-05
Boron (B)-Total			105		%		75-125	10-NOV-05
Cadmium (Cd)-Total			96		%		75-125	10-NOV-05
Calcium (Ca)-Total			97		%		75-125	10-NOV-05
Cesium (Cs)-Total			99		%		75-125	10-NOV-05
Chromium (Cr)-Total			97		%		75-125	10-NOV-05
Cobalt (Co)-Total			97		%		75-125	10-NOV-05
Copper (Cu)-Total			97		%		75-125	10-NOV-05
Iron (Fe)-Total			97		%		75-125	10-NOV-05
Lead (Pb)-Total			99		%		75-125	10-NOV-05
Lithium (Li)-Total			95		%		75-125	10-NOV-05
Magnesium (Mg)-Total			98		%		75-125	10-NOV-05
Manganese (Mn)-Total			98		%		75-125	10-NOV-05
Molybdenum (Mo)-Total			97		%		75-125	10-NOV-05
Nickel (Ni)-Total			96		%		75-125	10-NOV-05
Phosphorus (P)-Total			97		%		75-125	10-NOV-05
Potassium (K)-Total			97		%		75-125	10-NOV-05
Rubidium (Rb)-Total			97		%		75-125	10-NOV-05
Selenium (Se)-Total			97		%		75-125	10-NOV-05
Silver (Ag)-Total			96		%		75-125	10-NOV-05
Sodium (Na)-Total			98		%		75-125	10-NOV-05
Strontium (Sr)-Total			97		%		75-125	10-NOV-05
Tellurium (Te)-Total			98		%		75-125	10-NOV-05
Thallium (TI)-Total			100		%		75-125	10-NOV-05
Tin (Sn)-Total			96		%		75-125	10-NOV-05

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# **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water							
Batch R345886								
WG377806-2 CVS								
Titanium (Ti)-Total			95		%		75-125	10-NOV-05
Tungsten (W )-Total			98		%		75-125	10-NOV-05
Uranium (U)-Total Vanadium (V)-Total			98		%		75-125	10-NOV-05
Zinc (Zn)-Total			96		%		75-125	10-NOV-05
Zirconium (Zr)-Total			96		%		75-125	10-NOV-05
			96		%		75-125	10-NOV-05
WG377806-3 CVS Aluminum (AI)-Total			95		%		75-125	10-NOV-05
Antimony (Sb)-Total			99		%		75-125 75-125	
Arsenic (As)-Total			99		%		75-125 75-125	10-NOV-05 10-NOV-05
Barium (Ba)-Total			98		%		75-125 75-125	10-NOV-05 10-NOV-05
Beryllium (Be)-Total			96		%		75-125 75-125	10-NOV-05
Bismuth (Bi)-Total			97		%		75-125 75-125	10-NOV-05
Boron (B)-Total			96		%		75-125 75-125	10-NOV-05
Cadmium (Cd)-Total			98		%		75-125	10-NOV-05
Calcium (Ca)-Total			100		%		75-125	10-NOV-05
Cesium (Cs)-Total			96		%		75-125	10-NOV-05
Chromium (Cr)-Total			100		%		75-125	10-NOV-05
Cobalt (Co)-Total			99		%		75-125	10-NOV-05
Copper (Cu)-Total			97		%		75-125	10-NOV-05
Iron (Fe)-Total			99		%		75-125	10-NOV-05
Lead (Pb)-Total			100		%		75-125	10-NOV-05
Lithium (Li)-Total			97		%		75-125	10-NOV-05
Magnesium (Mg)-Total			99		%		75-125	10-NOV-05
Manganese (Mn)-Total			100		%		75-125	10-NOV-05
Molybdenum (Mo)-Total			99		%		75-125	10-NOV-05
Nickel (Ni)-Total			100		%		75-125	10-NOV-05
Phosphorus (P)-Total			99		%		75-125	10-NOV-05
Potassium (K)-Total			101		%		75-125	10-NOV-05
Rubidium (Rb)-Total			98		%		75-125	10-NOV-05
Selenium (Se)-Total			99		%		75-125	10-NOV-05
Silver (Ag)-Total			102		%		75-125	10-NOV-05
Sodium (Na)-Total			99		%		75-125	10-NOV-05
Strontium (Sr)-Total			100	1	%		75-125	10-NOV-05
Tellurium (Te)-Total			98	•	%		75-125	10-NOV-05
Thallium (TI)-Total			98	•	%		75-125	10-NOV-05
Tin (Sn)-Total			97	·	%		75-125	10-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water	***************************************					***************************************	
Batch R345886								
WG377806-3 CVS			00		04			
Titanium (Ti)-Total Tungsten (W)-Total			99 100		%		75-125	10-NOV-05
Uranium (U)-Total			100		%		75-125	10-NOV-05
Vanadium (V)-Total					%		75-125	10-NOV-05
Zinc (Zn)-Total			100		%		75-125	10-NOV-05
, ,			97		%		75-125	10-NOV-05
Zirconium (Zr)-Total			99		%		75-125	10-NOV-05
WG376937-4 DUP Aluminum (AI)-Total		<b>WG376937-3</b> 0.08	0.09	J	mg/L	0.01	0.061	10-NOV-05
Antimony (Sb)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Arsenic (As)-Total		0.0037	0.0039	J	mg/L	0.0002	0.0015	10-NOV-05
Barium (Ba)-Total		0.0070	0.0069		mg/L	1.2	15	10-NOV-05
Beryllium (Be)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Bismuth (Bi)-Total		0.0001	0.0001	j	mg/L	0.0000	0.00031	10-NOV-05
Boron (B)-Total		<0.03	<0.03	RPD-NA	mg/L	N/A	15	10-NOV-05
Cadmium (Cd)-Total		<0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Calcium (Ca)-Total		7.2	7.4		mg/L	2.1	15	10-NOV-05
Cesium (Cs)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Chromium (Cr)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Cobalt (Co)-Total		<0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Copper (Cu)-Total		<0.001	0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Iron (Fe)-Total		0.10	0.11	J	mg/L	0.00	0.15	10-NOV-05
Lead (Pb)-Total		<0.0005	<0.0005	RPD-NA	mg/L	N/A	15	10-NOV-05
Lithium (Li)-Total		<0.01	<0.01	RPD-NA	mg/L	N/A	15	10-NOV-05
Magnesium (Mg)-Total		1.94	1.97		mg/L	1.7	15	10-NOV-05
Manganese (Mn)-Total		0.0058	0.0060		mg/L	4.2	15	10-NOV-05
Molybdenum (Mo)-Total		<0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Nickel (Ni)-Total		<0.002	<0.002	RPD-NA	mg/L	N/A	15	10-NOV-05
Phosphorus (P)-Total		0.14	0.12	J	mg/L	0.01	0.15	10-NOV-05
Potassium (K)-Total		0.8	0.8	J	mg/L	0.0	0.31	10-NOV-05
Rubidium (Rb)-Total		0.0014	0.0015	J	mg/L	0.0001	0.00061	10-NOV-05
Selenium (Se)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Silver (Ag)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Sodium (Na)-Total		1.43	1.45		mg/L	1.4	15	10-NOV-05
Strontium (Sr)-Total		0.0202	0.0209		mg/L	3.7	15	10-NOV-05
Tellurium (Te)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Thallium (TI)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Tin (Sn)-Total		<0.0006	<0.0006	RPD-NA	mg/L	N/A	15	10-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	<u>Water</u>							
Batch R345886								
WG376937-4 DUP Titanium (Ti)-Total		<b>WG376937-3</b> 0.0010	0.0013	J	mg/L	0.0002	0.0028	10-NOV-05
Tungsten (W)-Total		<0.0002	<0.0002	RPD-NA	mg/L	N/A	15	10-NOV-05
Uranium (U)-Total		<0.0001	<0.0001	RPD-NA	mg/L	N/A	15	10-NOV-05
Vanadium (V)-Total		<0.001	<0.001	RPD-NA	mg/L	N/A	15	10-NOV-05
Zinc (Zn)-Total		0.01	0.01	J	mg/L	0.00	0.031	10-NOV-05
Zirconium (Zr)-Total		0.0007	0.0005	J	mg/L	0.0002	0.0012	10-NOV-05
WG376937-2 LCS Aluminum (Al)-Total			106		%		80-120	10-NOV-05
Antimony (Sb)-Total			96		%		80-120	10-NOV-05
Arsenic (As)-Total			95		%		80-120	10-NOV-05
Barium (Ba)-Total			96		%		80-120	10-NOV-05
Beryllium (Be)-Total			93		%		80-120	10-NOV-05
Bismuth (Bi)-Total			97		%		80-120	10-NOV-05
Boron (B)-Total			98		%		80-120	10-NOV-05
Cadmium (Cd)-Total			93		%		89-112	10-NOV-05
Calcium (Ca)-Total			100		%		80-120	10-NOV-05
Cesium (Cs)-Total			98		%		80-120	10-NOV-05
Chromium (Cr)-Total			99		%		80-120	10-NOV-05
Cobalt (Co)-Total			99		%		80-120	10-NOV-05
Copper (Cu)-Total			100		%		92-121	10-NOV-05
Iron (Fe)-Total			99		%		80-120	10-NOV-05
Lead (Pb)-Total			99		%		91-117	10-NOV-05
Lithium (Li)-Total			89		%		80-120	10-NOV-05
Magnesium (Mg)-Total			100		%		92-120	10-NOV-05
Manganese (Mn)-Total			99		%		80-120	10-NOV-05
Molybdenum (Mo)-Total			97		%		80-120	10-NOV-05
Nickel (Ni)-Total			101		%		80-120	10-NOV-05
Phosphorus (P)-Total			126		%		73-127	10-NOV-05
Potassium (K)-Total			97		%		80-120	10-NOV-05
Rubidium (Rb)-Total			98		%		80-120	10-NOV-05
Selenium (Se)-Total			91		%		80-120	10-NOV-05
Silver (Ag)-Total			92		%		80-120	10-NOV-05
Sodium (Na)-Total			102		%		80-120	10-NOV-05
Strontium (Sr)-Total			98		%		80-120	10-NOV-05
Tellurium (Te)-Total			91		%		80-120	10-NOV-05
Thallium (TI)-Total			98		%		80-120	10-NOV-05
Tin (Sn)-Total			97		%		80-120	10-NOV-05

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## **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-WP	Water							
Batch R345886								
WG376937-2 LCS Titanium (Ti)-Total			95		%		80-120	10-NOV-05
Tungsten (W)-Total			97		%		80-120	10-NOV-05
Uranium (U)-Total			98		%		80-120	10-NOV-05
Vanadium (V)-Total			98		%		80-120	10-NOV-05
Zinc (Zn)-Total			96		%		83-126	10-NOV-05
Zirconium (Zr)-Total			96		%		80-120	10-NOV-05
WG376937-1 MB							00 .20	10-110-03
Aluminum (AI)-Total			<0.02		mg/L		0.1	10-NOV-05
Antimony (Sb)-Total			<0.001		mg/L		0.005	10-NOV-05
Arsenic (As)-Total			<0.0005		mg/L		0.0025	10-NOV-05
Barium (Ba)-Total			<0.0003		mg/L		0.0015	10-NOV-05
Beryllium (Be)-Total			<0.001		mg/L		0.005	10-NOV-05
Bismuth (Bi)-Total			<0.0001		mg/L		0.0005	10-NOV-05
Boron (B)-Total			<0.03		mg/L		0.15	10-NOV-05
Cadmium (Cd)-Total			<0.0002		mg/L		0.001	10-NOV-05
Calcium (Ca)-Total			<0.1		mg/L		0.5	10-NOV-05
Cesium (Cs)-Total			<0.0001		mg/L		0.0005	10-NOV-05
Chromium (Cr)-Total			<0.001		mg/L		0.005	10-NOV-05
Cobalt (Co)-Total			<0.0002		mg/L		0.001	10-NOV-05
Copper (Cu)-Total			<0.001		mg/L		0.005	10-NOV-05
Iron (Fe)-Total			<0.05		mg/L		0.25	10-NOV-05
Lead (Pb)-Total			<0.0005		mg/L		0.0025	10-NOV-05
Lithium (Li)-Total			<0.01		mg/L		0.05	10-NOV-05
Magnesium (Mg)-Total			<0.01		mg/L		0.05	10-NOV-05
Manganese (Mn)-Total			<0.0003		mg/L		0.0015	10-NOV-05
Molybdenum (Mo)-Total			<0.0002		mg/L		0.001	10-NOV-05
Nickel (Ni)-Total			<0.002		mg/L		0.01	10-NOV-05
Phosphorus (P)-Total			<0.05		mg/L		0.25	10-NOV-05
Potassium (K)-Total			<0.1		mg/L		0.5	10-NOV-05
Rubidium (Rb)-Total			<0.0002		mg/L		0.001	10-NOV-05
Selenium (Se)-Total			<0.001		mg/L		0.005	10-NOV-05
Silver (Ag)-Total			<0.001		mg/L		0.005	10-NOV-05
Sodium (Na)-Total			<0.03		mg/L		0.15	10-NOV-05
Strontium (Sr)-Total			<0.0001		mg/L		0.0005	10-NOV-05
Tellurium (Te)-Total			<0.001		mg/L		0.005	10-NOV-05
Thallium (TI)-Total			<0.0001		mg/L		0.0005	10-NOV-05
Tin (Sn)-Total			<0.0006		mg/L		0.003	10-NOV-05

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## **Enviro-Test Quality Control Report**

				vvorkorder	. L336009			
Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MET-SCAN-TOT-LOW-W	<u>P Water</u>							
Batch R345886								
WG376937-1 MB Titanium (Ti)-Total			<0.0009		mg/L		0.0045	40 NOV 05
Tungsten (W )-Total			<0.0002		mg/L		0.0043	10-NOV-05 10-NOV-05
Uranium (U)-Total			<0.0001		mg/L		0.0005	10-NOV-05
Vanadium (V)-Total			<0.001		mg/L		0.005	10-NOV-05
Zinc (Zn)-Total			<0.01		mg/L		0.05	10-NOV-05
Zirconium (Zr)-Total			<0.0004		mg/L		0.002	10-NOV-05
N-TOTKJ-WP	Water							,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Batch R346542	<del></del>							
WG378469-2 CCV								
Total Kjeldahl Nitrogen	1		102		%		93-107	15-NOV-05
WG378469-1 CVS Total Kjeldahl Nitrogen			101		%		00.407	45.145.455
WG376780-5 DUP		WG376780-4	101		70		93-107	15-NOV-05
Total Kjeldahl Nitrogen		2.7	2.7		mg/L	0.73	20	15-NOV-05
WG376780-2 LCS								
Total Kjeldahl Nitrogen			99		%		79-115	15-NOV-05
WG376780-1 MB Total Kjeldahl Nitrogen			<0.2					
WG376780-3 MS		1 220200 40	<0.2		mg/L		0.2	15-NOV-05
Total Kjeldahl Nitrogen		L339266-12	102	E	%		79-115	15-NOV-05
N2N3-DIS-WP	Water						70 1,0	10 110 1-00
Batch R344055								
WG375512-3 CCV								
Nitrate+Nitrite-N - Disso	olved		97		%		93-107	07-NOV-05
WG375512-2 CVS Nitrate+Nitrite-N - Disso	lved		105		%			
WG375150-1 MB	ived		105		70		93-107	07-NOV-05
Nitrate+Nitrite-N - Disso	ived		0.02		mg/L		0.05	07-NOV-05
N2N3-SOL-WP	Water				•			07 110 7 00
Batch R344055								
WG375512-3 CCV								
Nitrate+Nitrite-N			97		%		93-107	07-NOV-05
WG375512-2 CVS					•			
Nitrate+Nitrite-N			105		%		93-107	07-NOV-05
WG375512-5 DUP Nitrate+Nitrite-N		<b>WG375512-4</b> 0.50	0.50		mg/L	0.078	15	07-NOV-05
WG375512-1 MB			•		· · · · · ·	5.576		07-140 V-03
Nitrate+Nitrite-N			0.02		mg/L		0.05	07-NOV-05
H3-DIS-WP	<u>Water</u>							

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### **Enviro-Test Quality Control Report**

Matrix						vvorkoraer	. L330009			
Batch   R344055   WG375812-3   CVS   MB   MB   MB   MB   MB   MB   MB   M	Test		Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
MG375513-1   MB	NH3-DIS-WP		Water						· · · · · · · · · · · · · · · · · · ·	
MG375519-1   Ammonia (NH-1)   Dissolved   98   %   99-107   O7-NOV-05	WG375512-3	CCV	olved		100		%		93-107	07-NOV-05
Note			olved		98		%			
Batch   R345178   WG376628-1   CCV   Total Phosphorous   99   76   93-107   10-NOV-05   WG376628-2   CCV   Total Phosphorous   99   76   93-107   10-NOV-05   WG376628-2   CCV   Total Phosphorous   99   76   93-107   10-NOV-05   WG376427-2   CVS   70tal Phosphorous   94   76   93-107   10-NOV-05   WG376427-3   CVS   70tal Phosphorous   94   76   93-107   10-NOV-05   WG376427-3   CVS   70tal Phosphorous   94   76   77.1   77   10-NOV-05   WG376427-4   DUP   L338005-1   70-NOV-05   WG376427-1   MB   70tal Phosphorous   0.363   0.338   mg/L   7.1   17   10-NOV-05   WG376427-1   MB   70tal Phosphorous   0.363   0.338   mg/L   7.1   17   10-NOV-05   WG376427-1   MB   70tal Phosphorous   0.363   0.305   mg/L   7.1   17   10-NOV-05   WG376427-1   MB   70tal Phosphorous   70-NOV-05   WG376427-1   MB   70tal Phosphorous   70-NOV-05   WG376427-1   MB   70tal Phosphorous   70-NOV-05   WG375427-1   MB   70tal Phosphorous   70-NOV-05   WG375427-1   MB   70tal Phosphorous   70-NOV-05   WG375519-3   CVS   70-NOV-05   WG3			olved		<0.01		mg/L		0.01	
MG376628-1   CCV   Total Phosphorous   99   %   93-107   10-NOV-05   MG376628-2   CCV   70   70   70   70   70   70   70   7	P-TOTAL-WP		Water							
WG376628-2   CCV   Total Phosphorous   99   %   93.107   10-NOV-05   MG376427-2   CVS   Total Phosphorous   101   %   93.107   10-NOV-05   MG376427-3   CVS   701al Phosphorous   94   %   93.107   10-NOV-05   MG376427-4   DUP   L338005-1   70.363   0.338   mg/L   7.1   17   10-NOV-05   MG376427-1   MB   701al Phosphorous   0.363   0.338   mg/L   7.1   17   10-NOV-05   MG376427-5   MS   L338009-3   70.305   mg/L   7.1   17   10-NOV-05   MG376427-5   MS   L338009-3   70.305   mg/L   7.1   7.1   7.2   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.3   7.4   7.3   7.3   7.3   7.3   7.3   7.4   7.3   7.3   7.4   7.3   7.3   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4   7.4	WG376628-1	CCV			103		%		02.407	40 NOV 05
MG376427-2   CVS   Total Phosphorous   Total Phosphorous   Total Phosphorous   Total Phosphorous   Part   Total Phosphorous   Part	WG376628-2	CCV								
Total Phosphorous         94         %         93-107         10-NOV-05           WG376427-4         DUP Total Phosphorous         0.363         0.338         mg/L         7.1         17         10-NOV-05           WG376427-1         MB Total Phosphorous         0.005         mg/L         0.005         10-NOV-05           WG376427-5         MS Total Phosphorous         L338009-3         103         %         84-114         10-NOV-05           PH-WP         Water         L338009-3         100         %         84-114         10-NOV-05           WG375519-3         CCV PH         100         %         93-107         07-NOV-05           WG375519-3         CVS PH         101         %         9H units         0.45         3.8         07-NOV-05           WG375519-7 PH         101         7.45         PH units         0.20         3.8         07-NOV-05           Batch R344388	Total Phosphor	rous			101		%			
Total Phosphorous 0.363 0.338 mg/L 7.1 17 10-NOV-05  WG376427-1 MB Total Phosphorous 0.005 mg/L 0.005 10-NOV-05  WG376427-5 MS Total Phosphorous 103 % 84-114 10-NOV-05  WG376427-5 MS Total Phosphorous 103 % 84-114 10-NOV-05  PH-WP	Total Phosphor	rous			94		%		93-107	10-NOV-05
Total Phosphorous         0.005         mg/L         0.005         10-NOV-05           WG376427-5 NG TOTAL Phosphorous         MS TOTAL Phosphorous         L33809-3 103         %         84-114         10-NOV-05           PH-WP Batch R344056 WG375519-4 PH         CCV PH         100         %         93-107         07-NOV-05           WG375519-3 PH         CVS PH         101         %         97-103         07-NOV-05           WG375519-6 PH         DUP 7.41         7.45         pH units         0.45         3.8         07-NOV-05           WG375519-7 PH         DUP 7.05         1.338046-1 7.05         7.06         pH units         0.20         3.8         07-NOV-05           Batch R344368 WG375934-4 PH         CCV PH         100         %         93-107         08-NOV-05           WG375934-3 PH         CVS PH         101         %         97-103         08-NOV-05           WG375934-5 PH         DUP R38009-1 PH         101         %         97-103         08-NOV-05	Total Phosphor	ous			0.338		mg/L	7.1	17	10-NOV-05
Total Phosphorus   103	Total Phosphor	ous		1 222000 0	0.005		mg/L		0.005	10-NOV-05
Batch R34056         WG375519-4 PH       CCV PH       100       %       93-107       07-NOV-05         WG375519-3 PH       CVS PH       101       %       97-103       07-NOV-05         WG375519-6 PH       DUP PH       L338009-2 7.41       7.45       PH units       0.45       3.8       07-NOV-05         WG375519-7 PH       DUP PH       L338046-1 7.05       7.06       PH units       0.20       3.8       07-NOV-05         Batch R344368       WG375934-4 PH       CCV PH       100       %       93-107       08-NOV-05         WG375934-3 PH       CVS PH       101       %       97-103       08-NOV-05         WG375934-6 PH       DUP T.338009-1 7.32       7.32       7.35       PH units       0.35       3.8       08-NOV-05	Total Phosphore			L338009-3	103		%		84-114	10-NOV-05
WG375519-4 PH         CCV         100         %         93-107         07-NOV-05           WG375519-3 PH         CVS         101         %         97-103         07-NOV-05           WG375519-6 PH         DUP 7.41         7.45         PH units         0.45         3.8         07-NOV-05           WG375519-7 PH         DUP 1.338046-1 PH         7.05         7.06         PH units         0.20         3.8         07-NOV-05           Batch R344368 WG375934-4 PH         CCV PH         100         %         93-107         08-NOV-05           WG375934-3 PH         CVS PH         101         %         97-103         08-NOV-05           WG375934-6 PH         DUP 7.32         7.35         PH units         0.35         3.8         08-NOV-05		44050	Water							
PH	WG375519-4				100		%		93-107	07-NOV-05
PH 7.41 7.45 pH units 0.45 3.8 07-NOV-05  WG375519-7 DUP		cvs			101		%		97-103	07-NOV-05
PH 7.05 7.06 pH units 0.20 3.8 07-NOV-05  Batch R344368 WG375934-4 CCV PH 100 % 93-107 08-NOV-05  WG375934-3 CVS PH 101 % 97-103 08-NOV-05  WG375934-6 DUP L338009-1 PH 7.32 7.35 pH units 0.35 3.8 08-NOV-05	PH			7.41	7.45		pH units	0.45	3.8	07-NOV-05
WG375934-4 PH         CCV         100         %         93-107         08-NOV-05           WG375934-3 PH         CVS         101         %         97-103         08-NOV-05           WG375934-6 PH         DUP         L338009-1         7.32         7.35         pH units         0.35         3.8         08-NOV-05	PH				7.06		pH units	0.20	3.8	07-NOV-05
WG375934-3 PH         CVS         101         %         97-103         08-NOV-05           WG375934-6 PH         DUP 7.32         L338009-1 7.35         PH units         0.35         3.8         08-NOV-05	WG375934-4				100		%		93-107	08-NOV-05
PH 7.32 7.35 pH units 0.35 3.8 08-NOV-05		cvs			101		%			
O4-DIS-WP Water		DUP			7.35		pH units	0.35	3.8	
	04-DIS-WP		<u>Water</u>							

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### **Enviro-Test Quality Control Report**

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
SO4-DIS-WP	Water							
Batch R344055								
WG375512-3 CCV Sulphate (SO4) - Disso	olved		100		%		93-107	07-NOV-05
WG375512-2 CVS					,•		33-107	07-110-05
Sulphate (SO4) - Disso	lved		98		%		93-107	07-NOV-05
WG375150-1 MB Sulphate (SO4) - Disso	lved		<9		mg/L		9	07-NOV-05
Batch R344388								
WG375888-3 CCV	hd		400		07			
Sulphate (SO4) - Disso	ivea		100		%		93-107	08-NOV-05
WG375888-2 CVS Sulphate (SO4) - Disso	lved		100		%		93-107	08-NOV-05
SO4-SOL-WP	Water							
Batch R344055								
WG375512-3 CCV								
Sulphate (SO4) - Solub	le		100		%		93-107	07-NOV-05
WG375512-2 CVS Sulphate (SO4) - Solub	le		98		%		93-107	07-NOV-05
WG375512-5 DUP		WG375512-4			÷		00 101	0
Sulphate (SO4) - Solub	e	133	132		mg/L	0.24	15	07-NOV-05
WG375512-1 MB Sulphate (SO4) - Solubl	•		<9		ma/l		9	07.1101/05
	C		<del>- 9</del>		mg/L		3	07-NOV-05
Batch R344388 WG375888-3 CCV								
Sulphate (SO4) - Solubi	е		100		%		93-107	08-NOV-05
WG375888-2 CVS	_		400		0/			
Sulphate (SO4) - Solubl	е	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	100		%		93-107	08-NOV-05
WG375888-5 DUP Sulphate (SO4) - Soluble	е	<b>WG375888-4</b> 126	126		mg/L	0.73	15	08-NOV-05
WG375888-1 MB								
Sulphate (SO4) - Soluble	€		<9		mg/L		9	08-NOV-05
SOLIDS-TDS-WP	<u>Water</u>							
Batch R344261								
WG375047-3 CVS Total Dissolved Solids			100		%		96-104	07-NOV-05
WG375047-4 CVS							00 101	07.107.00
Total Dissolved Solids			101		%		96-104	07-NOV-05
WG375047-6 DUP		L338024-1	4500		/I			
Total Dissolved Solids		1500	1500		mg/L	0.81	7.7	07-NOV-05
WG375047-1 MB Total Dissolved Solids			<5		mg/L		5	07-NOV-05
WG375047-2 MB					-			
<b>Total Dissolved Solids</b>			<5		mg/L		5	07-NOV-05

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### **Enviro-Test Quality Control Report**

Test		Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
SOLIDS-TOT-WP		<u>Water</u>	***************************************						
Batch R34	4261								
WG375047-6 Total Solids	DUP		<b>L338024-1</b> 2000	2000		mg/L	0.099	20	07-NOV-05
WG375047-1 Total Solids	МВ		,	<5		mg/L		5	07-NOV-05
WG375047-2 Total Solids	MB			<5		mg/L		5	07-NOV-05
SOLIDS-TOTSUS-WI	<u>P</u>	<u>Water</u>							
Batch R344	4261								
WG375047-3 Total Suspended	CVS Solids			102		%		86-108	07-NOV-05
WG375047-4 C Total Suspended	CVS Solids			100		%		86-108	07-NOV-05
WG375047-5 I Total Suspended	DUP Solids		L337755-1 71	73		mg/L	2.8	15	07-NOV-05
WG375047-6 I Total Suspended	DUP Solids		<b>L338024-1</b> 420	420		mg/L	0.95	15	07-NOV-05
WG375047-1 M Total Suspended	MB Solids			<5		mg/L		5	07-NOV-05
WG375047-2 Notal Suspended	<b>MB</b> Solids			<5		mg/L		5	07-NOV-05
TEH-WP		<u>Water</u>							
Batch R344	530								
<b>WG376129-2</b> CTEH (C11-C30)	CCV			103		%		70-130	09-NOV-05
<b>WG376129-1</b> CTEH (C11-C30)	cvs			97		%		87-129	09-NOV-05
<b>WG375661-2</b> L TEH (C11-C30)	.cs			135	н	%		73-131	09-NOV-05
WG375661-1 N TEH (C11-C30)	/B			<0.1		mg/L		0.1	09-NOV-05
TURBIDITY-WP	1	<u>Water</u>							
Batch R3439									
	CV			101		%		97-103	07-NOV-05
WG375328-1 C Turbidity	vs			101		%		93-107	07-NOV-05
WG375328-4 D	UP		<b>L338009-2</b> 70	70		NTU	0.0	15	07-NOV-05
WG375328-3 M Turbidity	В			<0.05		NTU		0.05	07-NOV-05
<u>rvh-wp</u>	Y	<u>Vater</u>							

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### **Enviro-Test Quality Control Report**

Test		Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
TVH-WP		Water							
Batch R	344763								
WG376384-1 Total Volatiles	CCV			97		%		87-113	08-NOV-05
WG376384-2 Total Volatiles	CCV			102		%		87-113	08-NOV-05
WG376384-3 Total Volatiles	cvs			97		%		87-113	08-NOV-05
WG376350-3 Total Volatiles	DUP		<b>L338009-4</b> <0.1	<0.1	RPD-NA	mg/L	N/A	12	08-NOV-05
WG376350-1 Total Volatiles	МВ			<0.1		mg/L		0.1	08-NOV-05
WG376350-2 Total Volatiles	MS		L338009-5	90		%		80-120	08-NOV-05

### **ENVIRO-TEST QC REPORT**

Workorder # L338009

#### Legend:

Limit	95% Confidence Interval (Laboratory Warning Limits)
DUP	Duplicate
RPD	Relative Percent Difference
N/A	Not Available
LCS	Laboratory Control Sample
SRM	Standard Reference Material
MS	Matrix Spike
MSD	Matrix Spike Duplicate
ADE	Average Desorption Efficiency
MB	Method Blank
IRM	Internal Reference Material
CRM	Certified Reference Material
CCV	Continuing Calibration Verification
CVS	Calibration Verification Standard
	and the state of t

LCSD Laboratory Control Sample Duplicate

#### Qualifier:

RPD-NA A	Relative Percent Difference Not Available due to result(s) being less than detection limit.  Method blank exceeds acceptance limit. Blank correction not applied, unless the qualifier "RAMB" (result adjusted for method blank) appears in the Analytical Report.
В	Method blank result exceeds acceptance limit, however, it is less than 5% of sample concentration.  Blank correction not applied.
E	Matrix spike recovery may fall outside the acceptance limits due to high sample background.
Ē	Silver recovery low, likely due to elevated chloride levels in sample.
Ġ	Outlier - No assignable cause for nonconformity has been determined.
Ĥ	Result falls within the 99% Confidence Interval (Laboratory Control Limits)
J	Duplicate results and limit(s) are expressed in terms of absolute difference.
K	The sample referenced above is of a non-standard matrix type; standard QC acceptance criteria may not be achievable.

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# LGD of MYSTERY LAKE Geotechnical and Topographic Investigation for the Waste Disposal Ground





Prepared by:

J. R. Cousin Consultants Ltd.91A Scurfield Blvd.Winnipeg, ManitobaR3Y 1G4

#### **ACKNOWLEDGMENTS**

To prepare this report various sources of information were investigated and researched. J. R. Cousin Consultants Ltd. (JRCC) wishes to thank the LGD of Mystery Lake who assisted with organization and onsite works.

#### **REMARKS**

Conclusions reached in this report are based upon the generalization of data available to us at the time of forming our opinions. Information in this document may rely on previous studies, investigative work and data by others. JRCC cannot be responsible for actual site conditions proved to be at variance with any generalized data. This report was completed in accordance with generally accepted professional engineering principles and practice. Any use of this report by a third party is the responsibility of the third party, JRCC accepts no responsibility for third party decisions or actions based on the report. No other warranty or guarantee expressed, implied or statutory is made.

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#### **APPENDIX**

Plan 1: Test Hole Location Plan

Plan 2: Topographic Survey Plan with Contour Lines

Test Hole Logs

National Testing Laboratories Test Results

#### 1.0 INTRODUCTION

J. R. Cousin Consultants Ltd. (JRCC) conducted a geotechnical investigation for the Waste Disposal Ground (WDG) Expansion at the LGD of Mystery Lake. The LGD of Mystery Lake existing WDG is located on Part NW ¼ 18, S ½ and NW ¼ 19 in TWP 77-3 WPM and in Part SE ¼ 24-77-4 WPM, approximately 4 km south of the City of Thompson. The WDG services the LGD of Mystery Lake, the City of Thompson, the Town of Churchill and the Wuskawatim Generating Station. However, the Town of Churchill and the Wuskawatim Generating Station area scheduled to discontinue use of the WDG in the near future.

A total of thirteen test holes were drilled at the WDG site. Test hole locations are shown on Plan 1 attached in the Appendix. The test holes were drilled to determine suitability of the insitu soils for use as a clay landfill liner and clay leachate pond liner.

This report outlines the findings of the geotechnical investigation at the WDG site and evaluates the soils to determine their suitability for use as a landfill liner. The report also identifies potential difficulties (i.e. depth to bedrock, soil types and subsurface water elevations) associated with construction.

#### 2.0 BACKGROUND

The existing WDG is nearing capacity and requires expansion. The LGD of Mystery Lake intends to construct a lined expansion cell to the west of the municipal waste disposal area during Phase I and lined expansions to the north and east during future phases. A lined leachate collection pond will be constructed as part of the Phase I works. An upgraded burn area, soil remediation area and other various storage compounds will be constructed as part of future works.

The geotechnical investigation was required to evaluate potential use of insitu and re-worked soils as a clay landfill or leachate pond liner and for use in cell dike construction. Hydraulic conductivity tests were performed on Shelby tube samples to assess whether the insitu soils comply with the Manitoba Conservation criteria of  $1 \times 10^{-7}$  cm/sec or less for a landfill liner.

A previous geotechnical and topographic investigation was completed by AECOM in 2005. Eight test holes were drilled around the perimeter of the WDG and three holes were drilled within the former waste cells to determine the depth of waste. Shelby tube samples and laboratory analysis of the soils was not completed and therefore it is unknown if the soils could achieve a hydraulic conductivity of 1 x 10⁻⁷ cm/s insitu or when re-worked.

#### 3.0 TOPOGRAPHIC INVESTIGATION

The onsite topographic survey was completed on April 14, 2011. The existing WDG and the areas for the proposed cell expansion and leachate pond area were surveyed with a GPS Total Station.

The survey found that the top of the existing former and current waste disposal area slopes from an elevation of approximately 219.0 m in the east to 215.0 m in the west at a grade of approximately 2.0 % - 5.0%. The existing ground surrounding the WDG is approximately 4 m - 6 m lower than the top of waste and slopes to the southwest. The leachate pond area is relatively flat at an elevation of approximately 209.0 m. There is a rock outcrop east of the former and current waste disposal area which slopes up to a maximum elevation of approximately 225.0 m towards PTH 6.

Contour lines from the topographic survey are shown on Plan 2 attached in the Appendix.

#### 4.0 GEOTECHNICAL FIELD INVESTIGATION

The onsite investigation at the LGD of Mystery Lake was conducted on April 13, 2011. Maple Leaf Drilling Ltd. was employed to complete the test holes utilizing a DR150 track mounted drill rig under direct supervision by JRCC's field representative.

A total of thirteen test holes were drilled during the investigation. Three test holes were drilled in the leachate pond area (TH1 – TH3), three test holes were drilled in the Phase I expansion cell area (TH4 – TH 6), four test holes were drilled in the areas for future expansion (TH7 - TH10) and three test holes were drilled through the former waste disposal areas (TH11 – TH13). All test holes were drilled to a depth of 6.0 m with the exception of TH11, which was dug to a depth of 2.0 m.

#### 4.1 WDG Site

The subsurface soil profile within each test hole was logged, water conditions were noted and representative soil samples were taken as the soils varied along the profile. The samples were visually field-classified. Eight selected bagged samples from the test holes were sealed and submitted to National Testing Laboratories Ltd. for testing and analysis, along with three Shelby tube samples for hydraulic conductivity testing. Details of the laboratory analysis are provided in Section 5.0. Following drilling, the depth of standing water was measured and any caving of the holes was determined. Test holes were backfilled with bentonite and the excavated soils upon termination of drilling. Test hole locations are shown on Plan 1 attached in the Appendix.

#### 4.1.1 Soil Profile

The test holes taken across the site were fairly consistent with slight variations in the layer thicknesses and amount of silt in each layer. Bedrock was not encountered in any of the test holes. Details of the test holes can be found in the soils logs attached in the Appendix.

#### Leachate Pond Area

The soil profile observed in the test holes taken in the leachate pond area (TH1 – TH3) consisted of a surficial peat layer an average of 0.4 m thick, followed by a light brown

high plastic clay layer an average of 3.3 m thick, followed by a grey low-medium plastic clay layer with some silt lenses an average of 2.3 m thick.

#### Phase I Expansion Cell Area

The soil profile observed in the test holes taken in the Phase I cell expansion area (TH4 – TH6) consisted of a surficial peat layer an average of 0.4 m thick, followed by a brown high plastic clay layer an average of 3.0 m thick, followed by a grey high plastic clay layer with a trace of silt an average of 2.6 m thick.

#### Future Phase Expansion Cell Areas

The soil profile observed in the test holes taken in the proposed future phases of cell expansion (TH7 – TH10) consisted of a surficial peat layer an average of 0.4 m thick, followed by a brown high plastic clay layer an average of 3.0 m thick, followed by a grey low-medium plastic clay layer with silt lenses an average of 2.6 m thick.

#### **Existing Waste**

Test holes were taken in the existing waste to determine the depth of waste and to evaluate the soils serving as the existing landfill liner. TH11 was drilled to a depth of 2.0 m to determine if the area at the south end of the WDG was formerly used for waste disposal.

The soil profile observed in the test holes taken in the former waste disposal areas to a depth of 6.0 m (TH12 and TH13) consisted of an approximately 0.15 m thick soil cover layer followed by garbage an average of 4.6 m thick, and finally a brown high plastic clay layer with a trace of silt, observed to be at least 1.2 m thick.

#### 4.1.2 Groundwater

Short-term groundwater conditions were assessed in each test hole by observing standing water in the test holes prior to backfilling the holes. No standing water was observed in the test holes with the exception of TH1 and TH2, taken in the leachate pond area. The infiltrating water was caused by standing water on the ground surface around the test holes which flowed into the holes.

TH6 was left open for 4 hours to allow for longer-term water infiltration to occur. After the elapsed time, no standing water was observed in the hole. Caving of the hole was observed at approximately 3.6 m.

Groundwater in the test holes depends on high static groundwater conditions and on seasonal conditions, i.e. snowmelt and rainy seasons. The test holes were taken during a period of snow melt which may have contributed to the standing water observed on the ground surface in the leachate pond area. Other assumptions relating to the groundwater elevation cannot be made at this time as water levels will normally fluctuate seasonally.

Contractors will be made aware of the geotechnical conditions encountered onsite, as some dewatering of the ground surface may be required during construction.

#### 5.0 LABORATORY TESTING, ANALYSIS AND DISCUSSION

#### 5.1 Laboratory Analysis

Two representative soil samples from the leachate pond area, two samples from the proposed Phase I cell expansion area, two samples from the future expansion areas and two samples from the clay layer beneath the existing waste were submitted to National Testing Laboratories Ltd. on April 21, 2011, for analysis and a professional assessment. The analysis included the determination of the following:

- Moisture Content (ASTM D2216)
- Atterberg Limits (plastic limit, liquid limit, and plasticity index, ASTM D4318)
- Soil Classification (ASTM D2487)
- Particle Size Analysis (Hydrometer test, ASTM D422)
- Hydraulic Conductivity (ASTM D2435)

The WDG soils were analyzed to determine their suitability as a re-worked or insitu liner for a WDG cell or leachate pond, which requires a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less.

The laboratory analysis of the soils indicated that they are low to high plastic clay soils with a trace of silt. The overall Plasticity Index of the samples varied between 18 and 43 and the percentage of clay from 85.5% to 96.4%. Based on past experience, the laboratory has commented that homogeneous soils with a plasticity index greater than 25 and a clay content greater than 50% would typically be expected to have a hydraulic conductivity of 1 x  $10^{-7}$  cm/sec or less. Plasticity index analysis (i.e. Atterberg limits) of the soils indicated that all of the soil samples submitted were considered suitable for use as an insitu clay liner or when re-worked and re-compacted with the exception of TH8 from 3.9-6.0 m, which had a Plasticity Index of 18 and clay content of 85.5%.

The results indicate that the suitability of the soils for a clay liner is dependent upon the soils being homogeneous with no preferential flow paths. These preferential flow paths can be caused by lenses of unsuitable material, rocks or boulders or fissures in the soil.

Three Shelby tube samples (TH3 1.5 - 2.1 m, TH6 3.0 - 3.6 m, and TH8 3.0 - 3.6 m) were submitted to determine the insitu hydraulic conductivity, to determine the potential use as a WDG or leachate pond liner. Note that the Shelby tube sample from TH8 was taken in the layer of high plastic clay existing above the unfavourable clay layer which starts approximately 3.9 m from the

ground surface. The samples achieved hydraulic conductivities of  $8.9 \times 10^{-9}$  cm/sec,  $1.4 \times 10^{-8}$  cm/sec and  $9.9 \times 10^{-9}$  cm/sec, respectively which are less than the required  $1 \times 10^{-7}$  cm/sec for a clay lined cell. Therefore the soils would likely be suitable for a clay lined cell in an insitu state.

Details of National Testing Laboratories test results and analysis, dated May 27, 2011 are attached in the Appendix.

#### 6.0 WDG CELL LINER REQUIREMENTS

#### **6.1** Current Guidelines

Manitoba Conservation guidelines require that a standard WDG cell and leachate pond clay liner be 1.0 metre in thickness and have a hydraulic conductivity (i.e. the potential rate of fluid movement through the soil) of  $1 \times 10^{-7}$  cm/sec or less. This low rate is to protect the underlying groundwater and surrounding lands from leachate seepage. Generally, the higher a soil's plasticity the more likely a soil can achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec.

#### **6.2** Typical Clay Liner Construction Options

The insitu (undisturbed) soils can be used to construct the liner of a WDG cell or leachate pond if the soils can consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less in their insitu state.

If the insitu soils cannot be used, the liner can be constructed by excavating and re-compacting suitable high plastic clay soils to form the liner.

If the clay content of the soils is so low that even when excavated and re-compacted, the soils cannot consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, a liner constructed of high plastic clay from a borrow pit, or a synthetic geomembrane liner would be required.

#### 6.3 Liner for the LGD of Mystery Lake WDG

The following are the typical options for lining a WDG cell and leachate pond including using the insitu soil if it can achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, re-working and recompacting the existing soil, to achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, or utilizing a synthetic geomembrane liner.

#### 6.3.1 Insitu Soil

Based on the geotechnical investigation and laboratory analysis the soils in the leachate pond area from 0.4 m to 3.7 m below ground are suitable for use as an insitu clay liner. The soils in the Phase I expansion area from 0.4 – at least 6.0 m below ground are suitable for use as an insitu clay liner. The soils from the area for future cell expansion are suitable for an insitu clay liner from 0.3 – 3.4 m below ground.

In this option the vertical cutoff walls in the WDG perimeter dikes and the leachate pond dikes would be made of re-worked and re-compacted clay soils extended a minimum of 1.0 m into the insitu clay horizontal liner.

Using the insitu clay for the horizontal bottom liner in the leachate pond area, the Phase I expansion area and the future expansion area would be possible, provided that the soils are uniform throughout the proposed construction sites and no preferential flow paths exist.

If some unsuitable soils or boulders are encountered during excavation of the cells, they need to be removed and replaced with re-worked medium to high plastic clay from a borrow site or from previously excavated material.

#### 6.3.2 Re-Worked Soil

The WDG cell and leachate pond liner could be constructed by re-working and recompacting the insitu soils to form the bottom liner and vertical cut-off walls in the WDG cell and leachate pond dikes.

This option would provide a lower hydraulic conductivity in the horizontal layer and reduce the risk of not meeting the Manitoba Conservation guideline of a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less in the liner. However, this would add significant cost to the project and based on the Shelby tube samples taken at the site, the insitu hydraulic conductivity meets the guidelines and re-compaction of the bottom liner is not necessary.

If during final design, the insitu clay liner in the leachate pond extends below 3.7 m or the insitu liner in the future expansion cell area extends below 3.4 m, a re-worked and recompacted horizontal liner may be required in those areas.

#### 6.3.3 Geomembrane Liner

The WDG liner could be constructed with a synthetic geomembrane liner, using insitu soils as the bedding material for the liner and sand from a borrow pit used as a liner cover. The cost of installing a geomembrane liner would be significantly greater than utilizing a clay liner and unnecessary based on the laboratory test results of the insitu clay.

#### **6.3.4** Liner Under the Existing Waste

Laboratory analysis of the bagged samples from the clay liner beneath the existing waste found an average plasticity index of 41 and average clay content of 91.3% and a similar

soil structure to the samples which did have an insitu hydraulic conductivity of less than  $1 \times 10^{-7}$  cm/sec. Based on these results, it is likely that the clay liner under the existing waste does meet the Manitoba Conservation guideline for a WDG liner.

Shelby tube samples could not be completed in the layer and therefore insitu hydraulic conductivity testing could not be completed.

#### **6.3.5 Summary**

An insitu clay liner can be utilized in design of the leachate pond, Phase I expansion cell and future expansion cells. If unsuitable soils are encountered, specifications will indicate they will be replaced with high plastic clay borrow material. An insitu liner likely exists under the existing waste disposal areas, however this was not confirmed with insitu hydraulic conductivity testing.

#### 7.0 SUMMARY, RECOMMENDATIONS AND CLOSURE

#### 7.1 Summary

The topography of the WDG was surveyed and found that the top of the existing former and current waste disposal area slopes from east to west. The existing ground surrounding the WDG is approximately 4.0 - 6.0 m lower than the top of waste and slopes to the southwest. There is a rock outcrop east of the former and current waste disposal area which slopes up towards PTH 6.

Soils at the existing WDG were investigated by JRCC. Representative soil samples were analyzed by National Testing Laboratories Ltd. to determine their suitability for a clay liner. Based on the geotechnical investigation and laboratory analysis, all of the soils tested are suitable for construction of an insitu clay liner in accordance with Manitoba Conservation guidelines with the exception of TH8 (3.9-6.0 m).

It is not unusual to encounter differing soil types across a large area when constructing a liner for a WDG cell. If the soil type from TH8 (3.9 - 6.0 m) is encountered elsewhere at the WDG specifications will indicate they will be replaced with high plastic clay borrow soil and recompacted to achieve the required hydraulic conductivity.

If the insitu soils were re-worked and compacted, they would also meet the Manitoba Conservation guideline of  $1 \times 10^{-7}$  cm/sec, however, this option would be significantly more costly than utilizing an insitu liner.

The vertical cutoff walls in the WDG perimeter dikes and the leachate pond dikes would have to be made of re-worked and re-compacted clay soils extended a minimum of 1.0 m into the insitu clay horizontal liner.

Bagged samples taken in the layer below the existing waste suggest that the existing liner likely meets the Manitoba Conservation guideline of  $1 \times 10^{-7}$  cm/sec. Shelby tube samples were not taken in the clay layer and therefore insitu hydraulic conductivity testing could not be completed.

No water infiltration was observed in the test holes, with the exception of TH1 and TH2 in the leachate pond area which had standing water at the ground surface. Contractors will have to be made aware of these conditions prior to construction, however water levels can vary seasonally.

#### 7.2 Recommendations

It is recommended that an insitu clay horizontal bottom layer be used for the leachate pond area between 0.4-3.7 m below ground, the Phase I expansion cell area between 0.4-6.0 m below ground and in the future expansion area between 0.4-3.4 m below ground. If unsuitable material such as the soil found in TH8 (3.9-6.0 m) is encountered during WDG liner or leachate pond liner construction, specifications will indicate that it will be replaced with high plastic clay borrow material. It is recommended the vertical cut-off walls be constructed of re-worked and recompacted clay and extended a minimum of 1.0 m into the insitu clay layer.

#### 7.3 Closure

The conclusions and recommendations in this report are based on the results of the site investigation and laboratory analysis. In addition, soil and groundwater conditions between test hole locations were generalized to provide an overall assessment of the geotechnical site conditions. If conditions that appear different from those encountered at the test hole locations as described in this report, or if the assumptions stated herein are not in agreement with the design, JRCC should be informed in order that the recommendations can be reviewed and adjusted as required.

The site investigation was conducted for the purpose of identifying geotechnical conditions at the potential expansion cell sites and leachate pond site. Although no environmental issues were identified during the site investigation, it does not necessarily follow that such issues do not exist. If the client or any other parties have any environmental concerns regarding the proposed site and works, an appropriate environmental assessment must be conducted.

It is not uncommon for soil conditions to be highly variable across a site. Previous construction activities and placement of fill at a site can augment the variability of soil conditions, especially surficial soil conditions. A contingency must be included in any construction budget to allow for potential variations in soil conditions, which may result in modification of the design and construction procedures.

### **APPENDIX**

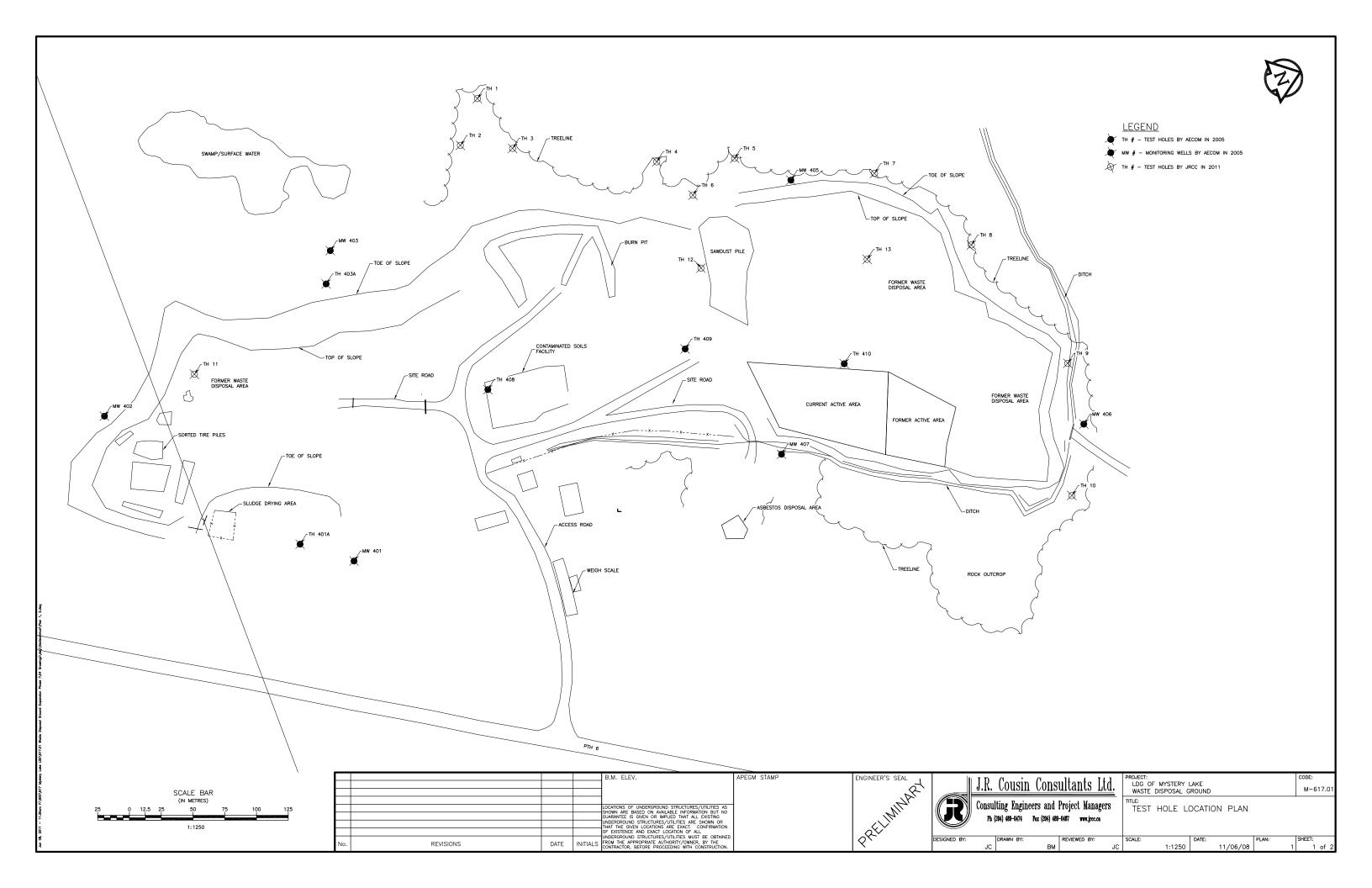
**Plan 1:** Test Hole Location Plan

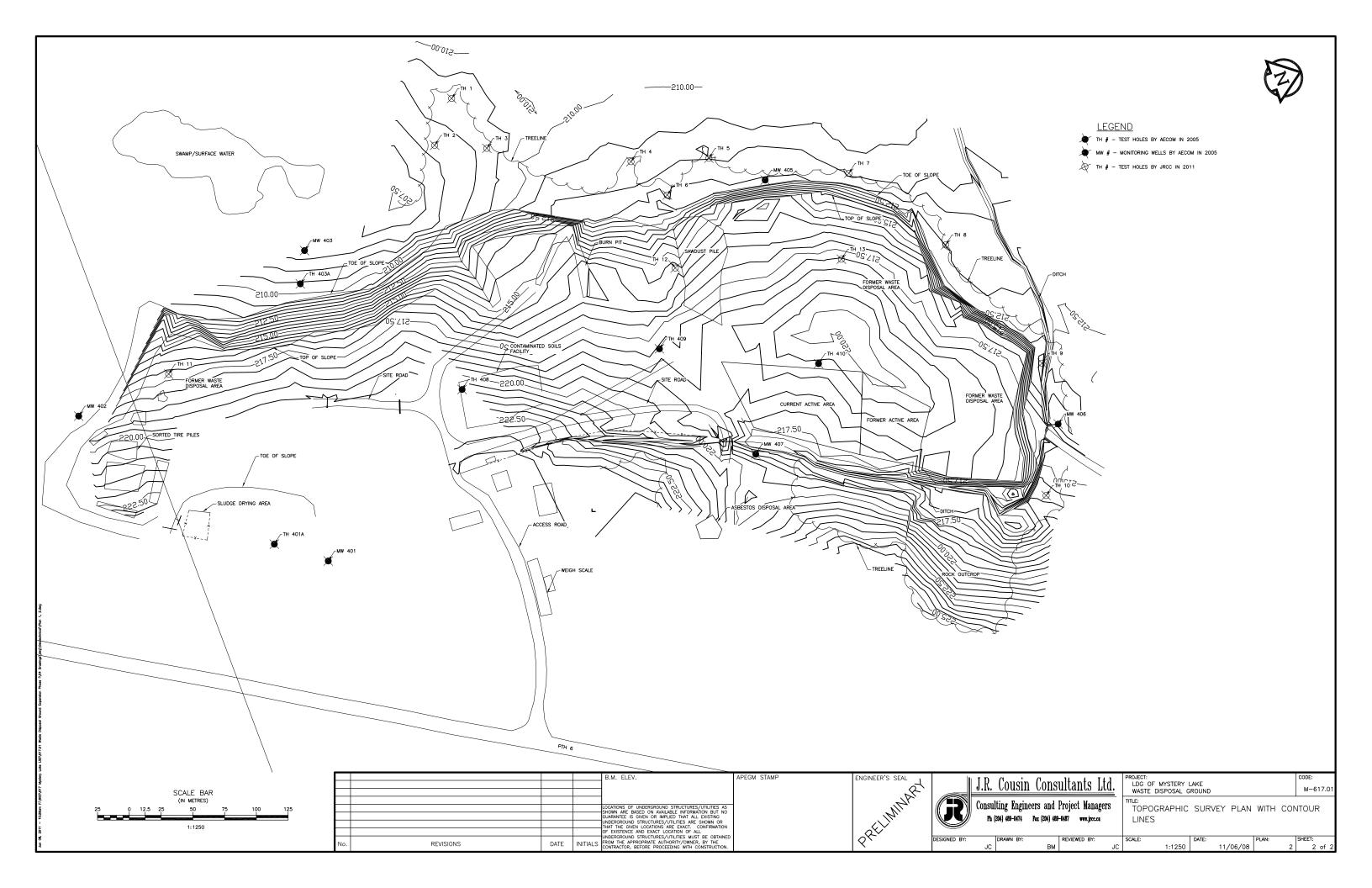
**Plan 2:** Topographic Survey Plan with Contour Lines

**Test Hole Logs** 

**National Testing Laboratories Ltd. Test Results** 









#### SYMBOL INDEX

SYMBOL INDEX
GW. : Well graded gravels and gravel sand mixtures, little or no fines
GP. : Poorly graded gravels, gravel - sand mixtures, little or no fines
GM. : Silty gravels, gravel-sand-silt mixtures
GC. : Clayey gravels, gravel-sand-clay mixtures
SW.: Well graded sands, gravelly sands, little or no fines
SP.: Poorly graded sands, or gravelly sands, little or no fines
SM. : Silty sands, sand-silt mixtures
SC. : Clayey sands, sand-clay mixtures
ML. : Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity
CL. : Inorganic clays of low plasticity, gravelly clays, sandy or silty clays, lean clays
OL. : Organic silts and organic silty clays of low plasticity
CI. : Inorganic clays of medium or intermediate plasticity
MH. : Inorganic silts, fine sandy or silty soils
CH.: Inorganic clays of high plasticity, fat clays
OH. : Organic clays of medium to high plasticity, organic silts
Pt. : Peat, humus, swamp soils with high organic contents

TOPSOIL

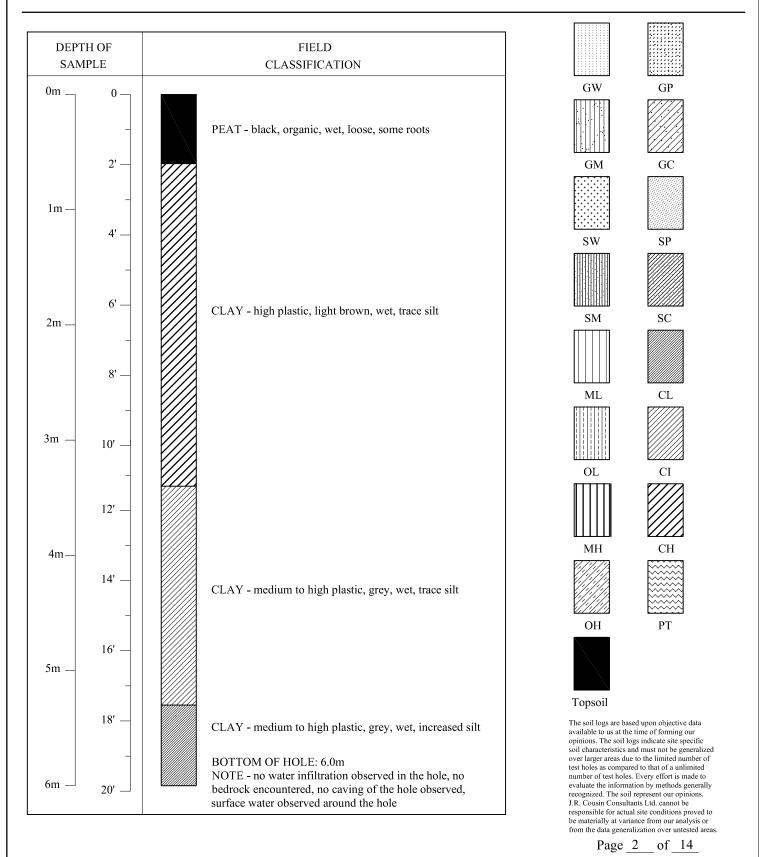
The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized over larger areas due to the limited number of test holes as compared to that of an unlimited number of test holes. Every effort is made to evaluate the information by methods generally recognized. The soil logs represent our opinions. J. R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

LOCATION: 6171154.68 N

567715.20 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 208.14 m

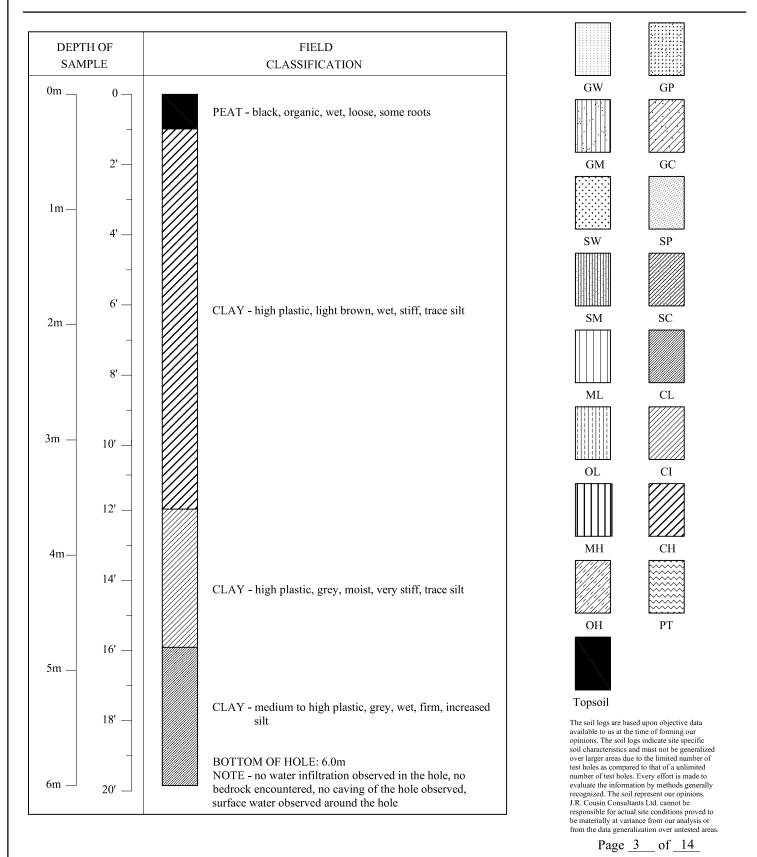


LOCATION: 6171129.72 N

567745.42 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 207.49 m

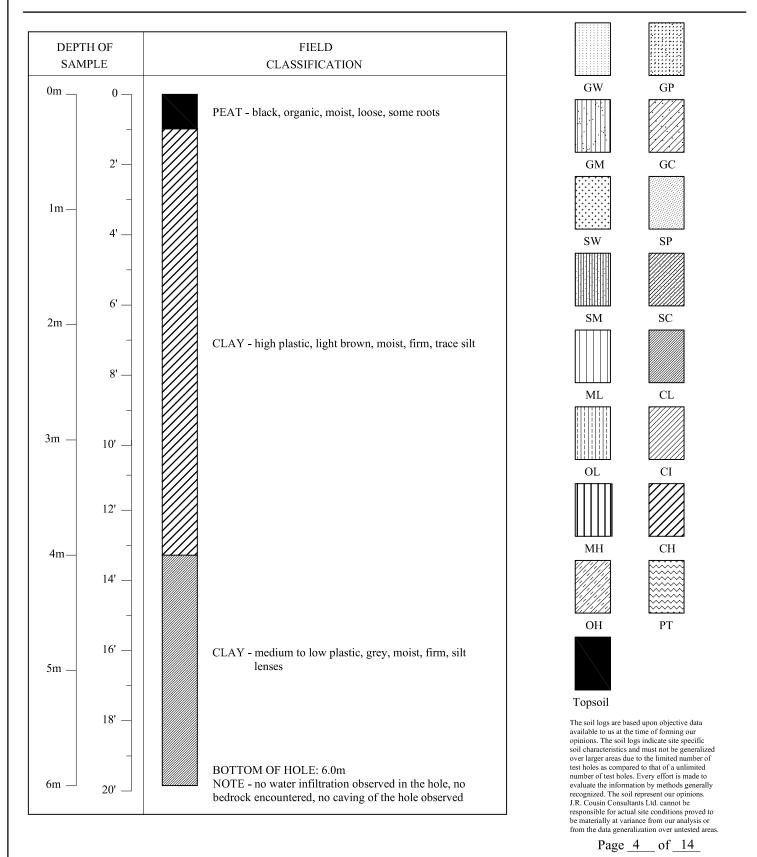


LOCATION: 6171167.60 N

567761.44 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 208.13 m

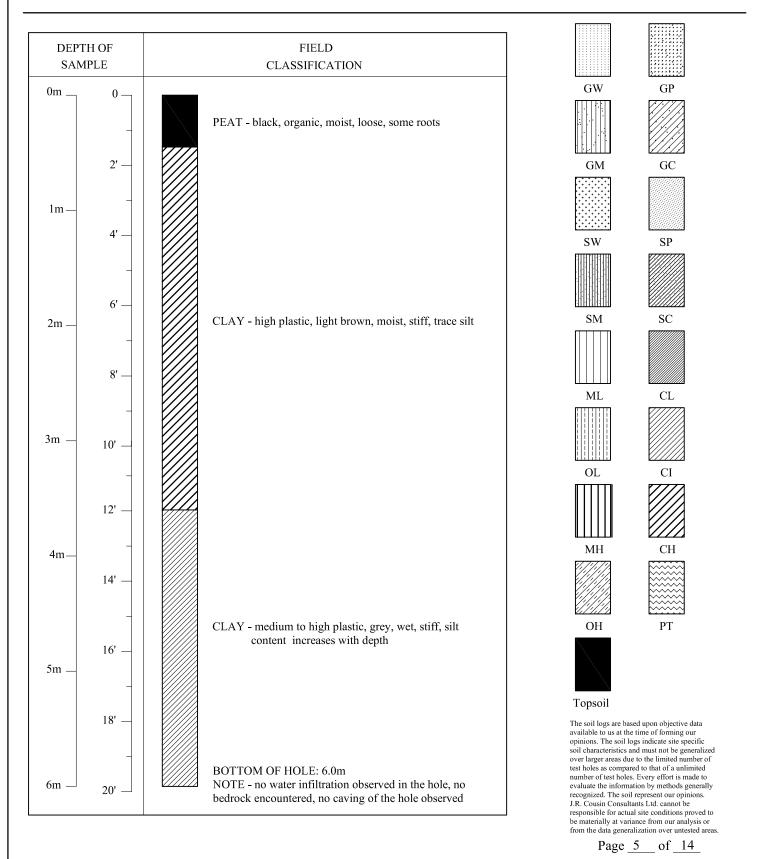


LOCATION: 6171270.91 N

567809.40 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 209.61 m



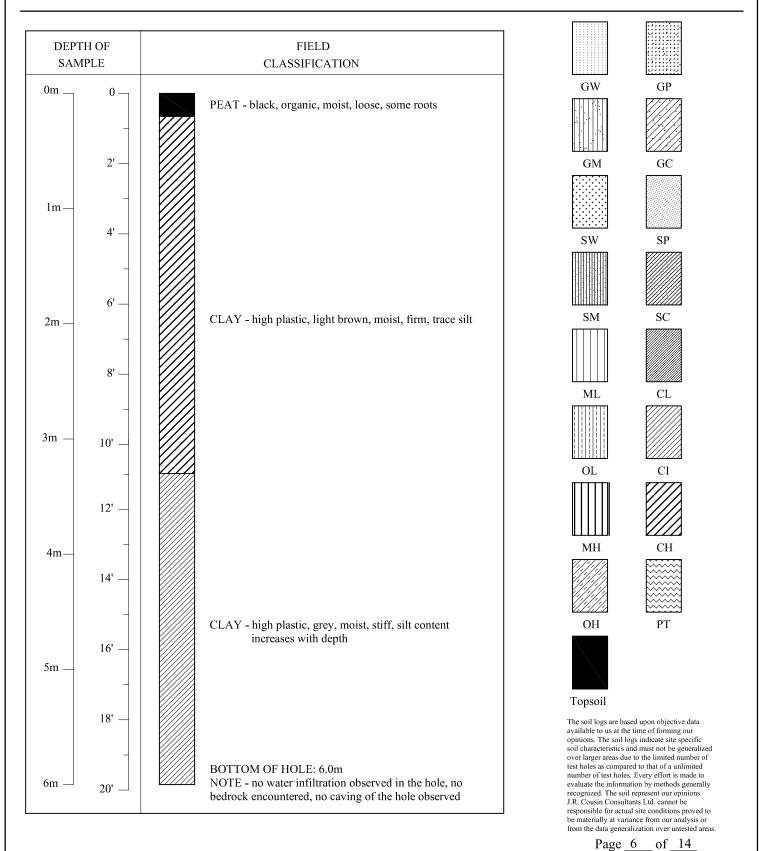
LOCATION: 6171329.55 N

567827.42 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011

ELEVATION: 209.88 m



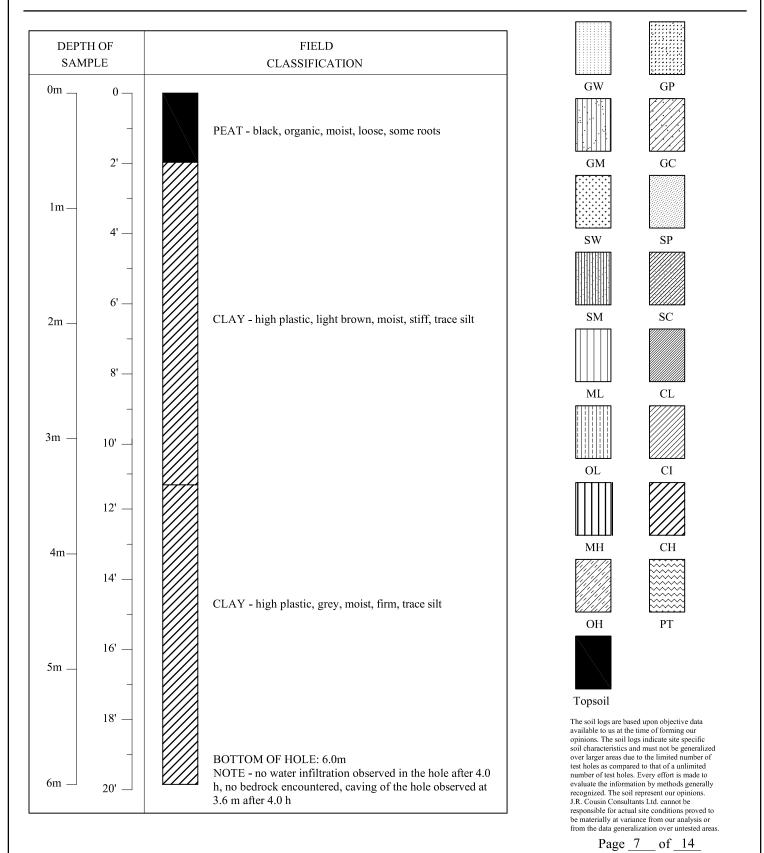
LOCATION: 6171288.86 N

567843.71 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE: April 13, 2011

ELEVATION: 210.19 m

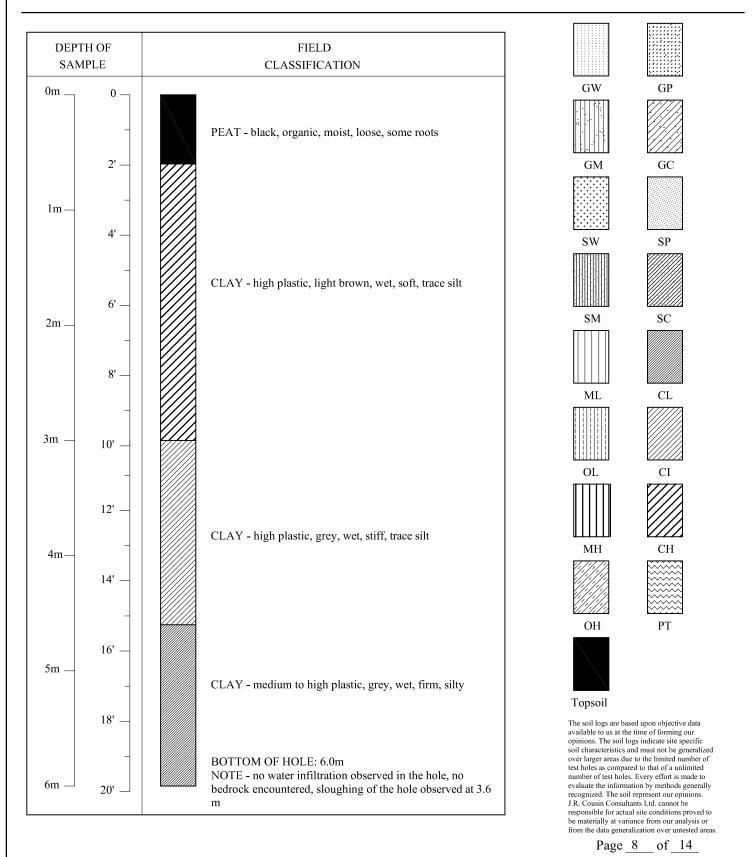


LOCATION: 6171429.28 N

567875.52 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 209.79 m



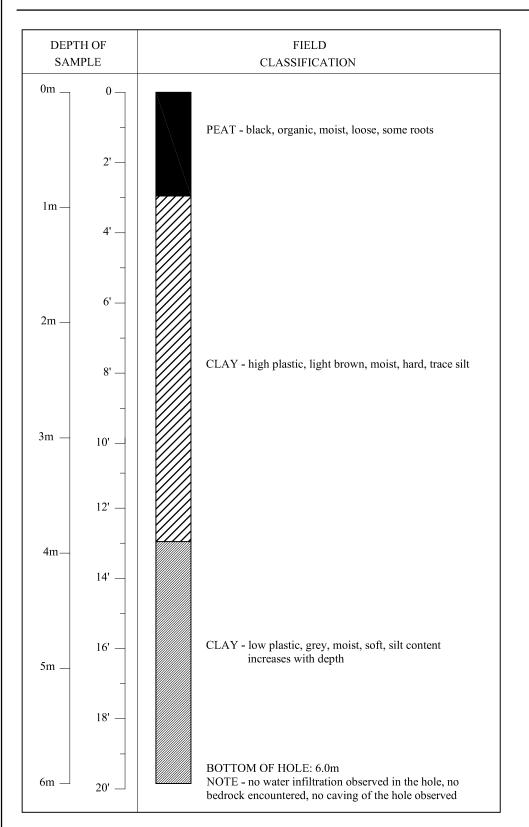
LOCATION: 6171482.16 N

567954.14 E

 $PROJECT: LGD\ of\ Mystery\ Lake\ -\ Waste\ Disposal\ Ground$ 

DATE : April 13, 2011
ELEVATION : 210.88 m

TEST HOLE #8 GW GC SWSP CLОН Topsoil The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific



The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized over larger areas due to the limited number of test holes as compared to that of a unlimited number of test holes. Every effort is made to evaluate the information by methods generally recognized. The soil represent our opinions. J.R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

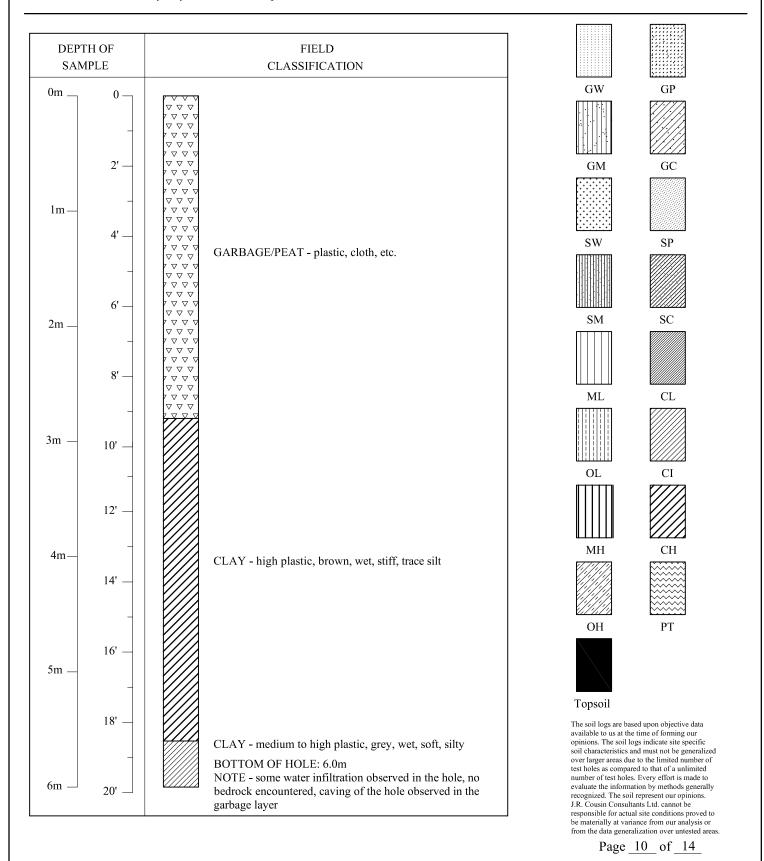
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LOCATION: 6171522.36 N

568067.31 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 211.67 m



LOCATION: 6171490.51 N

568166.36 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 214.83 m

TEST HOLE # 10

GW GP GCGMSP CLОН Topsoil The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized over larger areas due to the limited number of test holes as compared to that of a unlimited number of test holes. Every effort is made to number of test noies. Every effort is made to evaluate the information by methods generally recognized. The soil represent our opinions. J.R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

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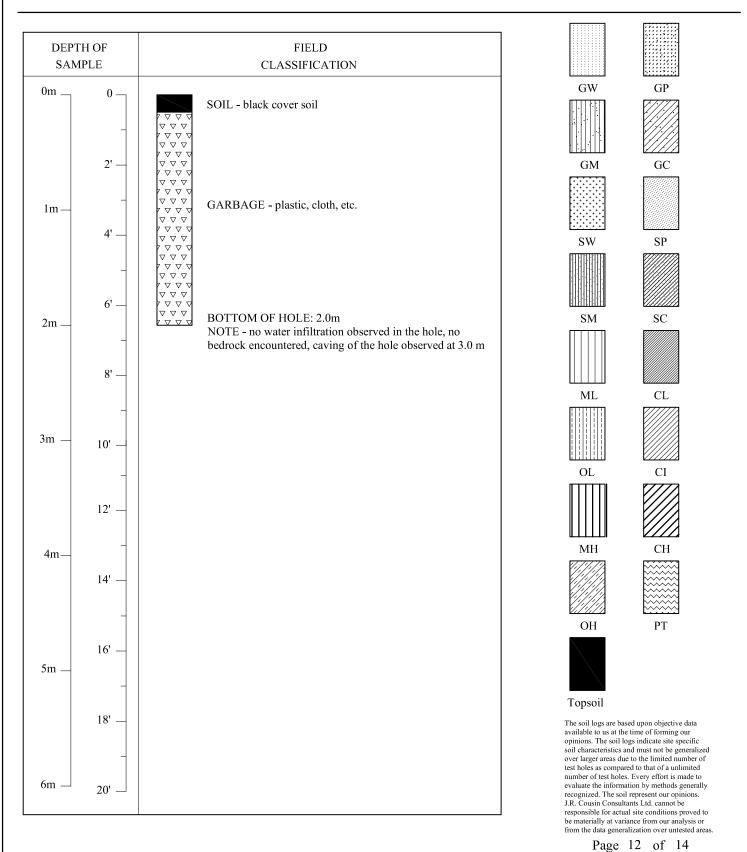
DEPT SAM		FIELD CLASSIFICATION
0m	0 _	PEAT - black, organic, moist, loose, some roots
1m —	2' —	
2m —	6' —	CLAY - high plastic, brown, dry, firm, trace silt
3m —	10' —	
4m—	12' —	
5m —	16' —	CLAY - high plastic, grey, moist, firm, trace silt
6m _	20'	BOTTOM OF HOLE: 6.0m  NOTE - no water infiltration observed in the hole, no bedrock encountered, caving of the hole observed at 3.0 m

LOCATION: 6170872.19 N

567844.70 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 216.13 m

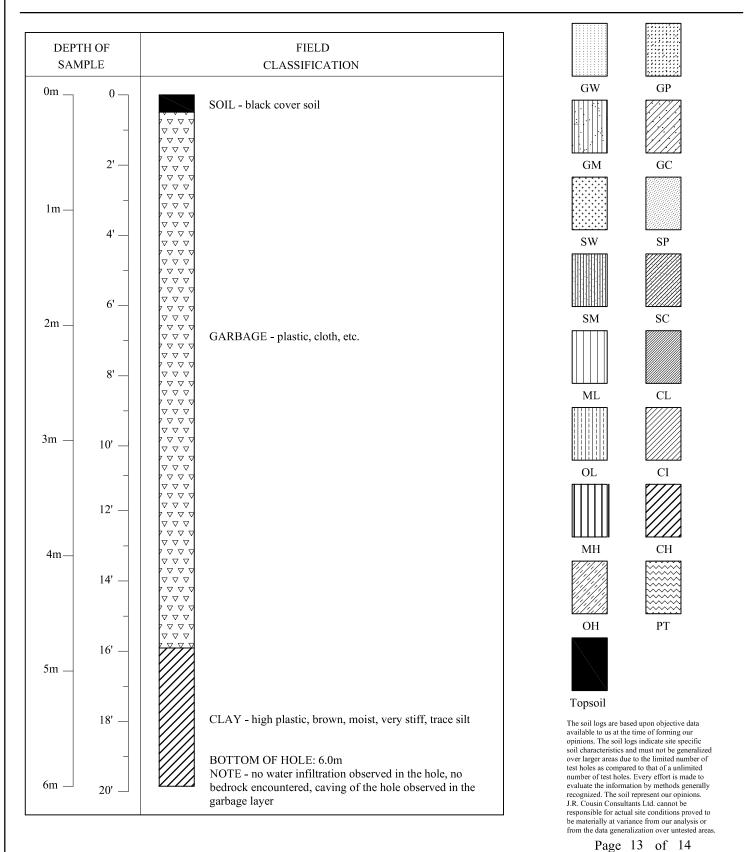


LOCATION: 6171275.63 N

567899.87 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011 ELEVATION : 214.70 m



### J. R. Cousin Consultants Ltd. TEST HOLE LOG SHEET

LOCATION: 6171401.11 N

567937.24 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : April 13, 2011
ELEVATION : 216.96 m

TEST HOLE # 13

DEPTH OF **FIELD** SAMPLE CLASSIFICATION GW GP 0mSOIL - black cover soil 2' GC 1m 4' SWSP 6' SC 2m -GARBAGE - plastic, cloth, etc. 8' CL 3m -10' 12' 4m 14' ОН 16' 5m -CLAY - high plastic, brown, moist, very stiff, some silt Topsoil 18' The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized BOTTOM OF HOLE: 6.0m over larger areas due to the limited number of test holes as compared to that of a unlimited number of test holes. Every effort is made to NOTE - no water infiltration observed in the hole, no 6m evaluate the information by methods generally recognized. The soil represent our opinions. bedrock encountered, caving of the hole observed in the 20' garbage layer

recognized. The soil represent our opinions.

J.R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

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199 Henlow Bay Winnipeg, MB R3Y 1G4 Phone (204) 488-6999 Fax (204) 488-6947 Email info@nationaltestlabs.com www.nationaltestlabs.com

J.R. Cousin Consultants Ltd. 91 A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

May 27, 2011

Project: Mystery Lake Waste Disposal Facility

Soil samples were submitted to our laboratory on April 21, 2011. The following tests were conducted on selected soil samples:

Attention: Brett McCormac

- water content (ASTM D2216)
- particle size analysis (ASTM D422)
- liquid limit, plastic limit, and plasticity index (ASTM D4318)
- hydraulic conductivity (ASTM D2435)
- soil classification (ASTM D2487)
- visual classification

The test results for the soil samples are summarized in the following tables and in the attached particle size analysis and hydraulic conductivity reports.

An assessment of the bagged soil samples was conducted to determine whether the soil represented by the bagged samples could be used in-situ as a landfill liner and would obtain a hydraulic conductivity of less than 1.0 x 10⁻⁷ cm/sec without being reworked, and when re-moulded and re-compacted.

Based upon previous testing conducted in our laboratory, homogeneous soil samples with a plasticity index greater than 25 and a clay content greater than 50% will typically have a hydraulic conductivity of 1.0 x 10⁻⁷ cm/sec or less. Sample TH8 3.9-6.0 m had a plasticity index of 18, which does not fall within this range. Hydraulic conductivity testing of a representative Shelby tube sample of this material is recommended to determine its suitability for use as a lagoon liner. The remaining bagged samples were considered suitable for use as a lagoon liner. Our comments regarding the potential use of the material as a lagoon liner are based upon the soil being homogeneous with no preferential flow paths and being properly placed and compacted to maximum density near its optimum moisture content. It should be noted that estimating the hydraulic conductivity of a soil based upon classification test results (plasticity index and particle size analysis) alone might be misleading if the soil contains layers of sand, silt, or organic material.

The hydraulic conductivity results for the 3 Shelby tube samples are less than the specified maximum hydraulic conductivity value of 1.0 x 10⁻⁷ cm/s for lagoon liners.

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Aron Piamsalee, B.Sc., EIT Geotechnical Project Manager

Ann Pinnedee



#### TABLE 2 HYDRAULIC CONDUCTIVITY SUMMARY MYSTERY LAKE WASTE DISPOSAL FACILITY

Sample ID	Depth (m)	Hydraulic Conductivity, "k ₂₀ "
TH3	1.5 – 2.1	8.9 x 10 ⁻⁹ cm/s
TH6	3.0 - 3.6	1.4 x 10 ⁻⁸ cm/s
TH8	3.0 - 3.6	9.9 x 10 ⁻⁹ cm/s



### TABLE 1 SUMMARY OF WATER CONTENT, PARTICLE SIZE, ATTERBERG LIMITS, SOIL CLASSIFICATION TEST DATA MYSTERY LAKE WASTE DISPOSAL FACILITY

	Double		Water	Gravel (%)		Sand (%)		Silt (%) Clay (%)	/ (%)	Dia atia		Soil	Potential Use as a Lagoon	Potential Use as a Lagoon	
Testhole [	Depth (m)	Visual Classification	Content (%)	ontent 75 to ´	Coarse <4.75 to	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	<0.075 to 0.005 mm	<0.005 mm	Limit	Limit	Index	Classification ASTM D2487	linor	Liner when re-moulded and re-compacted
TH3	0.3-4.0	brown, firm, moist, high plasticity clay, trace silt	35.7	0.0	0.0	0.0	0.2	3.4	96.4	62	23	39	CH(Fat Clay)	Yes	Yes
TH3		grey, firm, moist, low plasticity clay, trace silt	32.8	0.0	0.0	0.0	0.1	8.9	91.0	47	19	28	CL(Lean Clay)	Yes	Yes
TH6		brown, stiff, moist, high plasticity clay, trace silt	33.3	0.0	0.0	0.0	0.1	6.5	93.4	62	21	41	CH(Fat Clay)	Yes	Yes
TH6		grey, stiff, moist, high plasticity clay, trace silt	32.6	0.0	0.0	0.0	0.1	6.4	93.5	52	21	31	CH(Fat Clay)	Yes	Yes
TH8	11 4-3 4	brown, stiff, moist, high plasticity clay, trace silt	32.4	0.0	0.0	0.2	0.1	6.9	92.8	66	23	43	CH(Fat Clay)	Yes	Yes
TH8		grey, firm, moist, low plasticity clay, some silt	31.9	0.0	0.0	0.0	0.1	14.4	85.5	36	18	18	CL(Lean Clay)		esting mended
TH12		brown, firm, moist, high plasticity clay, trace silt	33.2	0.0	0.0	0.2	0.1	4.2	95.5	63	23	43	CH(Fat Clay)	Yes	Yes
TH13		brown, firm, moist, high plasticity clay, some silt, trace sand	32.0	0.0	0.0	0.3	1.0	11.7	87.0	63	24	39	CH(Fat Clay)	Yes	Yes

- Notes:

  1.A high speed stirring device was used for 1 minute to disperse the test samples for particle size analysis.

  2.Atterberg limits conducted in accordance with ASTM D4318 Method B (one-point liquid limit).
- 3. The soil samples were air-dried during sample preparation for Atterberg limits and particle size analysis.

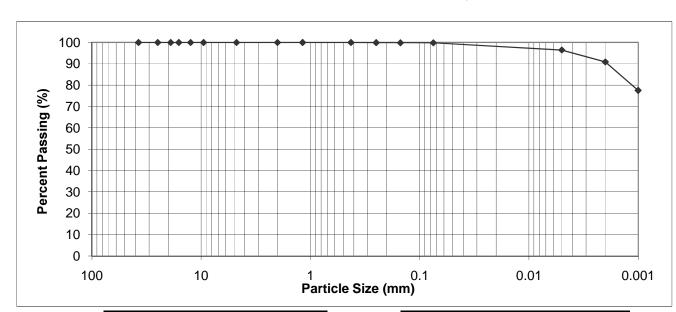


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH3 0.3 - 4.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE		PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0		1.18 mm	100.0
25.00 mm	100.0		0.425 mm	100.0
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	99.9
12.50 mm	100.0		0.075 mm	99.8
9.50 mm	100.0		0.005 mm	96.4
4.75 mm	100.0		0.002 mm	90.9
2.00 mm	100.0		0.001 mm	77.5

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.2	3.4	96.4	77.5

May 27, 2011

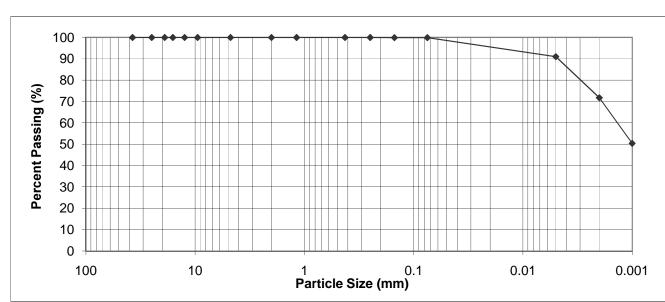


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH3 4.0 - 6.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	100.0
19.00 mm	100.0	0.250 mm	100.0
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.9
9.50 mm	100.0	0.005 mm	91.0
4.75 mm	100.0	0.002 mm	71.7
2.00 mm	100.0	0.001 mm	50.4

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.1	8.9	91.0	50.4

May 27, 2011

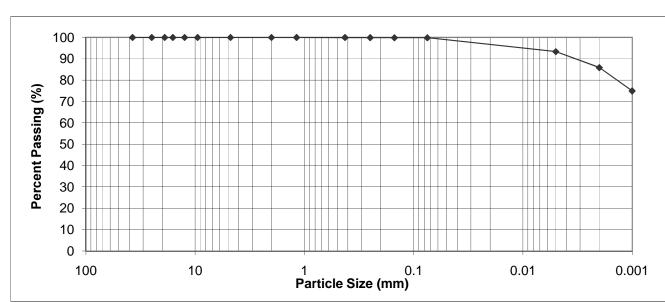


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH6 0.6 - 3.4 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	100.0
19.00 mm	100.0	0.250 mm	99.9
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.9
9.50 mm	100.0	0.005 mm	93.4
4.75 mm	100.0	0.002 mm	85.9
2.00 mm	100.0	0.001 mm	75.0

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.1	6.5	93.4	75.0

May 27, 2011

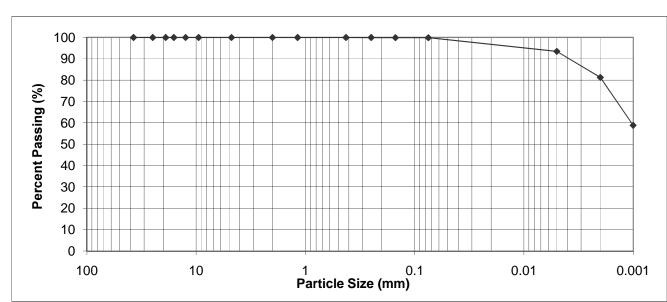


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH6 3.4 - 6.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	100.0
19.00 mm	100.0	0.250 mm	100.0
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.9
9.50 mm	100.0	0.005 mm	93.5
4.75 mm	100.0	0.002 mm	81.3
2.00 mm	100.0	0.001 mm	58.8

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.1	6.4	93.5	58.8

May 27, 2011

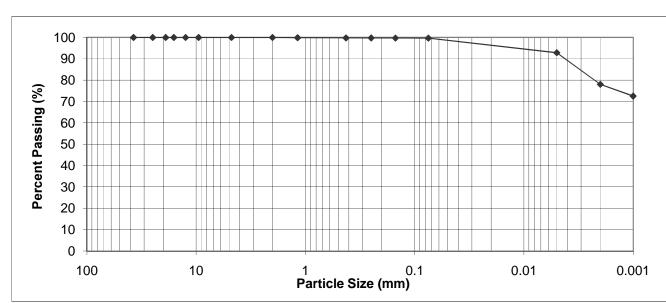


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH8 0.9 - 3.9 m TESTED BY: Larry Presado



PARTICLE	PERCENT	1	PARTICLE	PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0		1.18 mm	99.9
25.00 mm	100.0		0.425 mm	99.8
19.00 mm	100.0		0.250 mm	99.8
16.00 mm	100.0		0.150 mm	99.7
12.50 mm	100.0		0.075 mm	99.7
9.50 mm	100.0		0.005 mm	92.8
4.75 mm	100.0		0.002 mm	78.0
2.00 mm	100.0		0.001 mm	72.5

Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Sand, %  Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.2	0.1	6.9	92.8	72.5

May 27, 2011

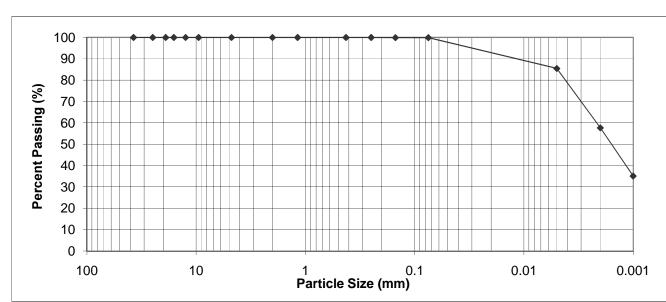


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH8 3.9 - 6.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	100.0
19.00 mm	100.0	0.250 mm	100.0
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.9
9.50 mm	100.0	0.005 mm	85.5
4.75 mm	100.0	0.002 mm	57.7
2.00 mm	100.0	0.001 mm	35.1

Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Sand, %  Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.1	14.4	85.5	35.1

May 27, 2011

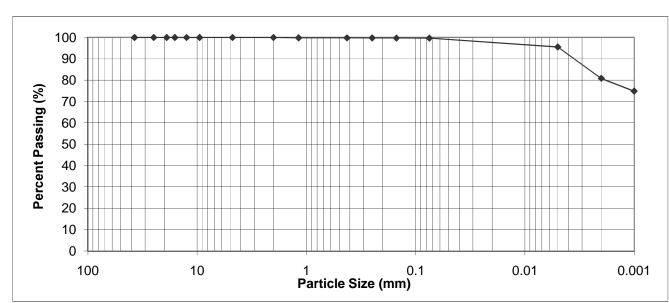


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH12 4.8 - 6.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	1	PARTICLE	PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0		1.18 mm	99.8
25.00 mm	100.0		0.425 mm	99.8
19.00 mm	100.0		0.250 mm	99.8
16.00 mm	100.0		0.150 mm	99.7
12.50 mm	100.0		0.075 mm	99.7
9.50 mm	100.0		0.005 mm	95.5
4.75 mm	100.0		0.002 mm	80.8
2.00 mm	100.0		0.001 mm	74.8

Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Sand, %  Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.2	0.1	4.2	95.5	74.8

May 27, 2011

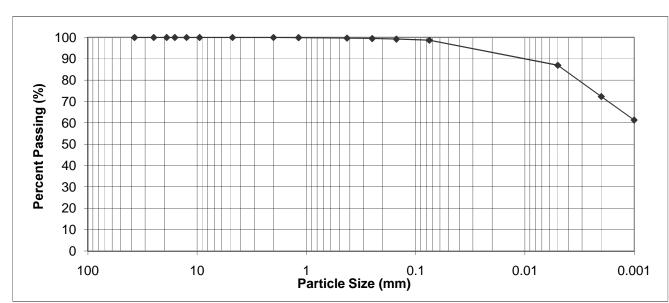


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal

Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: April 21, 2011 SAMPLE ID: TH13 4.5 - 6.0 m TESTED BY: Larry Presado



PARTICLE	PERCENT	1	PARTICLE	PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0	1	1.18 mm	99.9
25.00 mm	100.0		0.425 mm	99.7
19.00 mm	100.0		0.250 mm	99.5
16.00 mm	100.0		0.150 mm	99.2
12.50 mm	100.0		0.075 mm	98.7
9.50 mm	100.0		0.005 mm	87.0
4.75 mm	100.0		0.002 mm	72.3
2.00 mm	100.0		0.001 mm	61.3

Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Sand, %  Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.3	1.0	11.7	87.0	61.3

May 27, 2011



### HYDRAULIC CONDUCTIVITY ASTM D5084

J.R.Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac

SAMPLE I.D.: TH3 1.5 - 2.1 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

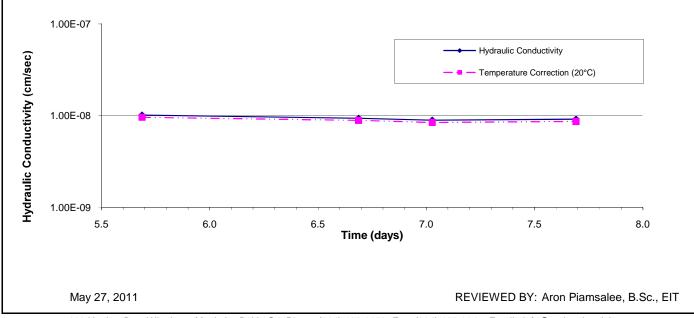
DATE TESTED: April 26 to May 16

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 20.1

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 9.4E-09
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 8.9E-09

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	71.9	72.5	571.7	1.461	31.9	100.5
Final Reading	73.7	72.8	581.6	1.399	35.4	101.7





### HYDRAULIC CONDUCTIVITY ASTM D5084

J.R.Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac

SAMPLE I.D.: TH6 3.0 - 3.6 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

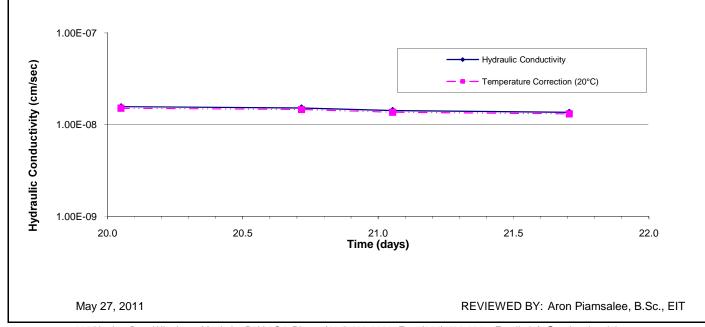
DATE TESTED: April 22 to May 14

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 20.4

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.5E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 1.4E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	71.9	72.7	517.5	1.277	35.8	86.1
Final Reading	72.6	72.6	573.5	1.394	36.8	104.9





### HYDRAULIC CONDUCTIVITY ASTM D5084

J.R.Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac

SAMPLE I.D.: TH8 3.0 - 3.6 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

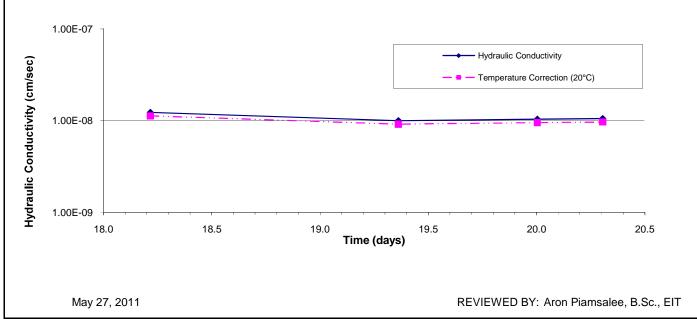
DATE TESTED: April 26 to May 16

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 18.8

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.1E-08 HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 9.9E-09

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	78.5	72.4	618.4	1.446	32.4	99.8
Final Reading	79.0	73.6	631.1	1.383	35.8	100.6



LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase I Works, JR Cousin Consultants Ltd., 2011

#### LGD of MYSTERY LAKE

# Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works



Prepared by:

J. R. Cousin Consultants Ltd.

91A Scurfield Blvd. Winnipeg, Manitoba

R3Y 1G4

September 2011

#### **ACKNOWLEDGMENTS**

To prepare this report various sources of information were investigated and researched. J. R. Cousin Consultants Ltd. (JRCC) wishes to thank the LGD of Mystery Lake who assisted with organization and onsite works.

#### **REMARKS**

Conclusions reached in this report are based upon the generalization of data available to us at the time of forming our opinions. Information in this document may rely on previous studies, investigative work and data by others. JRCC cannot be responsible for actual site conditions proved to be at variance with any generalized data. This report was completed in accordance with generally accepted professional engineering principles and practice. Any use of this report by a third party is the responsibility of the third party, JRCC accepts no responsibility for third party decisions or actions based on the report. No other warranty or guarantee expressed, implied or statutory is made.

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#### **APPENDIX**

Plan 1: Test Hole Location Plan

Plan 2: Topographic Survey Plan with Contour Lines

Plan 2: Past and Future Test Hole Location Plan

Test Hole Logs

National Testing Laboratories Test Results

#### 1.0 INTRODUCTION

J. R. Cousin Consultants Ltd. (JRCC) conducted a geotechnical investigation for the Waste Disposal Ground (WDG) Proposed Phase II Expansion at the LGD of Mystery Lake. The LGD of Mystery Lake existing WDG is located on Part NW ¼ 18, S ½ and NW ¼ 19 in TWP 77-3 WPM and in Part SE ¼ 24-77-4 WPM, approximately 4 km south of the City of Thompson. The proposed Phase II expansion area is east of the existing WDG as shown on Plan 1 attached in the Appendix. The WDG services the LGD of Mystery Lake, the City of Thompson, the Town of Churchill and the Wuskawatim Generating Station. However, the Town of Churchill and the Wuskawatim Generating Station area scheduled to discontinue use of the WDG in the near future.

A total of thirteen test holes were excavated at the WDG proposed Phase II expansion site and borrow pit area. Test hole locations are shown on Plan 1 attached in the Appendix. The test holes were excavated in the proposed Phase II expansion site to determine suitability of the insitu soils for use as a clay landfill liner and in the borrow pit to determine suitability of material for dike and cut-off wall construction.

This report outlines the findings of the geotechnical investigation at the WDG site and evaluates the soils to determine their suitability for use as a landfill liner. The report also identifies potential difficulties (i.e. depth to bedrock, soil types and subsurface water elevations) associated with construction.

#### 2.0 BACKGROUND

Due to wet site conditions at the WDG, the Phase I works cannot be completed in the fall of 2011 as planned. The current active cell has reached maximum capacity and a new active area must be constructed to allow the LGD to dispose waste through the winter and during construction of the Phase I works in the summer of 2012. The LGD of Mystery Lake proposed to construct a lined expansion cell to the east of the municipal waste disposal area as the proposed Phase II works.

The geotechnical investigation was required to evaluate potential use of insitu and re-worked soils as a clay landfill liner and for use in cell dike construction. Bagged soil samples were analysed by a laboratory to assess whether the insitu soils comply with the Manitoba Conservation hydraulic conductivity criteria of  $1 \times 10^{-7}$  cm/sec or less for a landfill liner.

A previous geotechnical and topographic investigation was completed by AECOM in 2005. Eight test holes were excavated around the perimeter of the WDG and three holes were excavated within the former waste cells to determine the depth of waste. Shelby tube samples and laboratory analysis of the soils was not completed and therefore it is unknown if the soils could achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/s insitu or when re-worked.

A geotechnical and topographic investigation was completed by JRCC in April 2011 to access the soils in the Phase I expansion area, the leachate pond area, future expansion areas and through the existing waste to assess the existing landfill liner. Shelby tube samples and laboratory analysis of the soils was

completed and it was determined that insitu clay liners with a hydraulic conductivity of  $1 \times 10^{-7}$  cm/s did exist across the testing area.

#### 3.0 TOPOGRAPHIC INVESTIGATION

The onsite topographic survey was completed on August 18 and 19, 2011. The proposed Phase II expansion area was surveyed with a GPS Total Station. Some areas of thick bush in the proposed Phase II expansion were not surveyed due to loss of satellite reception.

The survey confirmed data obtained during the Phase I topographic survey and evaluated test hole elevations. Elevations in the proposed Phase II Expansion area ranged from 214.70 m in the north end to 225.27 m in the south end.

Contour lines from the topographic survey are shown on Plan 2 attached in the Appendix.

#### 4.0 GEOTECHNICAL FIELD INVESTIGATION

The onsite geotechnical investigation at the LGD of Mystery Lake was conducted on August 18, 2011. Smook Contractors was employed to complete the test holes utilizing a Komatsu 270 track mounted excavator under direct supervision by JRCC's field representative.

A total of thirteen test holes were excavated during the investigation. Ten test holes were excavated in the proposed Phase II expansion area (TH14 – 19 and TH21 - 24), one test hole (TH20) was excavated in the area for future expansion. One test hole (TH25) was excavated in the potential borrow pit area and one test hole (TH26) was excavated on the path from the WDG to the borrow pit area. Test holes were excavated to a depth between 4.1 m and 5.4 m or to bedrock refusal.

#### 4.1 Proposed Phase II Expansion Area

The subsurface soil profile within each test hole was logged, water conditions were noted and representative soil samples were taken as the soils varied along the profile. The samples were visually field-classified. Eight selected bagged samples from the test holes were sealed and submitted to National Testing Laboratories Ltd. for testing and analysis. Details of the laboratory analysis are provided in Section 5.0. Following excavation, the depth of standing water was measured and any caving of the test holes was determined. Test holes were backfilled with the excavated soils and compacted upon termination of excavation. Test hole locations are shown on Plan 1 attached in the Appendix.

#### 4.1.1 Soil Profile

The soil profile in the test holes and the depth of bedrock varied significantly across the test holes taken in the proposed Phase II expansion area. Soil profiles were generalized for TH14 – TH21, TH22 – TH24 and TH25 and TH26. Details of individual test holes can be found in the soils logs attached in the Appendix.

#### Proposed Phase II Expansion Area TH14 - TH21

The average soil profile observed in TH14 – TH21 consisted of an average of 0.5 m of black topsoil followed by a sandy, silty low plastic clay to bedrock. The bedrock elevation varied between 0.6 m below ground in TH18 to 3.7 m below ground in TH15, with an average bedrock elevation of 3.0 m below the surface. TH20 had existing waste from 0-2.2 m below ground and TH21 had a medium plastic clay layer from 1.5-3.4 m below ground.

#### Proposed Phase II Expansion Area TH22 - TH24

The soil profile in TH22 consisted of existing waste from 0-2.4 m below ground and low - medium plastic clay soils from 2.4-4.5 m below ground. TH23 and TH24 consisted of an average of 0.8 m of topsoil followed by medium to high plastic clay to a depth of 4.9 and 5.4 m, respectively. Bedrock was not encountered in the test holes.

#### Borrow Pit Area and Path to Borrow Pit (TH25 and TH26)

TH25 and TH26 found high plastic clay from the ground surface to a depth of 4.1 and 4.2 m, respectively. TH25 became low – medium plastic at 1.6 m below ground surface. Bedrock was not encountered in the test holes.

#### 4.1.2 Groundwater

Short-term groundwater conditions were assessed in each test hole by observing standing water in the test holes prior to backfilling the holes. No standing water was observed in the test holes with the exception of TH20 which had leachate water infiltration at the bottom of the waste layer and TH21 which had high rate water infiltration from the surface.

TH15 was left open for approximately 2 hours to allow longer-term water infiltration to occur. When the hole was re-visited caving of the test hole walls occurred and no standing water was observed.

Groundwater in the test holes depends on high static groundwater conditions and on seasonal conditions, i.e. snowmelt and rainy seasons. Other assumptions relating to the groundwater elevation cannot be made at this time as water levels will normally fluctuate seasonally.

Contractors will be made aware of the geotechnical conditions encountered onsite, as some dewatering of the ground surface may be required during construction.

#### 5.0 LABORATORY TESTING, ANALYSIS AND DISCUSSION

#### 5.1 Laboratory Analysis

Eight representative samples were submitted to National Testing Laboratories Ltd. on August 23, 2011, for analysis and a professional assessment. The analysis included the determination of the following:

- Moisture Content (ASTM D2216)
- Atterberg Limits (plastic limit, liquid limit, and plasticity index, ASTM D4318)
- Soil Classification (ASTM D2487)
- Particle Size Analysis (Hydrometer test, ASTM D422)

The WDG soils were analyzed to determine their suitability as a re-worked or insitu liner for a WDG cell, which requires a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less.

Laboratory analysis of the soils indicated that soils from TH15 and TH21 had a clay content ranging between 61.2% and 73.6% and a Plasticity Index of 12. The soil from TH22 (2.4-4.5 m) had a clay content of 80.2% and a Plasticity Index of 16. The soils from TH23 – TH26 had a clay content ranging from 97.7% to 99.5% and a Plasticity Index between 24 and 45. Based on past experience, the laboratory has commented that homogeneous soils with a plasticity index greater than 25 and a clay content greater than 50% would typically be expected to have a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less.

Based on these comments and Plasticity Index analysis (i.e. Atterberg limits) of the soils indicated that the soils from TH23 (0.4-3.2 m), TH24 (1.2-3.7 m), TH25 (0-1.6 m) and TH26 (0-2.2 m) were considered suitable for use as an insitu clay liner or when re-worked and recompacted. The soils from TH15 (0.6-1.9 m), TH21 (1.5-3.4 m), TH22 (2.4-4.5 m) and TH25 (1.6-4.1 m) had clay contents above 50% but had Plasticity Index less than 25 and therefore hydraulic conductivity testing of the soils would be required to determine if the soils could achieve a hydraulic conductivity of 1 x  $10^{-7}$  cm/sec or less.

Upon further discussion with the National Testing Lab the sample from TH22 (2.4 - 4.5 m) had silt varves within the clay matrix and hydraulic conductivity testing would be highly recommended before use as an insitu clay liner. TH25 (1.6 - 4.5 m) had trace silt varves within the clay matrix. The sample had a high clay content but a low liquid limit as a result of the chemical properties of the clay. National Testing Laboratories has advised the material would

most likely be suitable for use as a landfill liner when re-worked and re-compacted, however it could not be known until hydraulic conductivity testing of the clay is performed.

The results indicate that the suitability of the soils for a clay liner is dependent upon the soils being homogeneous with no preferential flow paths. These preferential flow paths can be caused by lenses of unsuitable material, rocks or boulders or fissures in the soil.

Details of National Testing Laboratories test results and analysis, dated September 2, 2011 are attached in the Appendix.

#### 6.0 WDG CELL LINER REQUIREMENTS

#### **6.1** Current Guidelines

Manitoba Conservation guidelines require that a standard WDG cell clay liner be 1.0 metre in thickness and have a hydraulic conductivity (i.e. the potential rate of fluid movement through the soil) of 1 x  $10^{-7}$  cm/sec or less. This low rate is to protect the underlying groundwater and surrounding lands from leachate seepage. Generally, the higher a soil's plasticity the more likely a soil can achieve a hydraulic conductivity of 1 x  $10^{-7}$  cm/sec.

#### **6.2** Typical Clay Liner Construction Options

The insitu (undisturbed) soils can be used to construct the liner of a WDG cell if the soils can consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less in their insitu state.

If the insitu soils cannot be used, the liner can be constructed by excavating and re-compacting suitable high plastic clay soils to form the liner.

If the clay content of the soils is so low that even when excavated and re-compacted, the soils cannot consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, a liner constructed of high plastic clay from a borrow pit, or a synthetic geomembrane liner would be required.

#### 6.3 Liner for the Proposed Phase II Expansion Cell

The following are the typical options for lining a WDG cell including using the insitu soil if it can achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, re-working and re-compacting the existing soil or clay soil from a borrow source to achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, or utilizing a synthetic geomembrane liner.

#### 6.3.1 Insitu Soil

Based on the geotechnical investigation and laboratory analysis the soils in the proposed Phase II expansion area under TH14 – 22 are not capable of achieving an insitu hydraulic conductivity of  $1 \times 10^{-7}$  cm/s.

The soils below the surficial topsoil in the vicinity of TH23 – TH24 are suitable for use as an insitu clay liner. The clay under the existing waste layer in TH22 may be suitable for use as an insitu clay liner if additional hydraulic conductivity tests are completed. Additional test holes and laboratory testing are required in the vicinity of TH22 to determine the edge of the 1.0 m thick insitu suitable clay. Future test hole locations are shown on Plan 3 attached in the Appendix.

Once the edge of the horizontal clay liner in determined, vertical cut-off walls in the WDG perimeter dikes would be made of re-worked and re-compacted clay soils and extended a minimum of 1.0 m into the insitu clay horizontal liner creating the east WDG border.

Using the insitu clay for the horizontal bottom liner in the proposed Phase II expansion area would be possible, provided that the soils are uniform throughout the proposed construction area and no preferential flow paths exist.

If some unsuitable soils or boulders are encountered during excavation of the cell, they need to be removed and replaced with re-worked medium to high plastic clay from a borrow site or from previously excavated material.

#### 6.3.2 Re-Worked Soil

The soils below the surficial topsoil (or existing waste) layer in the vicinity of TH22 – TH24 would most likely be suitable for use as a clay liner when re-worked and recompacted. In this option (re-worked clay option) approximately 1.25 m of suitable clay soil would be excavated from its native state and re-worked and re-compacted to form a minimum 1.0 m thick horizontal clay liner. The vertical cut-off walls in the WDG perimeter dikes would be made of re-worked and re-compacted clay soils extended a minimum of 1.0 m into the insitu clay horizontal liner.

This re-worked clay option would provide a lower hydraulic conductivity in the horizontal layer and reduce the risk of not meeting the Manitoba Conservation guideline of a hydraulic conductivity of 1 x 10⁻⁷ cm/sec or less in the liner. However, this would add significant cost to the project and based on the laboratory analysis of bagged samples taken at the site in TH23 and TH24, the insitu hydraulic conductivity meets the guidelines and re-compaction of the bottom liner is not necessary.

Based on the geotechnical investigation and laboratory analysis the soils in the proposed Phase II expansion area under TH14 - 21 are not capable of achieving a hydraulic conductivity of 1 x  $10^{-7}$  cm/s when re-worked and re-compacted. If expansion was to occur over this area, a minimum 1.0 m thick clay liner would have to be hauled from a borrow pit and re-compacted and re-worked.

The clay soils from the borrow area were found to be marginally suitable for use as a landfill liner when re-worked and re-compacted. The sample from TH25 (1.6 - 4.1 m) had a high clay content (98.8%), but a low liquid limit (45) which resulted in a plasticity index of 24. The sample was deemed a lean clay and hydraulic conductivity testing was recommended prior to use as a landfill liner. Before use of the borrow pit soil, it is recommended that additional test holes in the borrow pit area be conducted as well as reworked hydraulic conductivity testing of the sample from TH25 (1.6 - 4.1 m). Future test hole locations are shown on Plan 3 attached in the Appendix.

#### **6.3.3** Geomembrane Liner

The WDG liner could be constructed with a synthetic geomembrane liner, using insitu soils as the bedding material for the liner and sand from a borrow pit used as a liner cover. The cost of installing a geomembrane liner would be significantly greater than utilizing re-worked and re-compacted clay from the borrow pit.

#### 6.3.4 Summary

The clay soils east of the WDG in the vicinity of TH23 – 24 can be utilized as an insitu clay liner. Additional test holes and laboratory testing are required in the vicinity of TH22 to determine the edge of the 1.0 m thick suitable clay liner. The soil east of TH22 – 24 under TH14 – TH21 cannot be utilized as a landfill liner whether re-worked or recompacted and if expansion was to occur over this area a minimum 1.0 m thick clay liner would have to be hauled from the borrow pit and re-worked and re-compacted. Additional soils testing in the borrow pit and additional laboratory analysis of the borrow pit soil is required before use as a landfill liner.

#### 7.0 SUMMARY, RECOMMENDATIONS AND CLOSURE

#### 7.1 Summary

The topographic survey at the WDG confirmed the data obtained during the Phase I topographic survey and evaluated test hole elevations. The survey found the elevations is the proposed Phase II expansion area ranged between 214.70 at the north end to 225.77 m in the south end.

Soils at the existing WDG were investigated by JRCC. Representative soil samples were analyzed by National Testing Laboratories Ltd. to determine their suitability for a clay liner.

Based on the geotechnical investigation and laboratory analysis, the clay in the vicinity of TH23 – 24 is suitable for use as an insitu clay liner. Additional test holes and laboratory testing are required in the vicinity of TH22 to determine the edge of the 1.0 m thick suitable clay liner.

The soils in the area of TH14 - 21 are not suitable for use as a clay liner insitu or when re-worked and re-compacted. If the landfill was expanded in this area a minimum 1.0 m thick horizontal clay liner would be required to be hauled from the borrow pit and re-worked and re-compacted. Additional soils testing in the borrow pit and additional laboratory analysis of the borrow pit soil is required before use as a landfill liner.

The soils from the borrow pit were found to be marginally suitable for use as a landfill liner when re-worked and re-compacted and additional test holes and laboratory analysis including hydraulic conductivity testing is required before use as a landfill liner.

The vertical cut-off walls in the WDG perimeter dikes and the leachate pond dikes would have to be made of re-worked and re-compacted clay soils extended a minimum of 1.0 m into the insitu clay horizontal liner.

No water infiltration was observed in the test holes, with the exception of TH20 which had leachate water infiltration at the bottom of the waste layer and TH21 which had high rate water infiltration from the surface. Contractors will have to be made aware of these conditions prior to construction, however water levels can vary seasonally.

#### 7.2 Recommendations

It is recommended that a perimeter dike with vertical cut-off walls extending a minimum 1.0 m into the horizontal clay liner wall be installed at the edge of the suitable horizontal clay liner. The location of the edge of the horizontal clay liner will be determined by further soils testing in the vicinity of TH22. If expansion in the area under TH14 -21 is required it is recommended a minimum 1.0 m thick clay liner from the borrow pit be hauled and re-worked and re-compacted. Additional soils testing in the borrow pit and additional laboratory analysis of the borrow pit soil is required before use as a landfill liner. Future test hole locations are shown on Plan 3 attached in the Appendix.

#### 7.3 Closure

The conclusions and recommendations in this report are based on the results of the site investigation and laboratory analysis. In addition, soil and groundwater conditions between test hole locations were generalized to provide an overall assessment of the geotechnical site conditions. If conditions that appear different from those encountered at the test hole locations as described in this report, or if the assumptions stated herein are not in agreement with the design, JRCC should be informed in order that the recommendations can be reviewed and adjusted as required.

The site investigation was conducted for the purpose of identifying geotechnical conditions at the potential expansion cell sites and leachate pond site. Although no environmental issues were identified during the site investigation, it does not necessarily follow that such issues do not exist. If the client or any other parties have any environmental concerns regarding the proposed site and works, an appropriate environmental assessment must be conducted.

It is not uncommon for soil conditions to be highly variable across a site. Previous construction activities and placement of fill at a site can augment the variability of soil conditions, especially surficial soil conditions. A contingency must be included in any construction budget to allow for potential variations in soil conditions, which may result in modification of the design and construction procedures.

#### 8.0 NEXT STEPS

The following are the additional geotechnical investigations which must be performed at the LGD of Mystery Lake WDG. Test holes and laboratory analysis must be completed east of the existing WDG in the vicinity of TH22 to determine the extent of the insitu clay liner. Additional soils testing in the borrow pit is required as well as laboratory analysis including hydraulic conductivity testing to determine if the soils are suitable for use as a waste disposal ground liner. Future test hole locations are shown on Plan 3 attached in the Appendix.

Item #	Task	Schedule	Reason
1	Additional test holes and laboratory	Prior to Phase I	To evaluate the actual hydraulic
	analysis of soils from the borrow pit	construction	conductivity of the borrow soil
	including re-worked hydraulic	works	and to evaluate remainder of
	conductivity testing		borrow pit soils
2	Additional test holes east of the	Prior to dike	To determine east boundary of
	existing WDG	construction east	1.0 m thick insitu clay liner
		of the WDG	
3	Insitu Shelby tube samples and	Prior to dike	To determine if the hydraulic
	hydraulic conductivity testing of	construction east	conductivity of the clay is suitable
	soils in the vicinity of TH22	of the WDG	for an insitu liner

### **APPENDIX**

Plan 1: Test Hole Location Plan

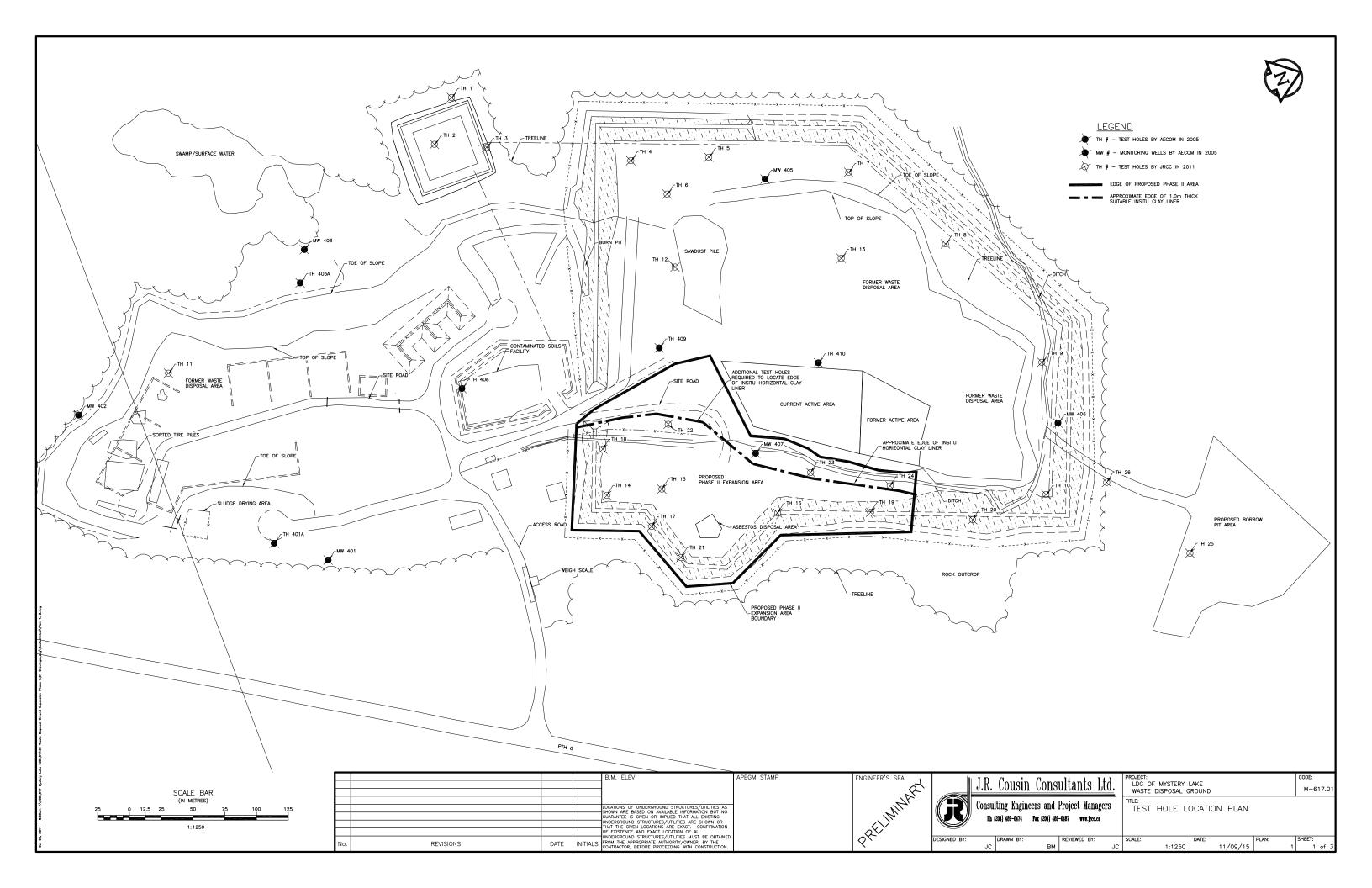
Plan 2: Topographic Survey Plan with Contour Lines

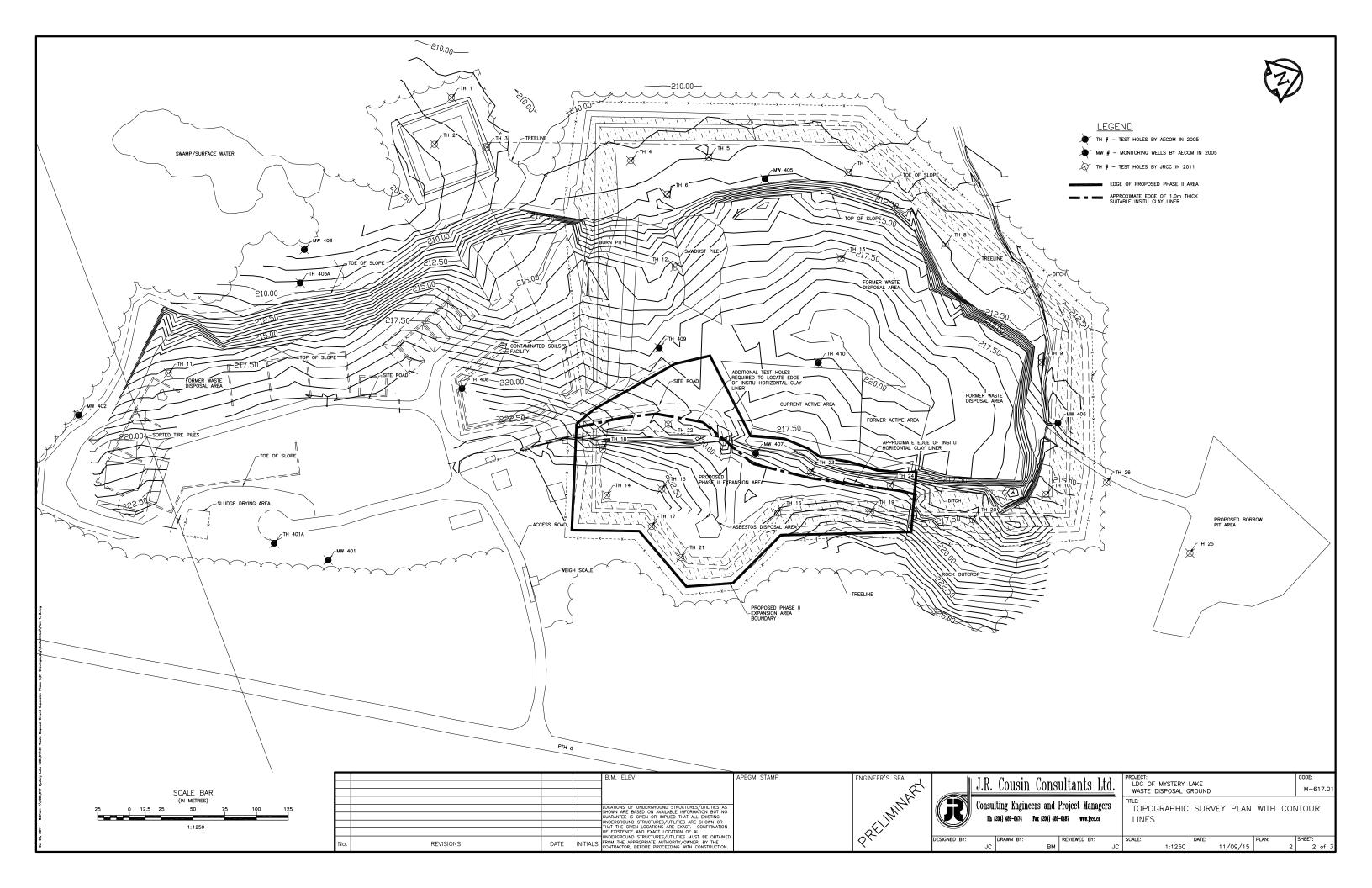
Plan 3: Past and Future Test Hole Location Plan

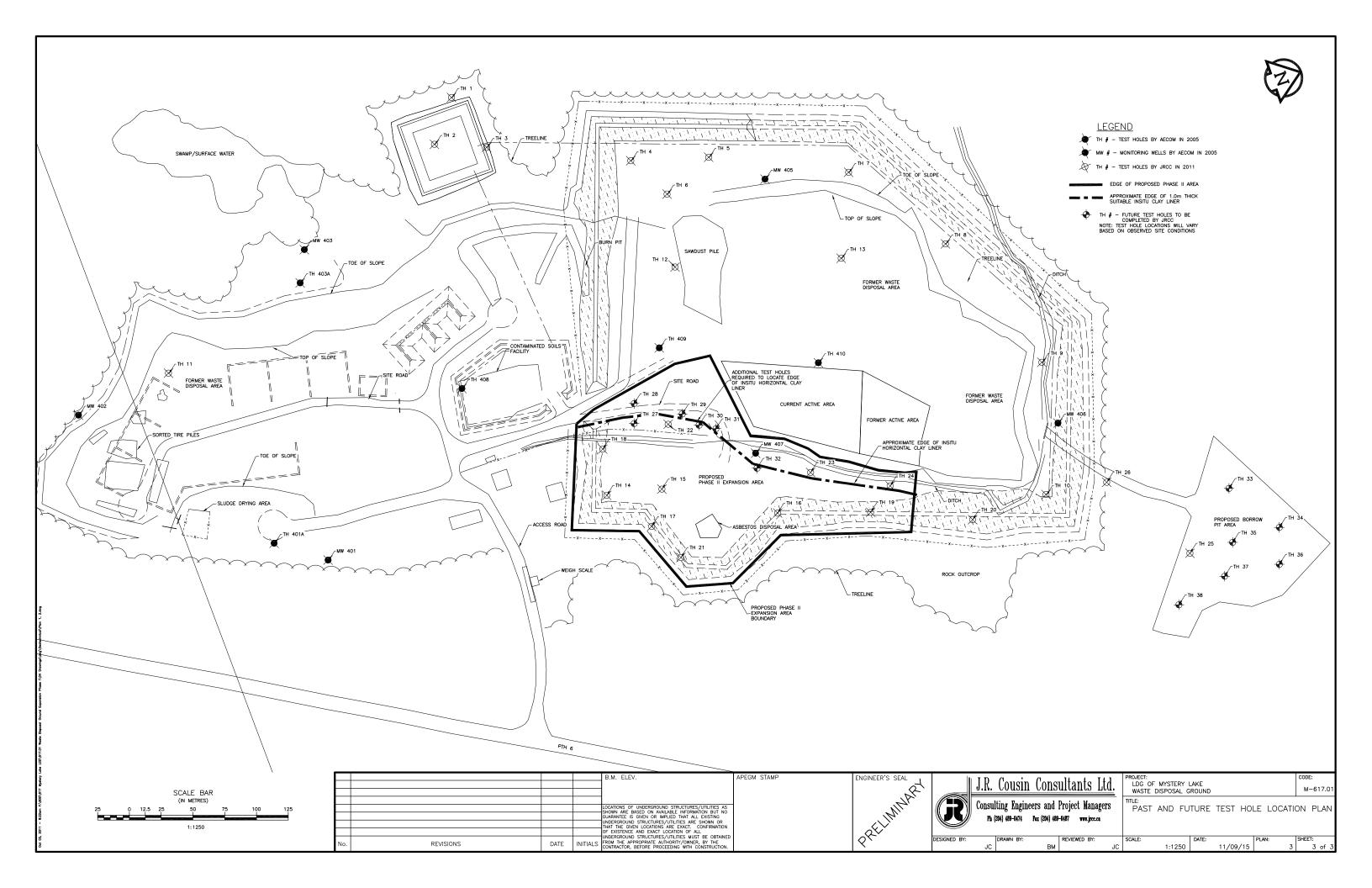
Test Hole Logs

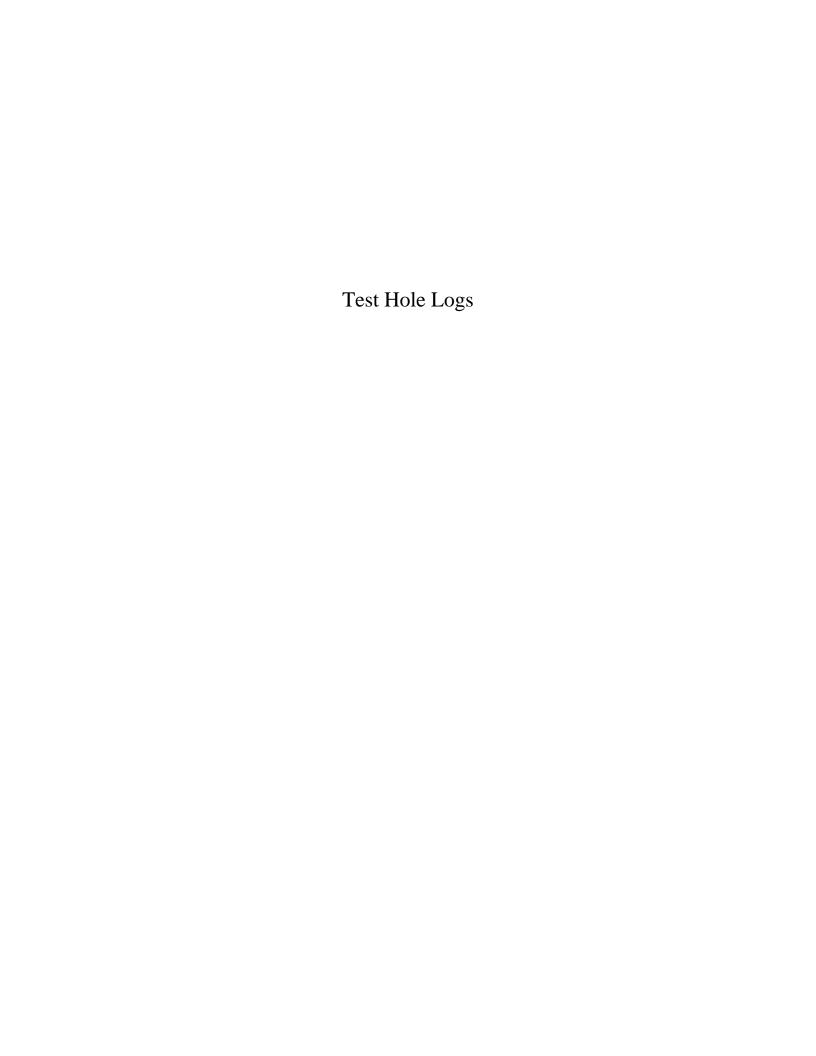
National Testing Laboratories Ltd. Test Results











## J. R. Cousin Consultants Ltd. TEST HOLE LOGS

#### SYMBOL INDEX

SYMBOL INDEX	
GW. : Well graded gravels and gravel sand mixtures, little or no fines	
GP. : Poorly graded gravels, gravel - sand mixtures, little or no fines	
GM. : Silty gravels, gravel-sand-silt mixtures	
GC. : Clayey gravels, gravel-sand-clay mixtures	
SW.: Well graded sands, gravelly sands, little or no fines	
SP.: Poorly graded sands, or gravelly sands, little or no fines	
SM. : Silty sands, sand-silt mixtures	
SC. : Clayey sands, sand-clay mixtures	
ML. : Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity	
CL. : Inorganic clays of low plasticity, gravelly clays, sandy or silty clays, lean clays	
OL. : Organic silts and organic silty clays of low plasticity	
CI. : Inorganic clays of medium or intermediate plasticity	
MH. : Inorganic silts, fine sandy or silty soils	
CH.: Inorganic clays of high plasticity, fat clays	
OH. : Organic clays of medium to high plasticity, organic silts	Ta c s c t
Pt. : Peat, humus, swamp soils with high organic contents	t n

TOPSOIL

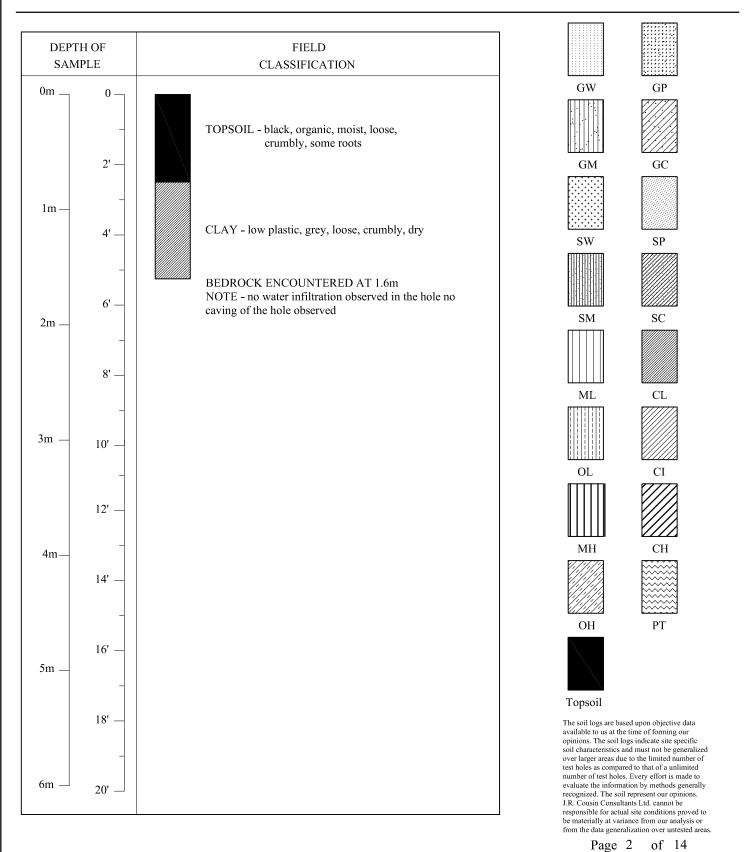
The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized over larger areas due to the limited number of test holes as compared to that of an unlimited number of test holes. Every effort is made to evaluate the information by methods generally recognized. The soil logs represent our opinions. J. R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

LOCATION: 6171164.05 N

568051.39 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 225.45 m

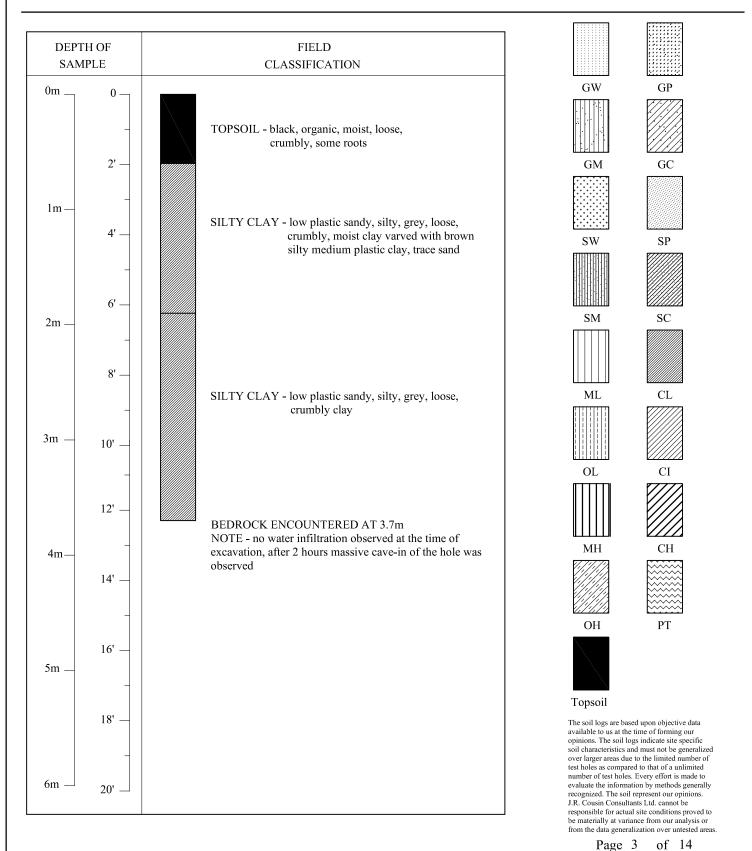


LOCATION: 6171206.45 N

568062.06 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 223.54 m

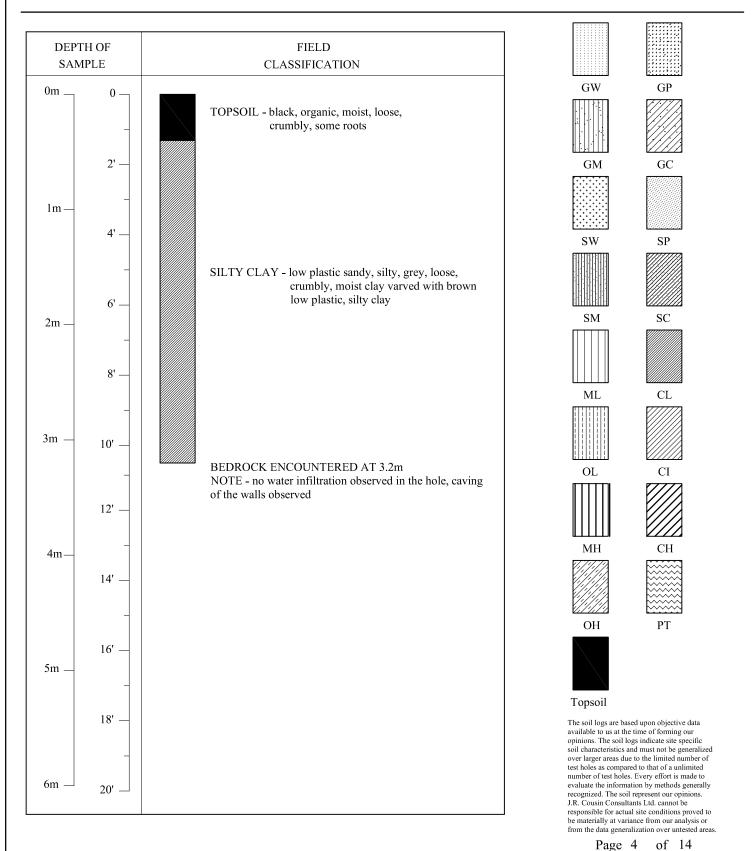


LOCATION: 6171285.89 N

568110.39 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 220.171 m

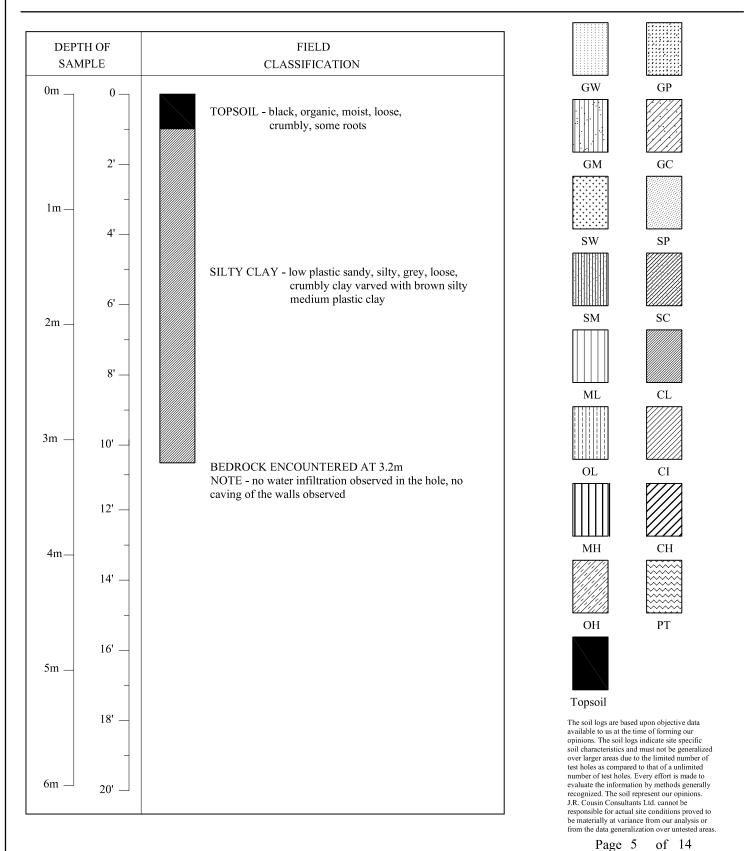


LOCATION: 6171189.12 N

568086.25 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 223.52 m



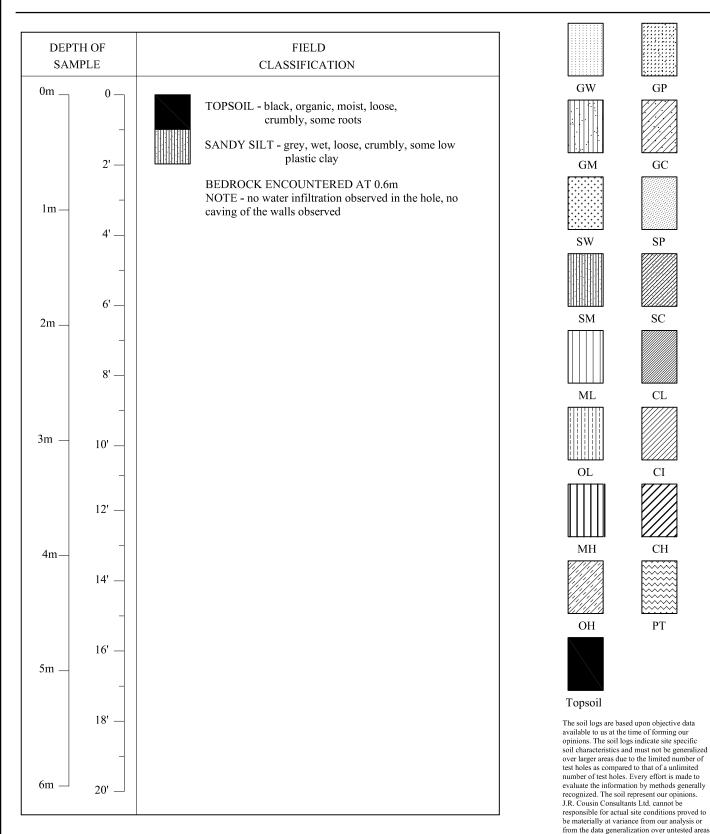
LOCATION: 6171173.25 N

568016.04 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: August 18, 2011 ELEVATION: 221.84 m

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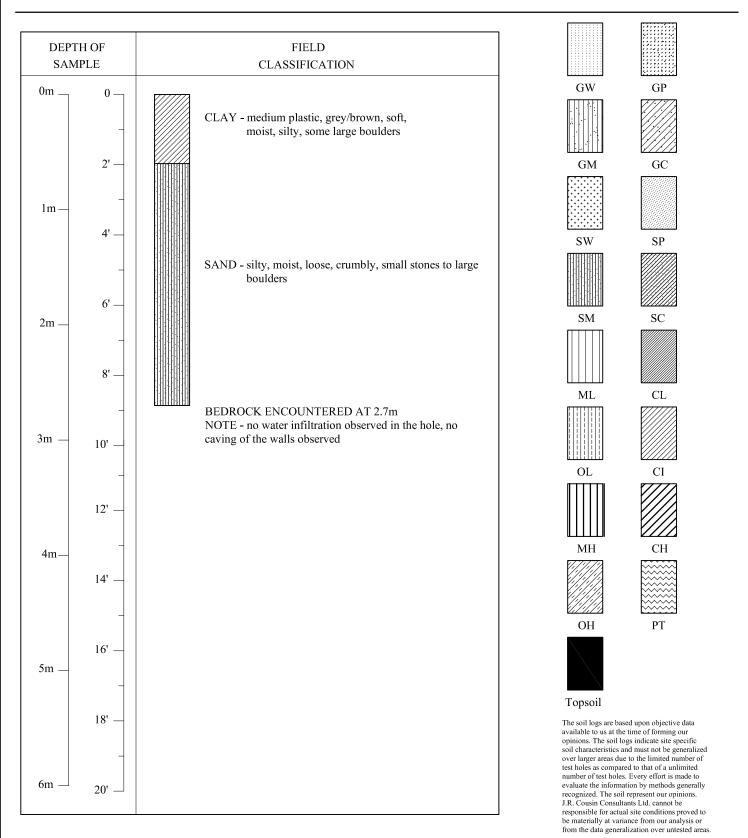
LOCATION: 6171355.00 N

568134.37 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 220.78 m

Page <u>7</u> of <u>14</u>



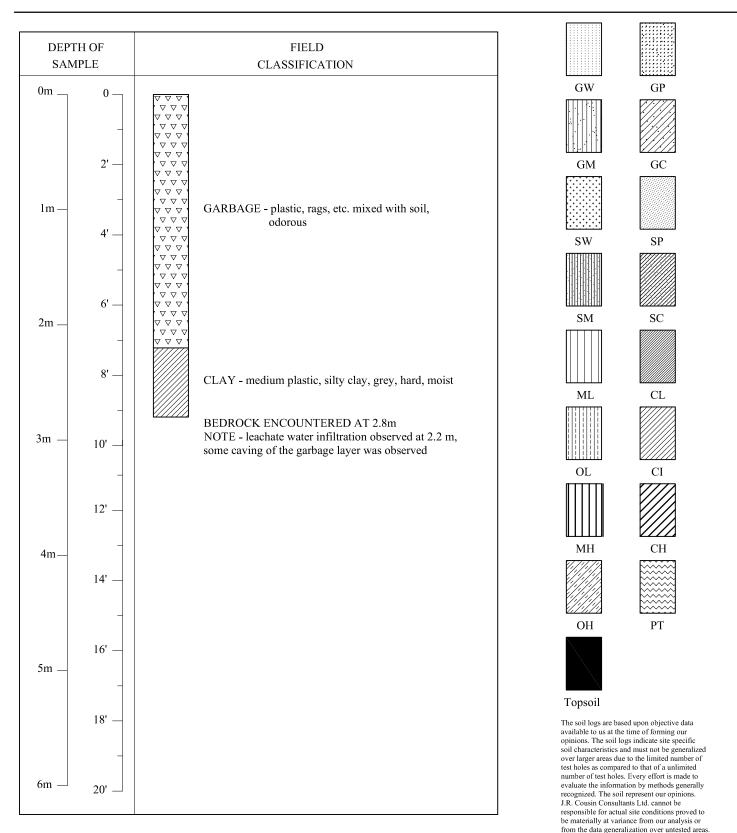
LOCATION: 6171428.64 N

568166.80 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 216.93 m

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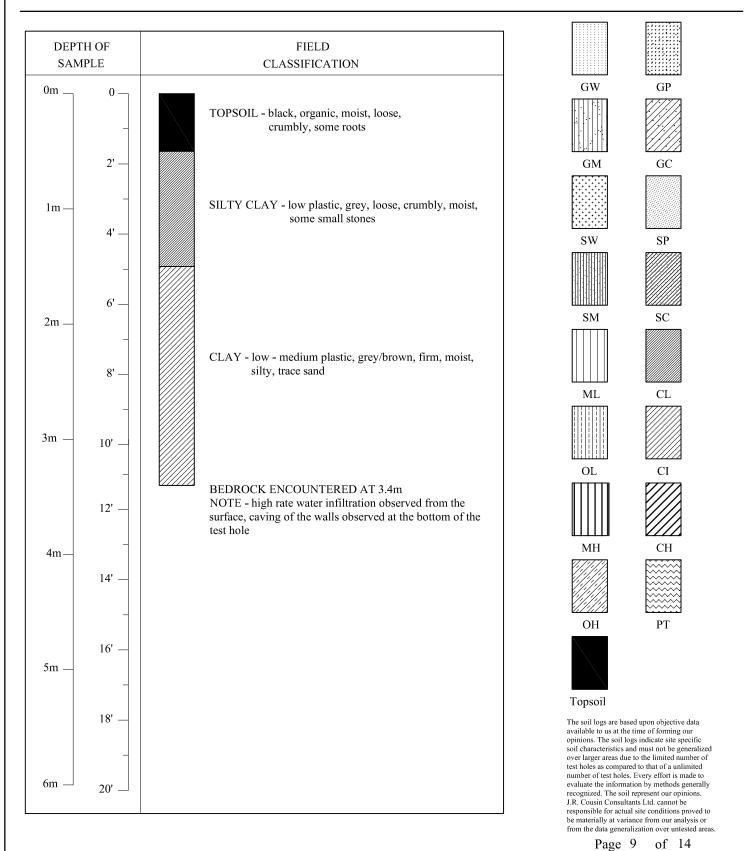


LOCATION: 6171202.60 N

568117.02 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 221.127 m

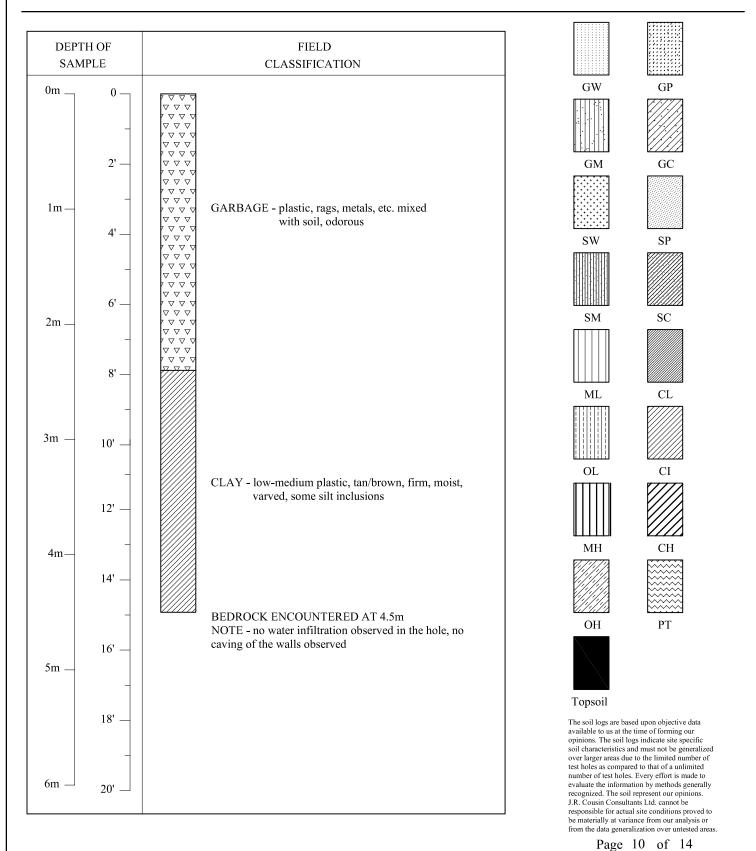


LOCATION: 6171228.22 N

568015.67 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 219.30 m

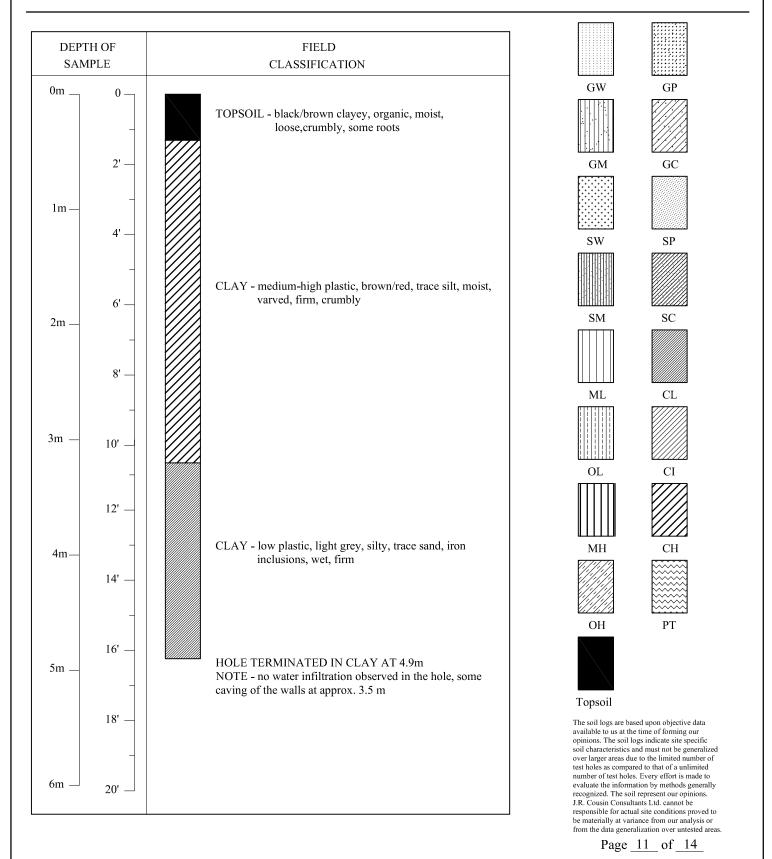


LOCATION: 6171321.04 N

568089.01 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 218.23 m

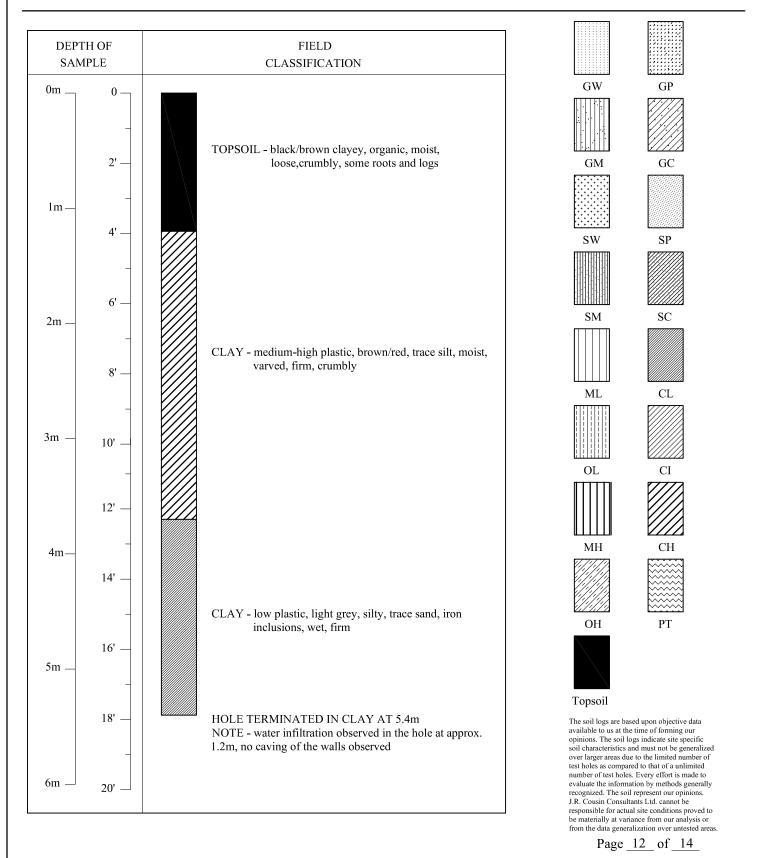


LOCATION: 6171376.48 N

568119.97 E

PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 217.38 m



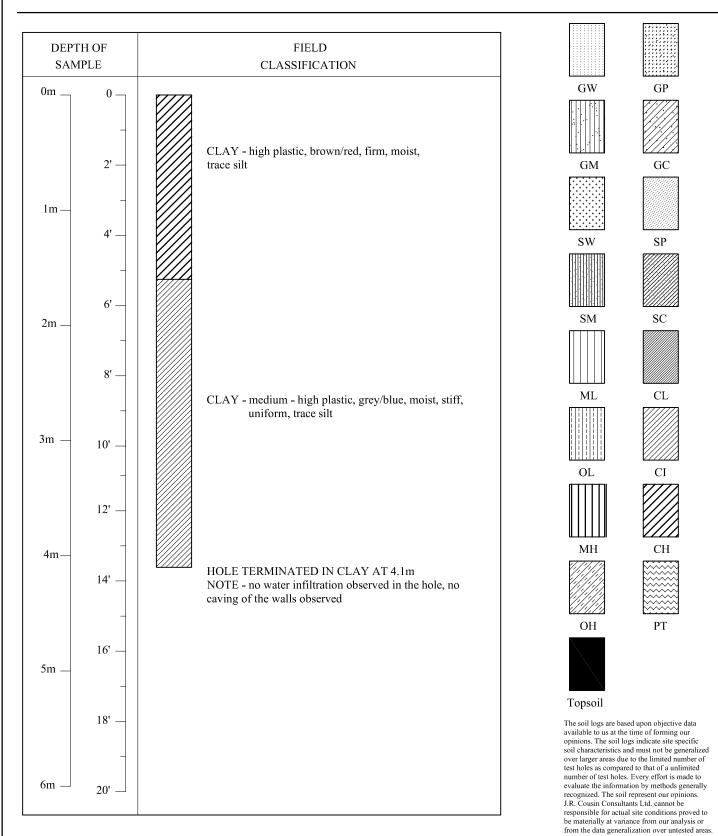
LOCATION: 6171580.87 N

568249.03 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 213.89 m

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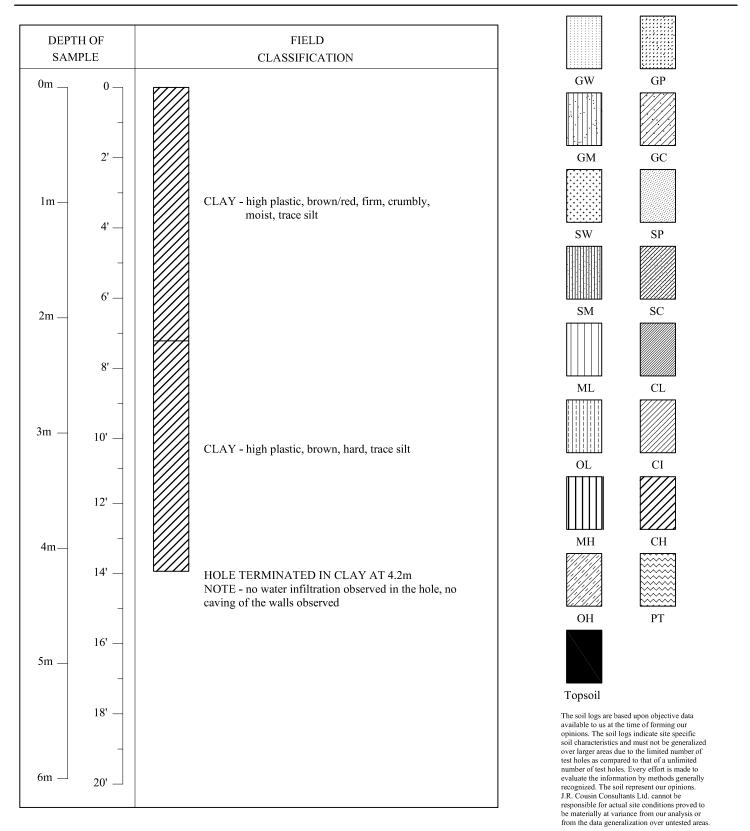
LOCATION: 6171537.90 N

568174.49 E

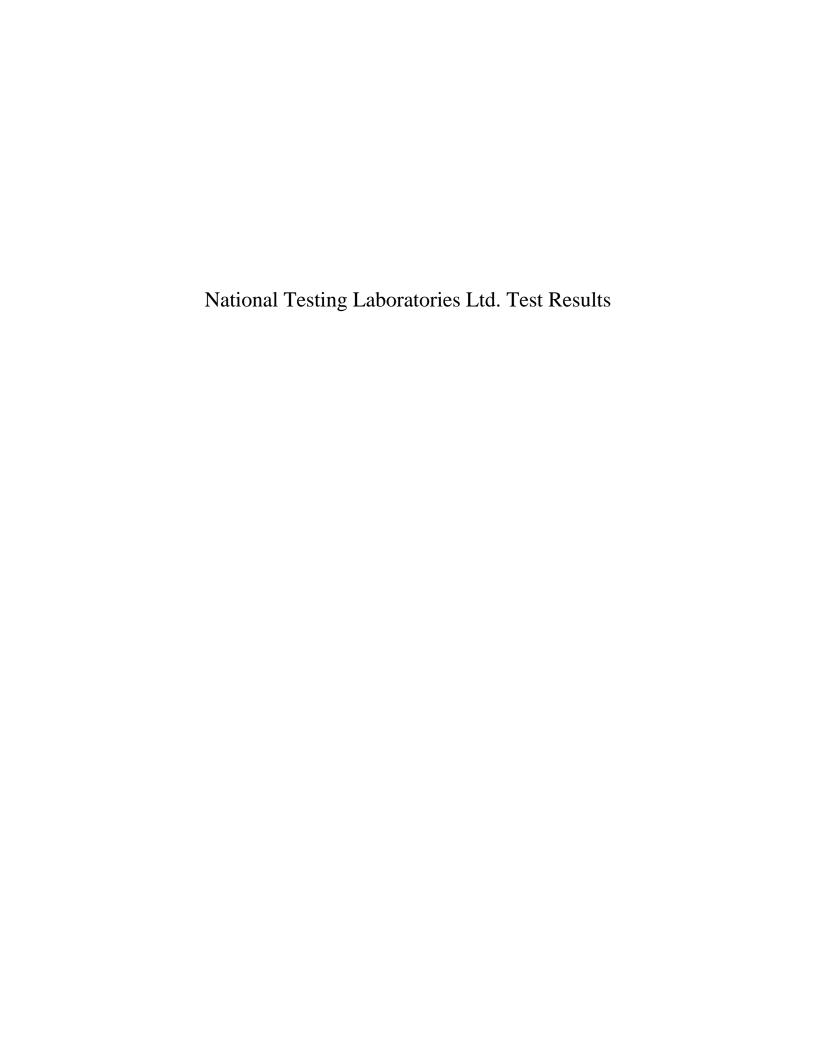
PROJECT : LGD of Mystery Lake - Waste Disposal Ground

DATE : August 18, 2011 ELEVATION : 214.76 m

TEST HOLE # 26



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199 Henlow Bay Winnipeg, MB R3Y 1G4 Phone (204) 488-6999 Fax (204) 488-6947 Email info@nationaltestlabs.com www.nationaltestlabs.com

J.R. Cousin Consultants Ltd. 91 A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 September 2, 2011

Project: Mystery Lake Waste Disposal Facility

Soil samples were submitted to our laboratory on August 23, 2011. The following tests were conducted on selected soil samples:

Attention: Brett McCormac

- water content (ASTM D2216)
- particle size analysis (ASTM D422)
- liquid limit, plastic limit, and plasticity index (ASTM D4318)
- soil classification (ASTM D2487)
- visual classification

The test results for the soil samples are summarized in the following tables and in the attached particle size analysis.

An assessment of the bagged soil samples was conducted to determine whether the soil represented by the bagged samples could be used in-situ as a waste disposal ground liner and would obtain a hydraulic conductivity of less than  $1.0 \times 10^{-7}$  cm/sec without being reworked, and when re-moulded and re-compacted.

Based upon previous testing conducted in our laboratory, homogeneous soil samples with a plasticity index greater than 25 and a clay content greater than 50% will typically have a hydraulic conductivity of 1.0 x 10⁻⁷ cm/sec or less. Samples TH15 0.6-1.9 m, TH21 1.5-3.4 m, TH22 2.4-4.5 m, and TH25 1.6-4.1 m all had plasticity indexes of below 25. Hydraulic conductivity testing of these materials is recommended to determine their suitability for use as a waste disposal ground liner. The remaining bagged samples were considered suitable for use as a waste disposal ground liner. Our comments regarding the potential use of the material as a waste disposal ground liner are based upon the soil being homogeneous with no preferential flow paths and being properly placed and compacted to maximum density near its optimum moisture content. It should be noted that estimating the hydraulic conductivity of a soil based upon classification test results (plasticity index and particle size analysis) alone might be misleading if the soil contains layers of sand, silt, or organic material.

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Aron Piamsalee, B.Sc., EIT Geotechnical Project Manager

Ann Pinnadee



### TABLE 1 SUMMARY OF WATER CONTENT, PARTICLE SIZE, ATTERBERG LIMITS, SOIL CLASSIFICATION TEST DATA MYSTERY LAKE WASTE DISPOSAL FACILITY

	<b>5</b> .1		Water (	Gravel (%)		Sand (%)			Clay (%)		<b>.</b>	<b>.</b>	Soil	Potential Use as a waste disposal	Potential Use as a waste disposal
Testhole	Depth (m)	Visual Classification	Content (%)	75 to ´ 4.75 mm	mm Coarse <4.75 to	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	<0.075 to 0.005 mm	<0.005 mm	Liquid Limit	Limit	Plasticity Index	ASTM D2487	liner without being	ground liner when re-moulded and re- compacted
TH15	0.6-1.9	tan to brown, firm to stiff, moist, low plasticity clay, silty, trace sand	25.9	0.4	0.2	0.4	1.7	23.7	73.6	29	17	12	CL(Lean Clay)		esting mended
TH21	1.5-3.4	brown, firm, moist, low plasticity clay, silty, trace sand	25.3	0.0	0.2	1.2	6.6	30.8	61.2	27	15	12	CL(Lean Clay)		esting mended
TH22	2.4-4.5	tan to brown, firm to stiff, moist, low plasticity clay, some silt	31.5	0.0	0.0	0.1	0.1	19.6	80.2	32	16	16	CL(Lean Clay)		esting mended
TH23	0.4-3.2	brown, firm to stiff, moist, high plasticity clay	34.6	0.0	0.0	0.1	0.2	0.2	99.5	70	25	45	CH(Fat Clay)	Yes	Yes
TH24	1.2-3.7	brown, stiff, moist, high plasticity clay	34.7	0.0	0.0	0.1	0.2	0.5	99.2	60	23	37	CH(Fat Clay)	Yes	Yes
TH25	U-1 h	brown, firm, moist, high plasticity clay	34.2	0.0	0.0	0.0	0.3	0.4	99.3	63	24	39	CH(Fat Clay)	Yes	Yes
TH25	1 0-4 1	tan to brown, stiff, moist, low plasticity clay, trace silt	31.6	0.0	0.0	0.1	0.1	1.0	98.8	45	21	24	CL(Lean Clay)		esting mended
TH26		brown, firm, moist, high plasticity clay, trace silt	29.3	0.0	0.0	0.1	0.4	1.8	97.7	57	20	37	CH(Fat Clay)	Yes	Yes

- Notes:

  1. A high speed stirring device was used for 1 minute to disperse the test samples for particle size analysis.

  2. Atterberg limits conducted in accordance with ASTM D4318 Method B (one-point liquid limit).
- 3. The soil samples were air-dried during sample preparation for Atterberg limits and particle size analysis.

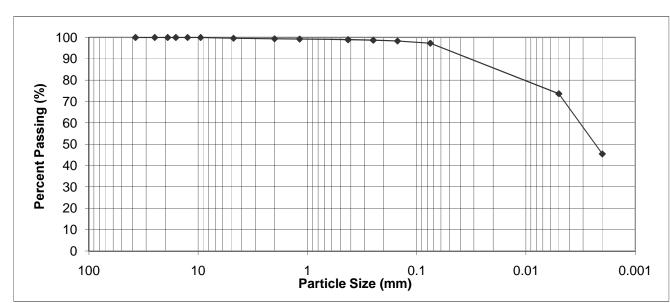


PROJECT: Mystery Lake Waste Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH15 0.6-1.9 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	]	PARTICLE	PERCENT
SIZE	PASSING		SIZE	
37.50 mm	100.0	1	1.18 mm	99.3
25.00 mm	100.0		0.425 mm	99.0
19.00 mm	100.0		0.250 mm	98.7
16.00 mm	100.0		0.150 mm	98.4
12.50 mm	100.0		0.075 mm	97.3
9.50 mm	100.0		0.005 mm	73.6
4.75 mm	99.6		0.002 mm	45.4
2.00 mm	99.4		0.001 mm	NT

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.4	0.2	0.4	1.7	23.7	73.6	NT

Note: Colloids content not tested

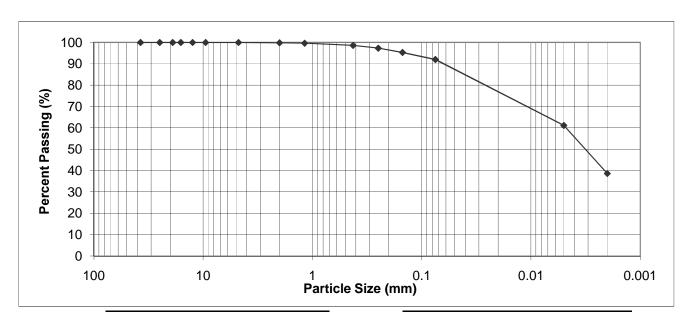


PROJECT: Mystery Lake Waste Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH21 1.5-3.4 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT		PARTICLE	PERCENT
SIZE	PASSING		SIZE	
37.50 mm	100.0	1.18 mm		99.7
25.00 mm	100.0		0.425 mm	98.6
19.00 mm	100.0		0.250 mm	97.3
16.00 mm	100.0		0.150 mm	
12.50 mm	100.0		0.075 mm	92.0
9.50 mm	100.0		0.005 mm	61.2
4.75 mm	100.0	0.002 mm		38.6
2.00 mm	99.8		0.001 mm	NT

			Sand, %		Silt, % <0.075 to 0.005 mm		Colloids, % < 0.001 mm	
	Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm		Clay, % <0.005 mm		
ſ	0.0	0.2	1.2	6.6	30.8	61.2	NT	

Note: Colloids content not tested

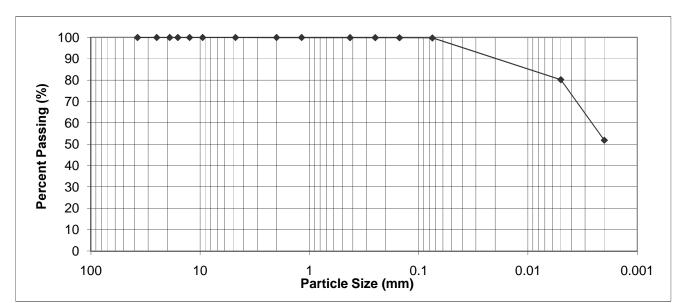


PROJECT: Mystery Lake Waste Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH22 2.4-4.5 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	]	PARTICLE	
SIZE	PASSING	SIZE		PASSING
37.50 mm	100.0		1.18 mm	100.0
25.00 mm	100.0		0.425 mm	99.9
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	99.9
12.50 mm	100.0		0.075 mm	99.8
9.50 mm	100.0		0.005 mm	80.2
4.75 mm	100.0		0.002 mm	51.8
2.00 mm	100.0		0.001 mm	NT

	Gravel, % 75 to 4.75 mm		Sand, %				
		Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
	0.0	0.0	0.1	0.1	19.6	80.2	NT

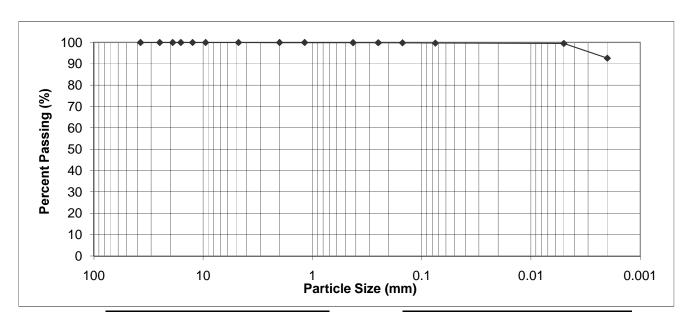
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH23 0.4-3.2 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT		PARTICLE	PERCENT
SIZE	PASSING	SIZE		PASSING
37.50 mm	100.0	1.18 mm		100.0
25.00 mm	100.0		0.425 mm	99.9
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	
12.50 mm	100.0		0.075 mm	99.7
9.50 mm	100.0		0.005 mm	99.5
4.75 mm	100.0	0.002 mm		92.6
2.00 mm	100.0		0.001 mm	NT

		Sand, %		Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm	
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm				
0.0	0.0	0.1	0.2	0.2	99.5	NT	

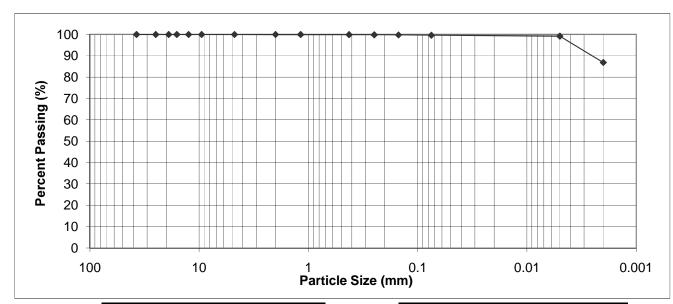
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH24 1.2-3.7 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	PARTICLE		PERCENT
SIZE	PASSING	SIZE		PASSING
37.50 mm	100.0	1.18 mm		100.0
25.00 mm	100.0		0.425 mm	99.9
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	
12.50 mm	100.0		0.075 mm	99.7
9.50 mm	100.0		0.005 mm	
4.75 mm	100.0	0.002 mm		86.8
2.00 mm	100.0		0.001 mm	NT

		Sand, %					
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm	
0.0	0.0	0.1	0.2	0.5	99.2	NT	

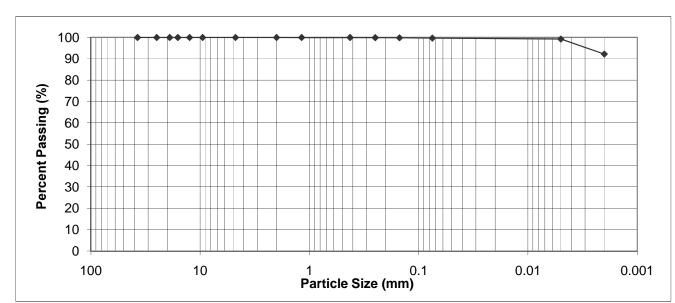
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH25 0.0-1.6 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	]	PARTICLE	PERCENT
SIZE	PASSING		SIZE	
37.50 mm	100.0		1.18 mm	100.0
25.00 mm	100.0		0.425 mm	100.0
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	99.8
12.50 mm	100.0		0.075 mm	99.7
9.50 mm	100.0		0.005 mm	99.3
4.75 mm	100.0		0.002 mm	92.2
2.00 mm	100.0		0.001 mm	NT

	Sand, %			011. 07		
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.3	0.4	99.3	NT

Note: Colloids content not tested

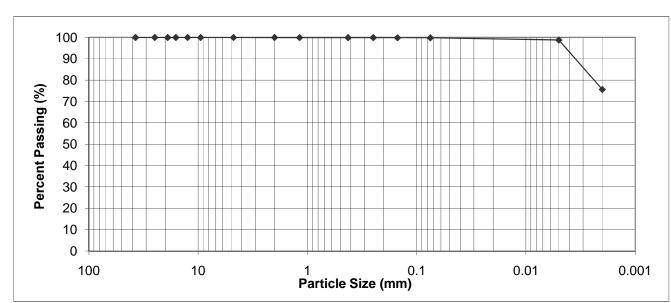


PROJECT: Mystery Lake Waste Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH25 1.6-4.1 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	]	PARTICLE	PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0		1.18 mm	100.0
25.00 mm	100.0		0.425 mm	99.9
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	99.9
12.50 mm	100.0		0.075 mm	99.8
9.50 mm	100.0		0.005 mm	98.8
4.75 mm	100.0		0.002 mm	75.6
2.00 mm	100.0		0.001 mm	NT

0 10	Sand, %			011. 07	01 01	0 11 11 0/
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.1	0.1	1.0	98.8	NT

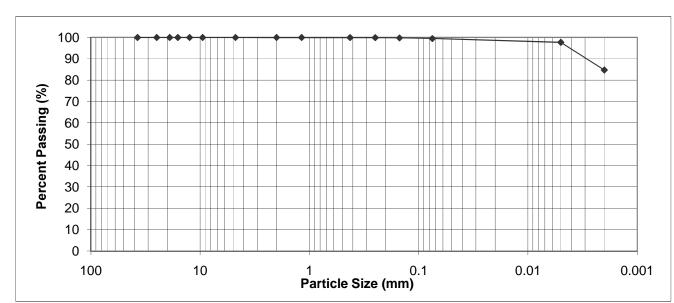
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: J.R. Cousin Consultants Ltd. DATE RECEIVED: August 23, 2011 SAMPLE ID: TH26 0.0-2.2 m TESTED BY: Nathan Boenders



PARTICLE	PERCENT	]	PARTICLE	PERCENT
SIZE	PASSING		SIZE	PASSING
37.50 mm	100.0		1.18 mm	100.0
25.00 mm	100.0		0.425 mm	99.9
19.00 mm	100.0		0.250 mm	99.9
16.00 mm	100.0		0.150 mm	99.8
12.50 mm	100.0		0.075 mm	99.5
9.50 mm	100.0		0.005 mm	97.7
4.75 mm	100.0		0.002 mm	84.7
2.00 mm	100.0		0.001 mm	NT

Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.1	0.425 10 0.075 111111	1.8	97.7	NIT
0.0	0.0	0.1	0.4	1.0	91.1	NI

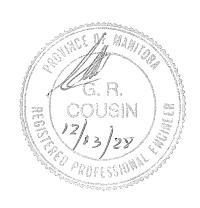
Note: Colloids content not tested

LGD of Mystery Lake Geotechnical and To – Additional Test Holes, JR Cousin Consul	iste Disposal Ground Scope Change #2

### LGD of MYSTERY LAKE

# Geotechnical Investigation for the Waste Disposal Ground Scope Change #2 – Additional Test Holes





Prepared by:

J. R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

### **ACKNOWLEDGMENTS**

To prepare this report various sources of information were investigated and researched. J. R. Cousin Consultants Ltd. (JRCC) wishes to thank the LGD of Mystery Lake who assisted with organization and onsite works.

### **REMARKS**

Conclusions reached in this report are based upon the generalization of data available to us at the time of forming our opinions. Information in this document may rely on previous studies, investigative work and data by others. JRCC cannot be responsible for actual site conditions proved to be at variance with any generalized data. This report was completed in accordance with generally accepted professional engineering principles and practice. Any use of this report by a third party is the responsibility of the third party, JRCC accepts no responsibility for third party decisions or actions based on the report. No other warranty or guarantee expressed, implied or statutory is made.

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## **APPENDIX**

Plan 1: Past and Current Test Hole Location Plan

Test Hole Logs

The National Testing Laboratories Test Results

### 1.0 INTRODUCTION

J. R. Cousin Consultants Ltd. (JRCC) conducted a geotechnical investigation for the Waste Disposal Ground (WDG) Expansion at the LGD of Mystery Lake. The existing WDG at the LGD of Mystery Lake is located on Part NW ¼ 18, S ½ and NW ¼ 19 in TWP 77-3 WPM and in Part SE ¼ 24-77-4 WPM, approximately 4 km south of the City of Thompson.

A total of 14 test holes were excavated at the WDG site. Test hole locations are shown on Plan 1 in the Appendix.

This report outlines the findings of the geotechnical investigation at the WDG site and evaluates the soils to determine their suitability for use as a landfill liner. The report also identifies potential difficulties (i.e. depth to bedrock, soil types and subsurface water elevations) associated with construction.

### 2.0 BACKGROUND

The geotechnical investigation was part of Scope Change #2 to determine the actual re-worked and recompacted hydraulic conductivity of the clay soils from the borrow pit and to determine the WDG east boundary of the minimum 1.0 m thick insitu clay liner. Test holes were also completed to determine the depth of waste in the area of the vertical cut-off wall to be constructed as part of the Phase I construction works.

The additional test holes were deemed necessary based on borderline laboratory test results received during the LGD of Mystery Lake Geotechnical and Topographic Investigation for the Waste Disposal Ground Proposed Phase II Works.

### 3.0 GEOTECHNICAL FIELD INVESTIGATION

The onsite investigation at the LGD of Mystery Lake was conducted on October 27, 2011. Smook Contractors Ltd. was employed to complete the test holes using a track mounted excavator under direct supervision by JRCC's field representative.

A total of 14 test holes were excavated during the investigation. Two test holes were excavated to determine the depth of waste near the vertical cut-off wall to be constructed as part of the Phase I Works (TH27 – TH28). Seven test holes were excavated along the east edge of the WDG to determine the edge of the insitu horizontal clay liner (TH29 – TH33 and TH 39 – TH40). Five test holes were excavated in the borrow pit area to determine the suitability of the clay soil for use as a re-worked and re-compacted clay liner (TH34 – TH38). Test holes were excavated to a depth ranging between 3.0 m and 5.8 m.

### 3.1 Test Holes

The subsurface soil profile within each test hole was logged, water conditions were noted and representative soil samples were taken as the soils varied along the profile. The samples were visually field-classified. Following excavation, the depth of standing water was measured and any caving of the holes was determined. Test holes were backfilled with the excavated soils. Test hole locations are shown on Plan 1 in the Appendix.

The following are the general soil profiles from the borrow pit, east of the WDG and of the existing waste. Details of each individual test hole can be found in the test hole logs in the Appendix.

#### 3.1.1 Soil Profile at the Borrow Pit

The general soil profile from the test holes taken in the borrow pit area (TH34 – TH38) consisted of a brown stiff high plastic clay and a brown stiff high plastic clay varved with a tan medium plastic silty clay between 1.3 and 4.8 m thick. The following layer was a grey high plastic clay observed to a maximum depth of 5.8 m.

The exception was TH38 which had medium plastic silty clay from 0 - 0.6 m followed by brown medium plastic clay varved with silty sandy grey low plastic clay.

### 3.1.2 Soil Profile East of the WDG

The soil profile from the test holes taken east of the WDG varied considerably. The soil profile from TH29 had existing waste from 0-1.3 m followed by high plastic clay varved with silty medium plastic clay. TH30 had existing waste from 0-3.6 m where the test hole was terminated. TH31 and TH32 had high plastic clay varved with silty low plastic clay from 0-5.3 and 0-4.8 m, respectively. TH33 had a medium plastic clay from 0-1.0 m and a silty, sandy low plastic clay from 1.0-3.6 m. TH 39 had organic topsoil from 0-1.9 m and silty, sandy low plastic clay from 1.9 to 4.9 m. TH40 had existing waste from 0-2.2 m and high plastic clay from 2.2-3.5 m and high plastic clay varved with silty low plastic clay from 3.5-4.4 m.

### 3.1.3 Soil Profile Through the Existing Waste

The soil profile through the existing waste consisted of 0 - 5.0 m of waste in TH27 and TH28. The excavator used for the test holes did not have the capacity to dig any deeper through the waste which was observed to an elevation of 211.07 in TH27 and 213.81 in TH28.

### 3.2 Groundwater

Short-term groundwater conditions were assessed in each test hole by observing standing water in the test holes prior to backfilling the holes. Water infiltration was observed in TH33 at a depth of 3.6 m with a cave-in observed at 1.0 m. Water infiltration was observed in TH29 at a depth of 1.3 m and leachate infiltration to the test hole was observed in TH40 at a depth of 2.2 m. No standing water or water infiltration was observed in the remainder of the test holes.

Groundwater in the test holes depends on high static groundwater conditions and on seasonal conditions, i.e. snowmelt and rainy seasons. Other assumptions relating to the groundwater elevation cannot be made at this time as water levels will normally fluctuate seasonally.

Contractors will be made aware of the geotechnical conditions encountered onsite, as some dewatering of the ground surface may be required during construction.

### 4.0 LABORATORY TESTING, ANALYSIS AND DISCUSSION

### 4.1 Laboratory Analysis

Four representative bagged soil samples from the borrow pit area and four representative bagged samples from the area east of the WDG were submitted to The National Testing Laboratories Ltd. on November 3, 2011, for analysis and a professional assessment. The analysis included the determination of the following:

- Moisture Content (ASTM D2216)
- Atterberg Limits (plastic limit, liquid limit, and plasticity index, ASTM D4318)
- Soil Classification (ASTM D2487)
- Particle Size Analysis (Hydrometer test, ASTM D422)
- Hydraulic Conductivity (ASTM D2435).

The soils were analyzed to determine their suitability as a re-worked and re-compacted or insitu liner for a WDG, which requires a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less.

The laboratory analysis of the soils from the borrow pit indicated that they are low to high plastic clay soils with a trace of silt. The overall Plasticity Index of the samples varied between 26 and 33 and the percentage of clay from 89.0% to 97.8%. Laboratory analysis of the soils from the area east of the WDG indicated they are low to high plastic clay with silt. The overall Plasticity Index of the samples varied between 19 and 40 and the percentage of clay from 88.1% to 95.2%.

Based on past experience, the laboratory has commented that homogeneous soils with a Plasticity Index greater than 25 and a clay content greater than 50% would typically be expected to have a

hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less. Plasticity Index analysis (i.e. Atterberg limits) of the soils indicated that all of the soil samples submitted were considered suitable for use as an insitu clay liner or when re-worked and re-compacted with the exception of TH31 from 1.5 - 5.3 m, which had a Plasticity Index of 19 and clay content of 88.1%.

The results indicate that the suitability of the soils for a clay liner is dependent upon the soils being homogeneous with no preferential flow paths. These preferential flow paths can be caused by lenses of unsuitable material, rocks or boulders or fissures in the soil.

One Shelby tube sample TH29 2.0-2.6 m was submitted to determine the insitu hydraulic conductivity, and one bagged sample TH36 0.4-3.1 m was submitted to determine the reworked and re-compacted hydraulic conductivity. The samples achieved hydraulic conductivities of  $2.1 \times 10^{-8}$  cm/sec and  $2.1 \times 10^{-8}$  cm/sec, respectively which are less than the required  $1 \times 10^{-7}$  cm/sec for a clay lined cell. This shows the layer of soil from TH29 from 1.3-4.7 m is suitable for use as an insitu clay liner and the layer of soil from TH36 from 0.4-3.1 is suitable as borrow material for use as a re-worked and re-compacted clay liner.

Details of The National Testing Laboratories test results and analysis, dated November 30, 2011 are in the Appendix.

### 5.0 WDG CELL LINER REQUIREMENTS

### **5.1** Current Guidelines

Manitoba Conservation guidelines require that a standard WDG cell clay liner be 1.0 metre in thickness and have a hydraulic conductivity (i.e. the potential rate of fluid movement through the soil) of  $1 \times 10^{-7}$  cm/sec or less. This low rate is to protect the underlying groundwater and surrounding lands from leachate seepage. Generally, the higher a soil's plasticity the more likely a soil can achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec.

### **5.2** Typical Clay Liner Construction Options

The insitu (undisturbed) soils can be used to construct the liner of a WDG cell if the soils can consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less in their insitu state.

If the insitu soils cannot be used, the liner can be constructed by excavating and re-compacting suitable high plastic clay soils to form the liner.

If the clay content of the soils is so low that even when excavated and re-compacted, the soils cannot consistently achieve a hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec, a liner constructed of high plastic clay from a borrow pit, or a synthetic geomembrane liner would be required.

### 5.3 Discussion

#### 5.3.1 East of the WDG

Based on the soils investigation and the laboratory analysis the soils under TH29 and TH40 are suitable for use as an insitu clay liner. The soils under TH30 – TH33 and TH39 were found to not be suitable for use as an insitu clay liner. A dike constructed between TH40 and TH29 will form the east boundary of the WDG with a vertical cut-off wall extended a minimum of 1.0 m into the suitable clay. The dike will be constructed during future work phases and is shown on Plan 1 in the Appendix.

#### 5.3.2 Borrow Pit Soils

Based on the soils investigation and laboratory analysis, the soils from the borrow pit around TH34 – TH37 are suitable for use as a re-worked and re-compacted clay liner, with the exception of TH38. All bagged samples submitted to the laboratory were deemed potential for use as a re-worked and re-compacted clay liner. This was confirmed by the bagged sample from TH36 0.4 - 3.1 which achieved a hydraulic conductivity of  $2.1 \times 10^{-8}$  cm/sec when re-worked and re-compacted. While the hydraulic conductivity was lower than the Manitoba Conservation requirement for a clay landfill liner of  $1 \times 10^{-7}$  cm/sec, it was only one order of magnitude lower which means proper compaction techniques will have to be followed to ensure the required hydraulic conductivity is met during construction of the WDG liner.

### 5.3.3 Vertical Cut-off Wall Through Existing Waste

The test holes taken through the existing waste for evaluation of the depth to clay found existing waste for at least 5.0 m from the surface. When the vertical cut-off wall is constructed through the waste during the Phase I works, it will have to be extended over 6.0 m from the surface of the waste as the cut-off wall will extend a minimum of 1.0 m into the existing clay liner.

### 6.0 RECOMMENDATIONS AND CLOSURE

### 6.1 Recommendations

It is recommended that a dike be constructed between TH40 and TH29 which will form the east boundary of the WDG with vertical cut-off walls in the dike extended a minimum of 1.0 m into the suitable clay.

It is recommended that the borrow pit soils be re-compacted and re-worked for use as liner material during Phase I construction works. Proper compaction techniques of the WDG liner will have to be followed to ensure the required hydraulic conductivity is met during construction because the laboratory re-worked and re-compacted hydraulic conductivity of TH36 from 0.4 –

3.1 m was only one order of magnitude lower than the Manitoba Conservation requirement for a clay landfill liner of  $1 \times 10^{-7}$  cm/sec.

When the vertical cut-off wall is constructed through the waste during the Phase I works, it will have to be extended over 6.0 m from the surface of the waste.

### 6.2 Closure

The conclusions and recommendations in this report are based on the results of the site investigation and laboratory analysis. In addition, soil and groundwater conditions between test hole locations were generalized to provide an overall assessment of the geotechnical site conditions. If conditions that appear different from those encountered at the test hole locations as described in this report, or if the assumptions stated herein are not in agreement with the design, JRCC should be informed in order that the recommendations can be reviewed and adjusted as required.

The site investigation was conducted for the purpose of identifying geotechnical conditions at the borrow pit site and the expansion area east of the WDG. Although no environmental issues were identified during the site investigation, it does not necessarily follow that such issues do not exist. If the client or any other parties have any environmental concerns regarding the proposed site and works, an appropriate environmental assessment must be conducted.

It is not uncommon for soil conditions to be highly variable across a site. Previous construction activities and placement of fill at a site can augment the variability of soil conditions, especially surficial soil conditions. A contingency must be included in any construction budget to allow for potential variations in soil conditions, which may result in modification of the design and construction procedures.

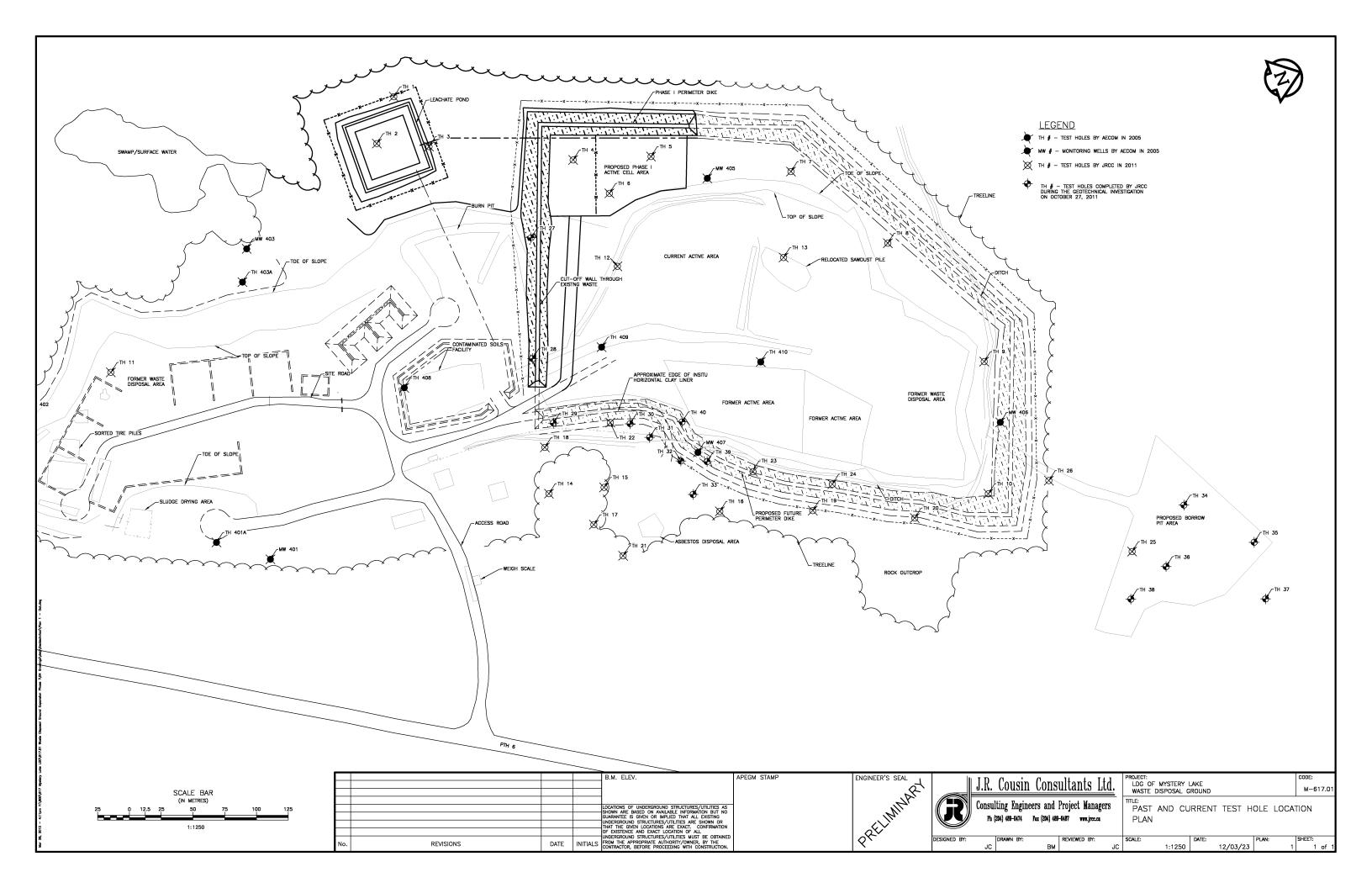
# **APPENDIX**

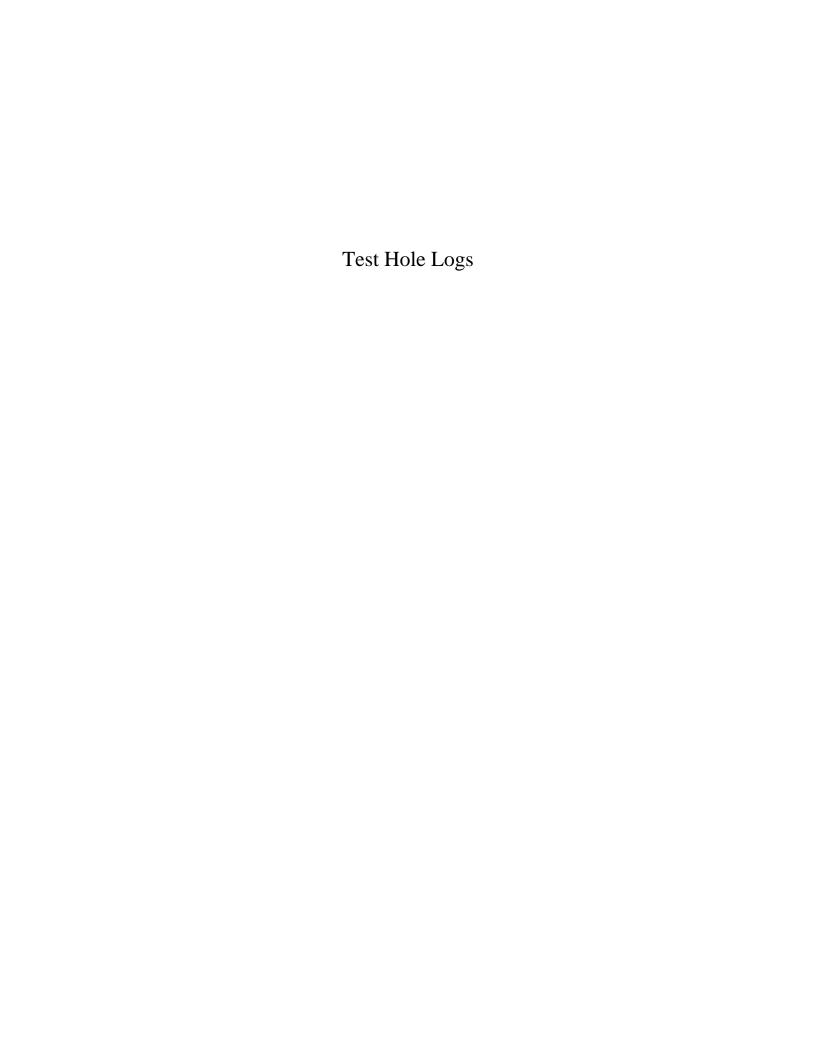
Plan 1: Test Hole Location Plan

Test Hole Logs

The National Testing Laboratories Ltd. Test Results

Plan 1: Test Hole Location Plan





### SYMBOL INDEX

STWIDOL INDEA
GW. : Well graded gravels and gravel sand mixtures, little or no fines
GP. : Poorly graded gravels, gravel - sand mixtures, little or no fines
GM. : Silty gravels, gravel-sand-silt mixtures
GC. : Clayey gravels, gravel-sand-clay mixtures
SW.: Well graded sands, gravelly sands, little or no fines
SP.: Poorly graded sands, or gravelly sands, little or no fines
SM. : Silty sands, sand-silt mixtures
SC. : Clayey sands, sand-clay mixtures
ML. : Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity
CL. : Inorganic clays of low plasticity, gravelly clays, sandy or silty clays, lean clays
OL. : Organic silts and organic silty clays of low plasticity
CI. : Inorganic clays of medium or intermediate plasticity
MH. : Inorganic silts, fine sandy or silty soils
CH.: Inorganic clays of high plasticity, fat clays
OH. : Organic clays of medium to high plasticity, organic silts
Pt. : Peat, humus, swamp soils with high organic contents

TOPSOIL

The soil logs are based upon objective data available to us at the time of forming our opinions. The soil logs indicate site specific soil characteristics and must not be generalized over larger areas due to the limited number of test holes as compared to that of an unlimited number of test holes. Every effort is made to evaluate the information by methods generally recognized. The soil logs represent our opinions. J. R. Cousin Consultants Ltd. cannot be responsible for actual site conditions proved to be materially at variance from our analysis or from the data generalization over untested areas.

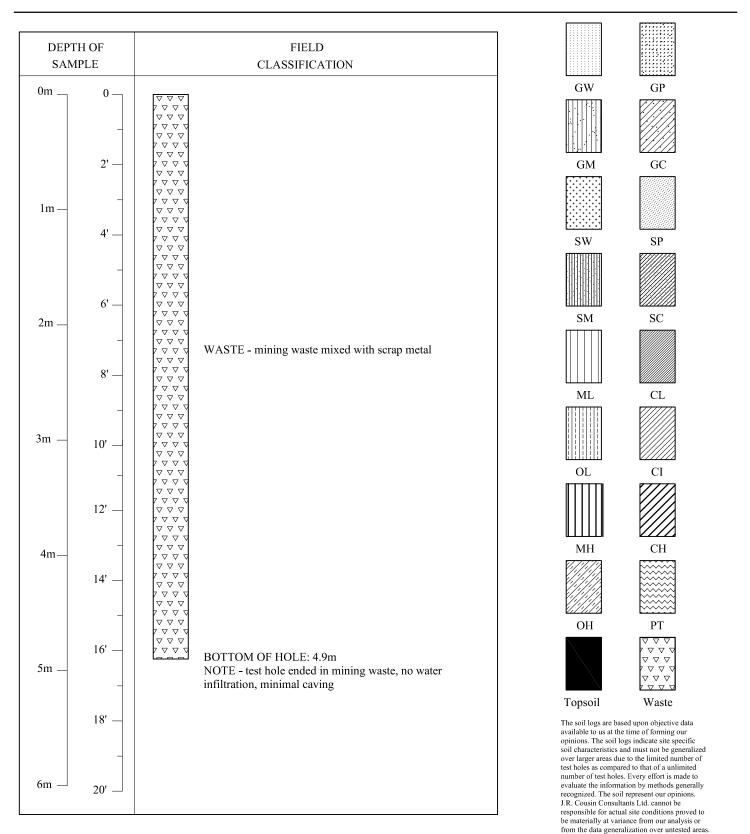
LOCATION: 6171218.24 N

567857.87 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 215.966 m

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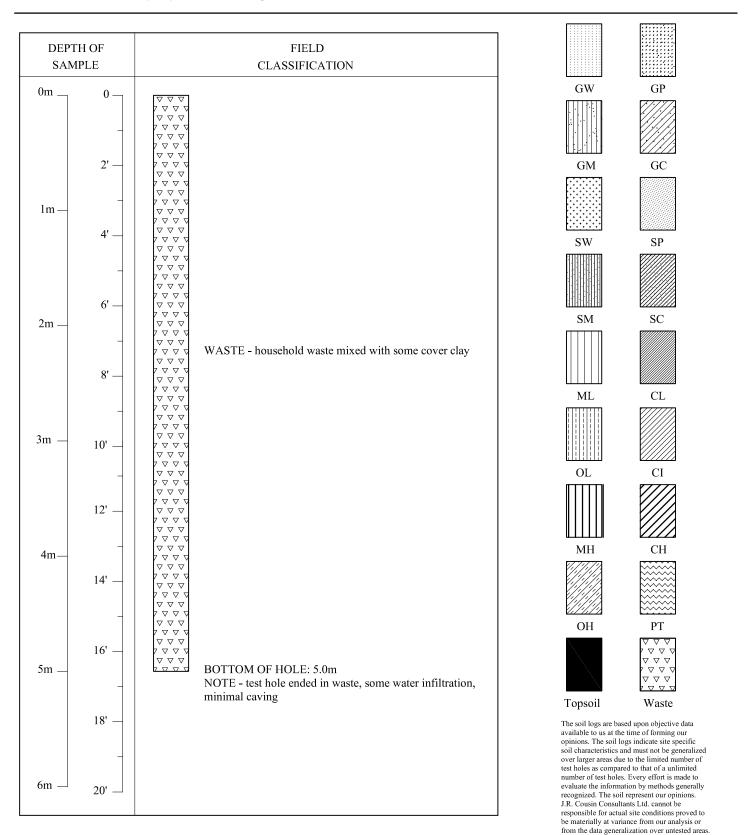
LOCATION: 6171187.37 N

567947.78 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 218.811 m

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LOCATION: 6171185.85 N

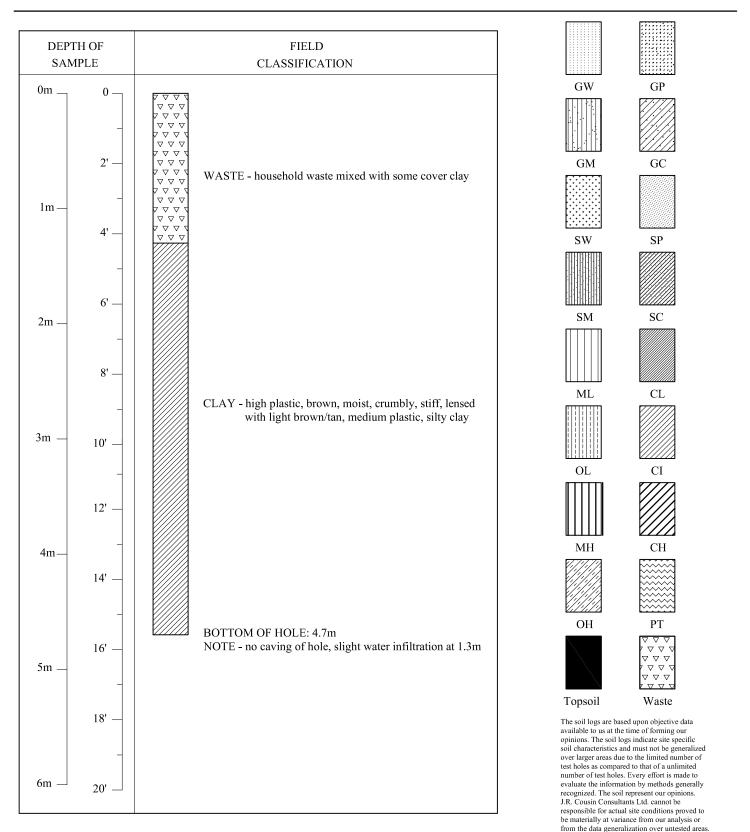
568001.06 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : October 27, 2011

ELEVATION: 219.898 m

TEST HOLE # 29



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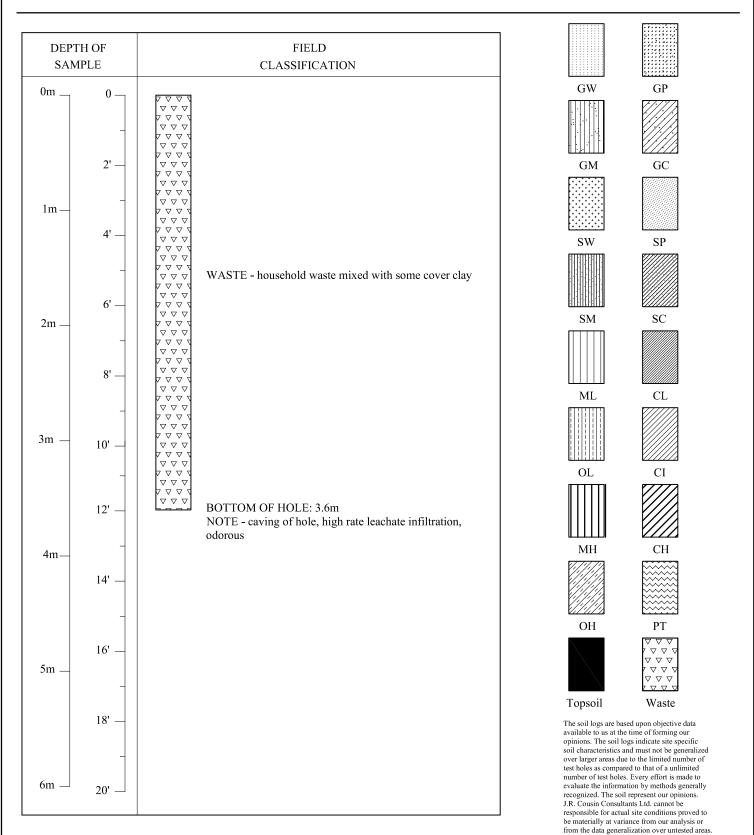
LOCATION: 6171242.53 N

568021.78 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : October 27, 2011 ELEVATION : 218.886 m

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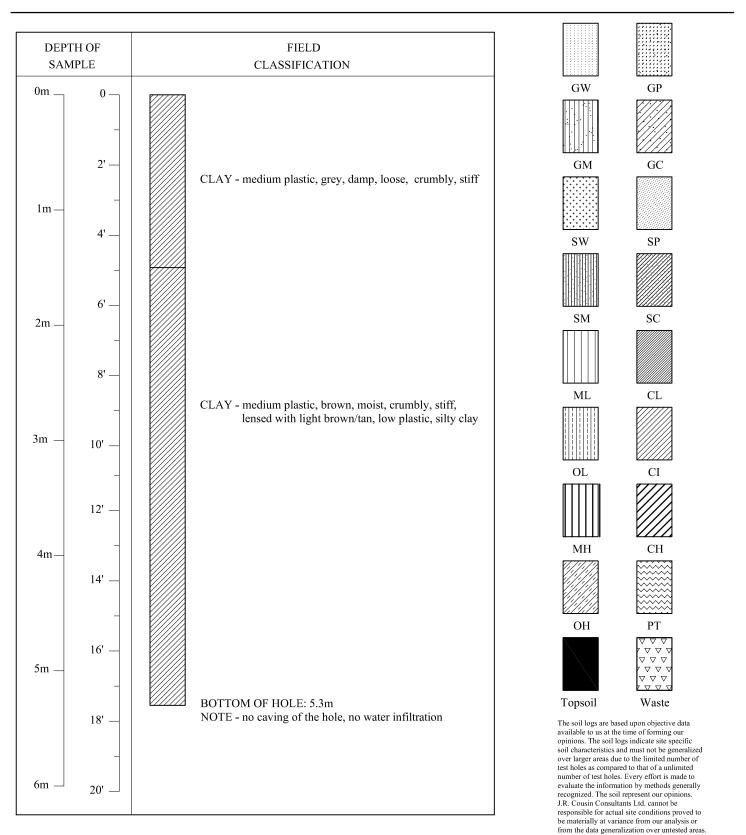
LOCATION: 6171253.45 N

568037.11 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 219.405 m

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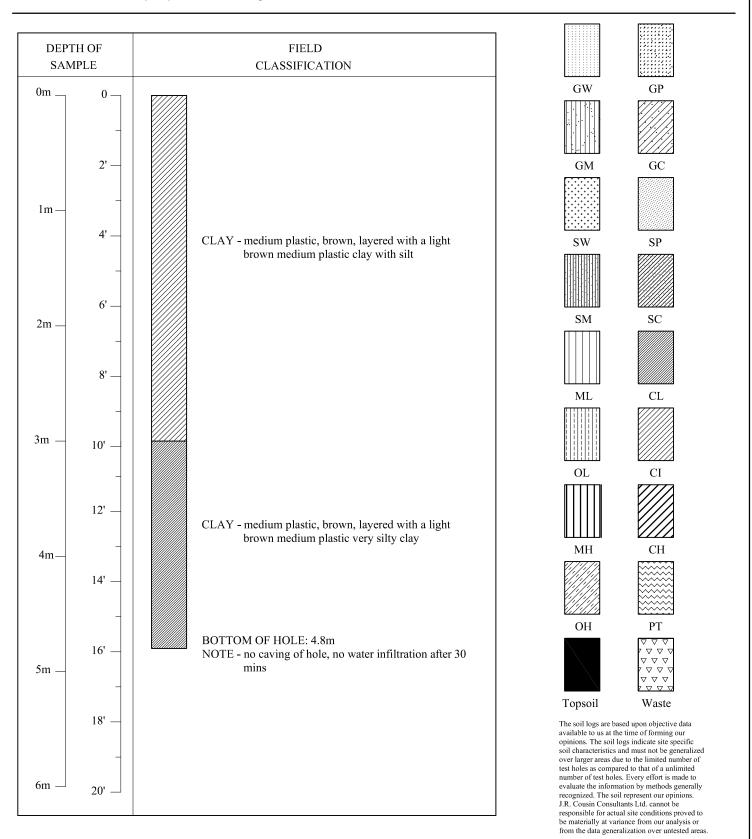
LOCATION: 6171270.34 N

568062.75 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : October 27, 2011 ELEVATION : 219.961 m

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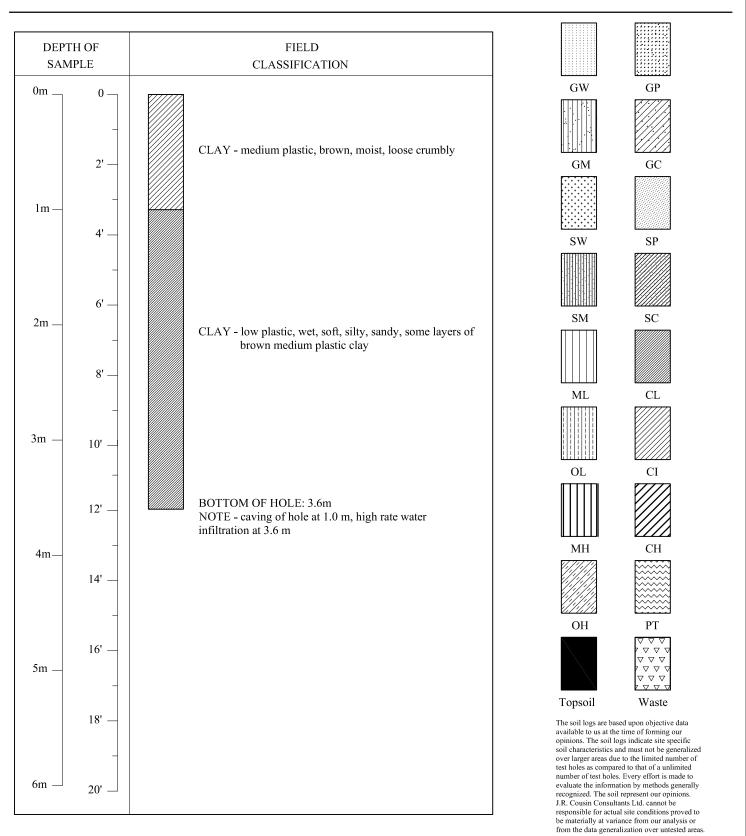
LOCATION: 6171270.60 N

568090.80 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : October 27, 2011 ELEVATION : 219.051 m

TEST HOLE # 33



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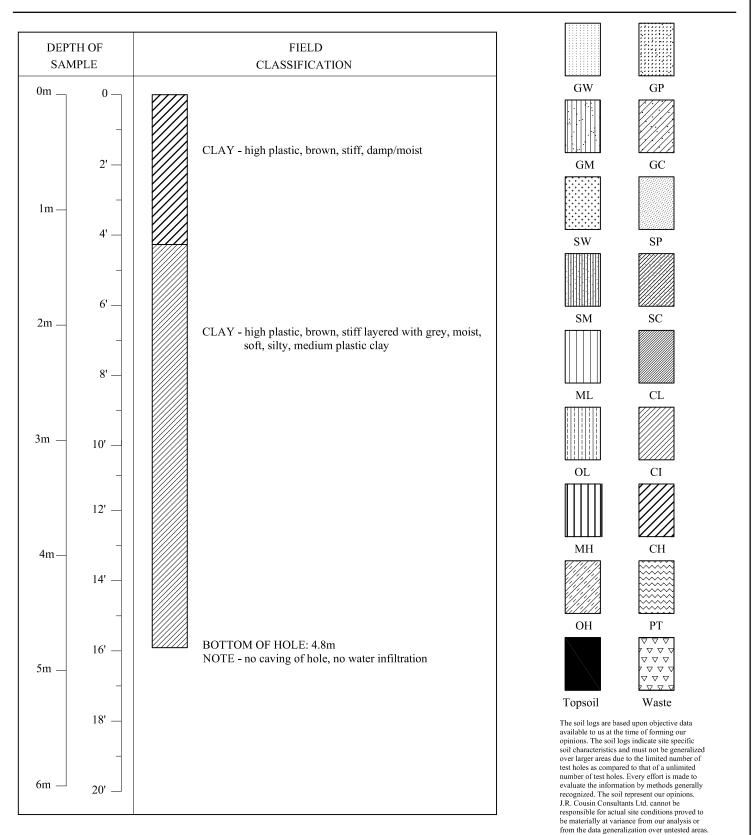
LOCATION: 6171631.52 N

56228.32 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 213.634 m

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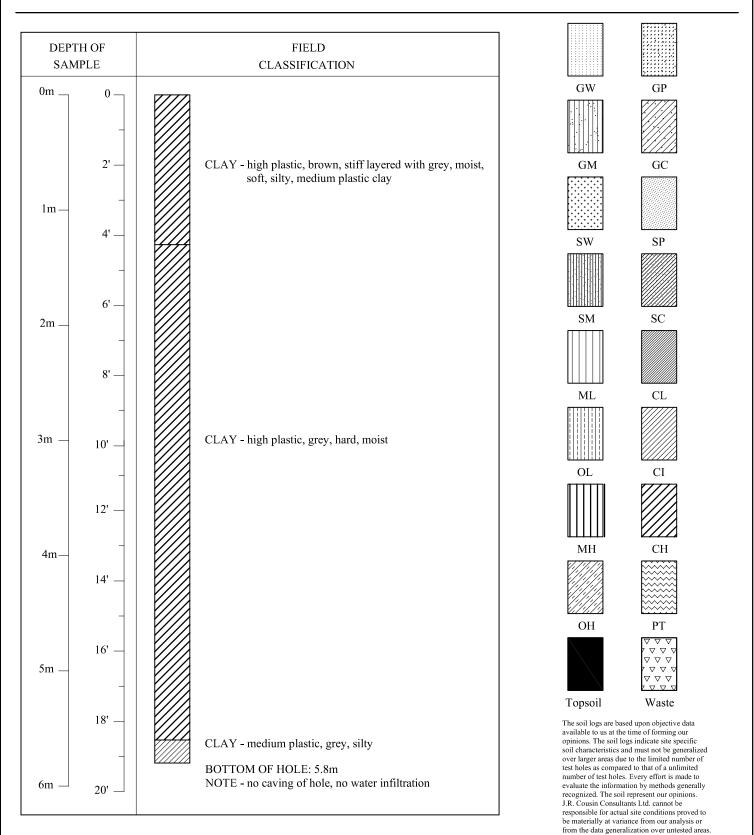
LOCATION: 6171673.76 N

568274.40 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE : October 27, 2011 ELEVATION : 213.321 m

TEST HOLE # 35



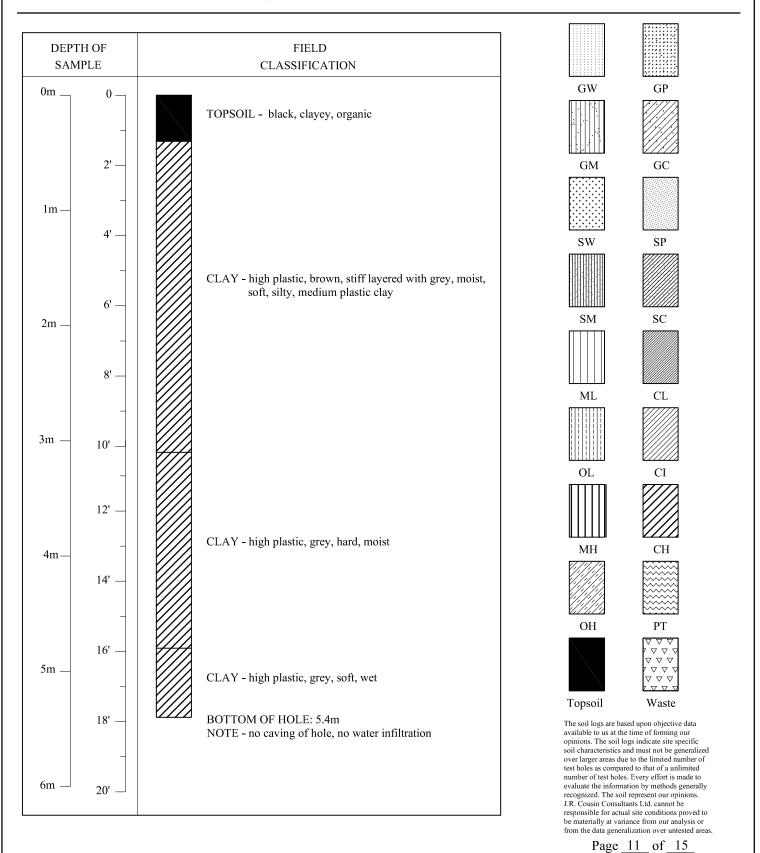
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LOCATION: 6171602.07 N

568269.15 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 215.197 m



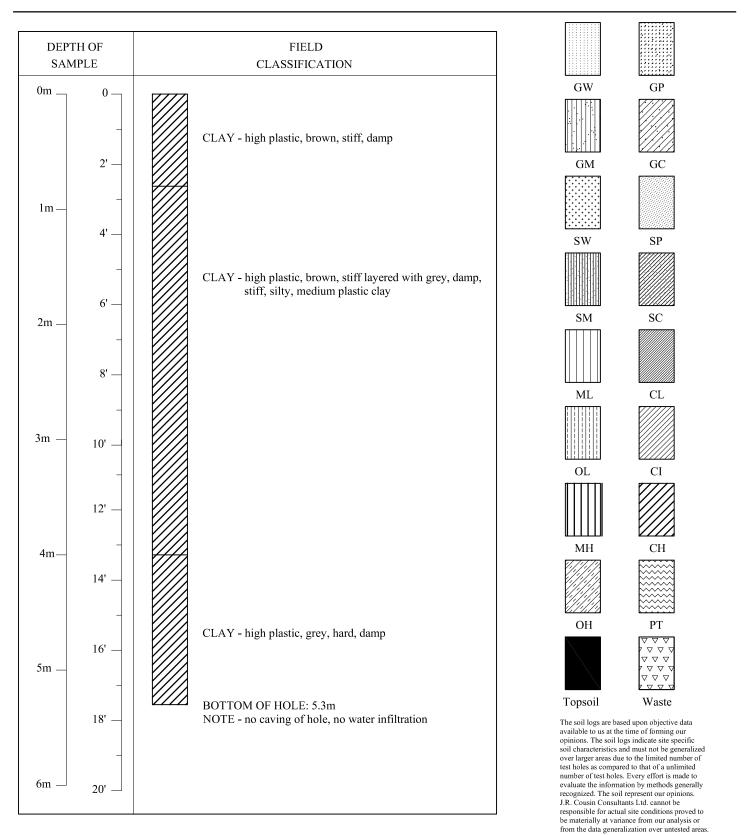
LOCATION: 6171667.30 N

568319.01 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 217.924 m

TEST HOLE # 37



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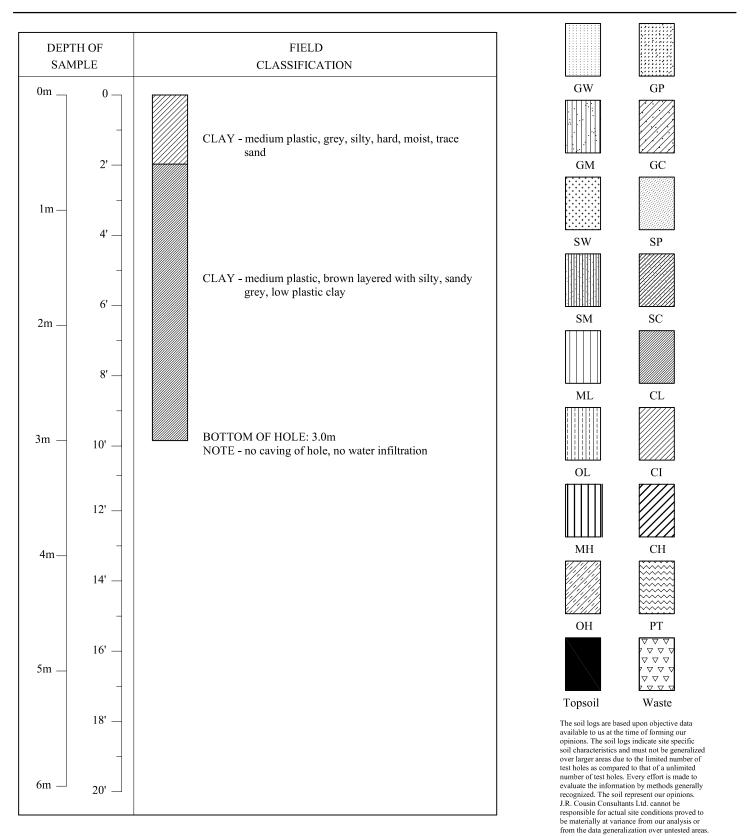
LOCATION: 6171567.38 N

568283.97 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 216.174 m

TEST HOLE # 38



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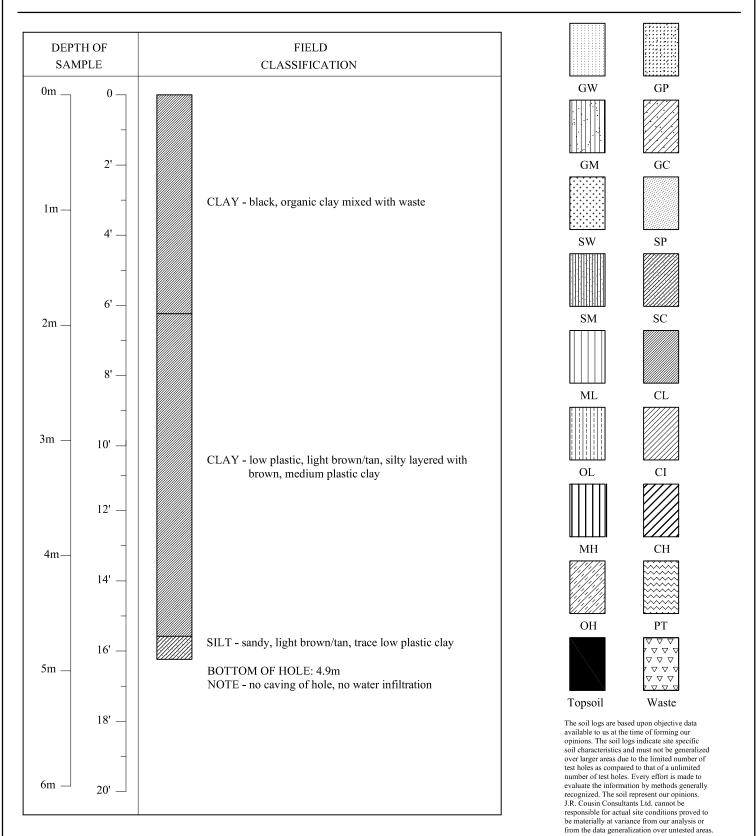
LOCATION: 6171289.60 N

568070.16 E

PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 218.280 m

TEST HOLE #39



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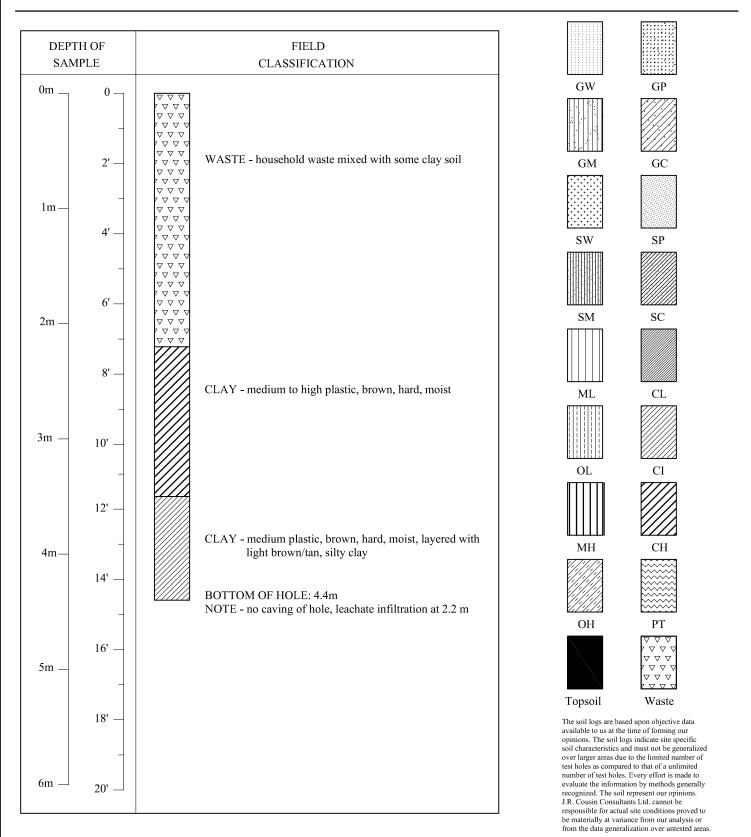
LOCATION: 6171281.60 N

568034.20 E

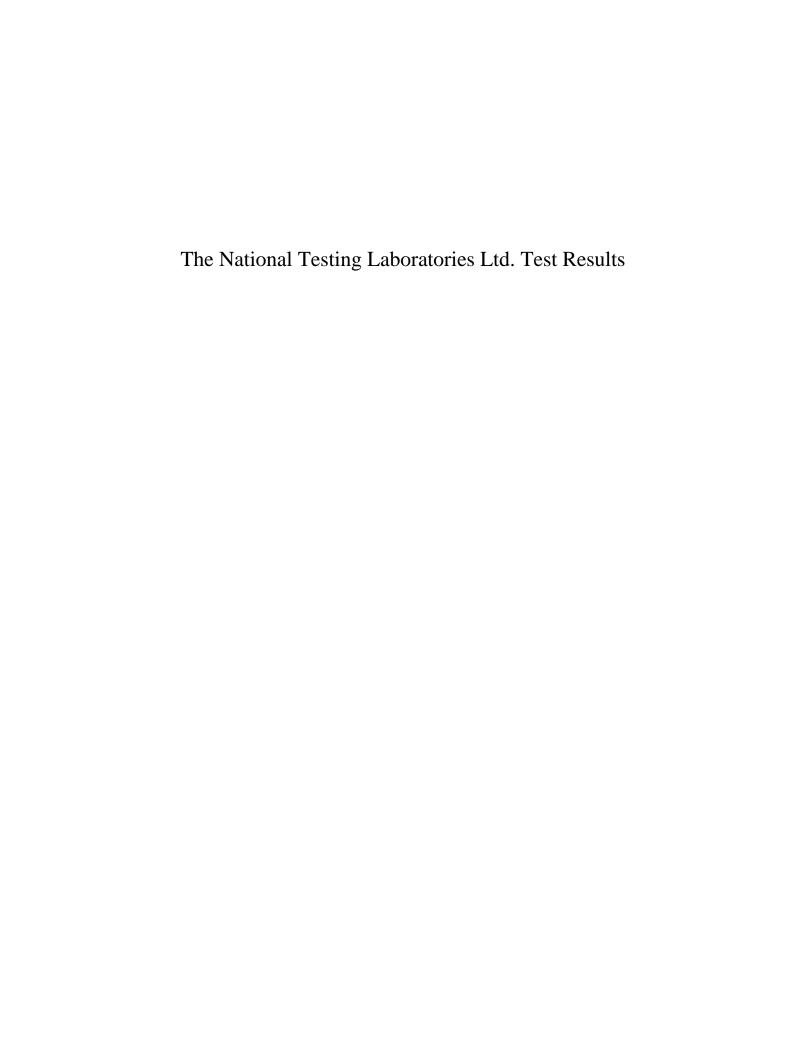
PROJECT: LGD of Mystery Lake - Waste Disposal Ground

DATE: October 27, 2011 ELEVATION: 218.157 m

TEST HOLE # 40



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199 Henlow Bay Winnipeg, MB R3Y 1G4 Phone (204) 488-6999 Fax (204) 488-6947 Email info@nationaltestlabs.com www.nationaltestlabs.com

J.R. Cousin Consultants Ltd. 91 A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 November 30, 2011

Project: Mystery Lake Waste Disposal Facility

Soil samples were submitted to our laboratory on November 3, 2011. The following tests were conducted on selected soil samples:

Attention: Brett McCormac

- water content (ASTM D2216)
- particle size analysis (ASTM D422)
- liquid limit, plastic limit, and plasticity index (ASTM D4318)
- hydraulic conductivity (ASTM D5084)
- soil classification (ASTM D2487)
- visual classification

The test results for the soil samples are summarized in the following tables and in the attached particle size analysis and hydraulic conductivity reports.

An assessment of the bagged soil samples was conducted to determine whether the soil represented by the bagged samples could be used in-situ as a landfill liner and would obtain a hydraulic conductivity of less than 1.0 x 10⁻⁷ cm/sec without being reworked, and when re-moulded and re-compacted.

Based upon previous testing conducted in our laboratory, homogeneous soil samples with a plasticity index greater than 25 and a clay content greater than 50% will typically have a hydraulic conductivity of 1.0 x 10⁻⁷ cm/sec or less. Sample TH31 1.5 – 5.3 m had a plasticity index of 19, which does not fall within this range. Hydraulic conductivity testing of this material is recommended to determine its suitability for use as a lagoon liner. The remaining bagged samples were considered suitable for use as a lagoon liner. Our comments regarding the potential use of the material as a lagoon liner are based upon the soil being homogeneous with no preferential flow paths and being properly placed and compacted to maximum density near its optimum moisture content. It should be noted that estimating the hydraulic conductivity of a soil based upon classification test results (plasticity index and particle size analysis) alone might be misleading if the soil contains layers of sand, silt, or organic material.

The hydraulic conductivity results for the 2 tested samples are less than the specified maximum hydraulic conductivity value of  $1.0 \times 10^{-7}$  cm/s for lagoon liners. It should be noted that sample TH29 2.0 - 2.6 m was a Shelby tube sample, and sample TH36 0.4 - 3.1m was a bagged sample which was remoulded in our laboratory prior to testing for hydraulic conductivity.

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Aron Piamsalee, B.Sc., EIT Geotechnical Project Manager

Aan Pinneslee



### TABLE 1 SUMMARY OF WATER CONTENT, PARTICLE SIZE, ATTERBERG LIMITS, SOIL CLASSIFICATION TEST DATA MYSTERY LAKE WASTE DISPOSAL FACILITY

	Doub	Wate		Gravel (%)	Sand (%)		Silt (%) Clay (%)	^{⁄o)} Liquid			Soil	Potential Use as a	Potential Use as a Landfill		
	Depth (m)		Content (%)	75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	<0.075 to 0.005 mm	<0.005 mm	Limit	Limit	Index	Soil Classification ASTM D2487	without being Reworked	Liner when re-moulded and re-compacted
TH29		brown, firm, moist, high plasticity clay, trace silt	33.4	0.1	0.0	0.1	0.4	4.2	95.2	64	24	40	CH(Fat Clay)	Yes	Yes
TH31	1.5 - 5.3	grey, firm, moist, low plasticity clay, some silt	29.4	0.0	0.1	0.0	0.1	11.7	88.1	38	19	19	CL(Lean Clay)		esting mended
TH34		brown, stiff, moist, high plasticity clay, trace silt	30.6	0.0	0.0	0.1	0.2	5.4	94.3	55	22	33	CH(Fat Clay)	Yes	Yes
TH34		grey, stiff, moist, low plasticity clay, some silt	33.2	0.0	0.0	0.0	0.2	10.8	89.0	46	19	27	CL(Lean Clay)	Yes	Yes
TH35		brown, stiff, moist, low plasticity clay, trace silt	38.0	0.0	0.0	0.1	0.1	8.3	91.5	45	19	26	CL(Lean Clay)	Yes	Yes
TH36	3.1 - 4.8	grey, firm, moist, high plasticity clay, trace silt	29.9	0.0	0.0	0.1	0.0	2.1	97.8	51	20	31	CH(Fat Clay)	Yes	Yes
TH40	2.2 - 3.5	brown, firm, moist, high plasticity clay, trace silt	35.9	0.5	0.1	0.0	0.4	5.3	93.7	65	25	40	CH(Fat Clay)	Yes	Yes
TH40		brown, firm, moist, low plasticity clay, some silt	34.3	0.0	0.0	0.1	0.5	10.7	88.7	49	21	28	CL(Lean Clay)	Yes	Yes

#### Notes:

- 1.A high speed stirring device was used for 1 minute to disperse the test samples for particle size analysis.

  2.Atterberg limits conducted in accordance with ASTM D4318 Method B (one-point liquid limit).
- 3. The soil samples were air-dried during sample preparation for Atterberg limits and particle size analysis.



### TABLE 2 HYDRAULIC CONDUCTIVITY SUMMARY MYSTERY LAKE WASTE DISPOSAL FACILITY

Testhole	Depth (m)	Hydraulic Conductivity, "k ₂₀ "
TH29	2.0 – 2.6	2.1 x 10 ⁻⁸ cm/s
TH36	0.4 - 3.1	2.1 x 10 ⁻⁸ cm/s

Note: Sample TH36 0.4 - 3.1 m was lab-remoulded prior to testing.

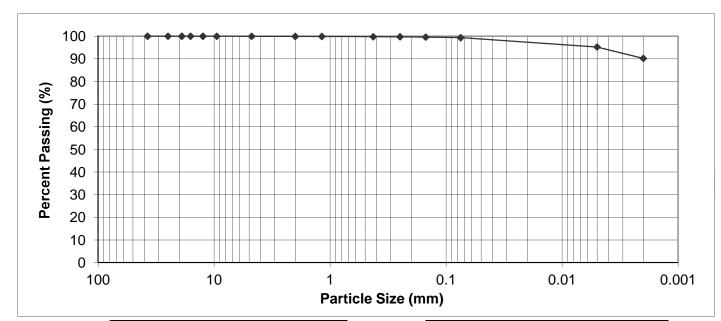


PROJECT: Mystery Lake Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH29 at 1.3 - 4.7 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	99.9
25.00 mm	100.0	0.425 mm	99.8
19.00 mm	100.0	0.250 mm	99.7
16.00 mm	100.0	0.150 mm	99.6
12.50 mm	100.0	0.075 mm	99.4
9.50 mm	100.0	0.005 mm	95.2
4.75 mm	99.9	0.002 mm	90.2
2.00 mm	99.9	0.001 mm	NT

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.1	0.0	0.1	0.4	4.2	95.2	NT

Note: Colloids content not tested

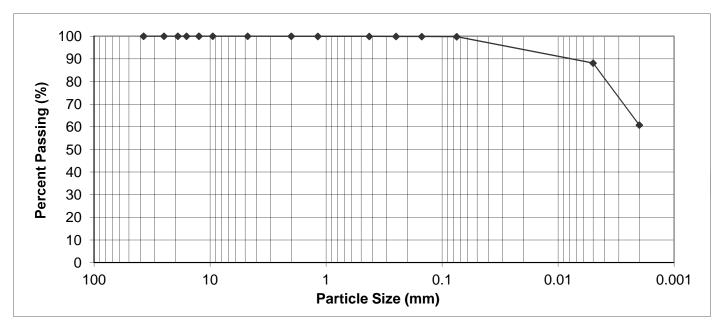


PROJECT: Mystery Lake Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH31 at 1.5 - 5.3 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	99.9
25.00 mm	100.0	0.425 mm	99.9
19.00 mm	100.0	0.250 mm	99.9
16.00 mm	100.0	0.150 mm	99.8
12.50 mm	100.0	0.075 mm	99.8
9.50 mm	100.0	0.005 mm	88.1
4.75 mm	100.0	0.002 mm	60.8
2.00 mm	99.9	0.001 mm	NT

		Sand, %					
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm	
0.0	0.1	0.0	0.1	11.7	88.1	NT	

Note: Colloids content not tested

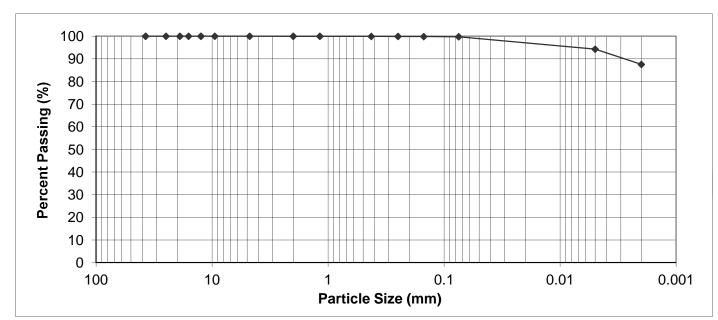


PROJECT: Mystery Lake Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH34 at 0 - 1.3 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	99.9
25.00 mm	100.0	0.425 mm	99.9
19.00 mm	100.0	0.250 mm	99.9
16.00 mm	100.0	0.150 mm	99.8
12.50 mm	100.0	0.075 mm	99.7
9.50 mm	100.0	0.005 mm	94.3
4.75 mm	100.0	0.002 mm	87.5
2.00 mm	100.0	0.001 mm	NT

		Sand, %		0111	Clay, % <0.005 mm	Colloids, % < 0.001 mm
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm		
0.0	0.0	0.1	0.2	5.4	94.3	NT

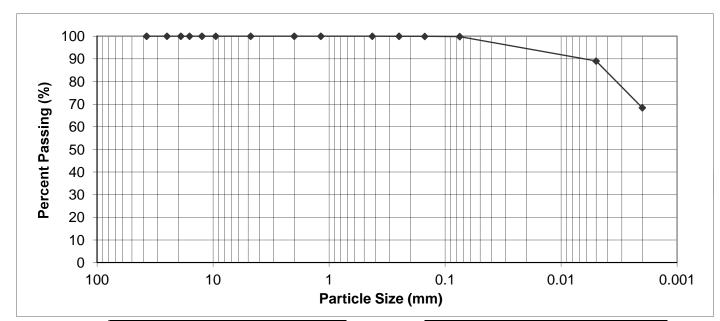
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH34 at 1.3 - 4.8 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	100.0
19.00 mm	100.0	0.250 mm	100.0
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.8
9.50 mm	100.0	0.005 mm	89.0
4.75 mm	100.0	0.002 mm	68.4
2.00 mm	100.0	0.001 mm	NT

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.0	0.2	10.8	89.0	NT

Note: Colloids content not tested

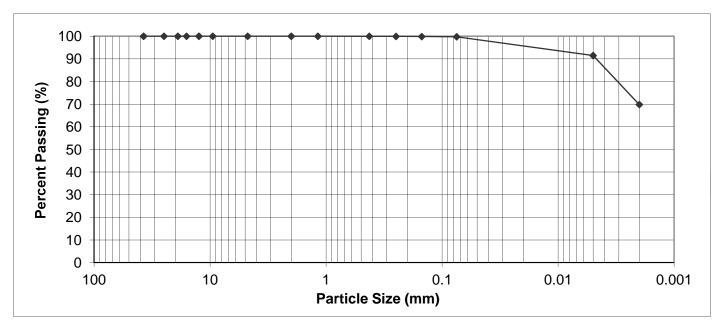


J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

PROJECT: Mystery Lake Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH35 at 1.3 - 5.6 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	PERCENT
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	99.9
19.00 mm	100.0	0.250 mm	99.9
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.8
9.50 mm	100.0	0.005 mm	91.5
4.75 mm	100.0	0.002 mm	69.8
2.00 mm	100.0	0.001 mm	NT

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.0	0.0	0.1	0.1	8.3	91.5	NT

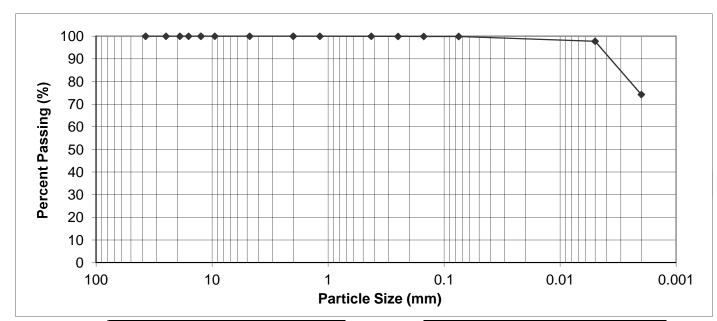
Note: Colloids content not tested



J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Disposal Facility

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH36 at 3.1 - 4.8m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	100.0
25.00 mm	100.0	0.425 mm	99.9
19.00 mm	100.0	0.250 mm	99.9
16.00 mm	100.0	0.150 mm	99.9
12.50 mm	100.0	0.075 mm	99.9
9.50 mm	100.0	0.005 mm	97.8
4.75 mm	100.0	0.002 mm	74.3
2.00 mm	100.0	0.001 mm	NT

	Gravel, % 75 to 4.75 mm		Sand, %				
		Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
	0.0	0.0	0.1	0.0	2.1	97.8	NT

Note: Colloids content not tested

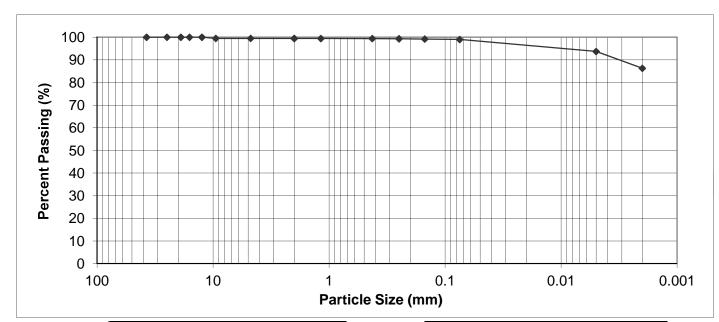


PROJECT: Mystery Lake Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

Attention: Brett McCormac PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011 SAMPLE ID: TH40 at 2.2 - 3.5m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	99.4
25.00 mm	100.0	0.425 mm	99.4
19.00 mm	100.0	0.250 mm	99.3
16.00 mm	100.0	0.150 mm	99.2
12.50 mm	100.0	0.075 mm	99.0
9.50 mm	99.5	0.005 mm	93.7
4.75 mm	99.5	0.002 mm	86.3
2.00 mm	99.4	0.001 mm	NT

		Sand, %				
Gravel, % 75 to 4.75 mm	Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
0.5	0.1	0.0	0.4	5.3	93.7	NT

Note: Colloids content not tested



PROJECT: Mystery Lake Disposal Facility

J.R. Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

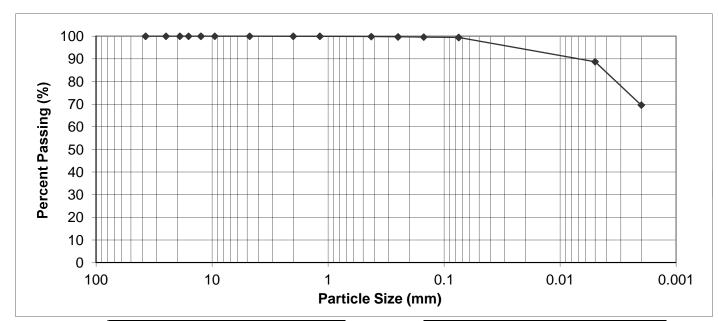
**Brett McCormac** 

Attention:

PROJECT NO.: JRC-1102

SAMPLED BY: Client DATE RECEIVED: November 3, 2011

SAMPLE ID: TH40 at 3.5 - 4.4 m TESTED BY: Larry Presado



PARTICLE	PERCENT	PARTICLE	
SIZE	PASSING	SIZE	PASSING
37.50 mm	100.0	1.18 mm	99.9
25.00 mm	100.0	0.425 mm	99.9
19.00 mm	100.0	0.250 mm	99.7
16.00 mm	100.0	0.150 mm	99.6
12.50 mm	100.0	0.075 mm	99.4
9.50 mm	100.0	0.005 mm	88.7
4.75 mm	100.0	0.002 mm	69.6
2.00 mm	100.0	0.001 mm	NT

	Gravel, % 75 to 4.75 mm		Sand, %				
		Coarse <4.75 to 2.0 mm	Medium <2.0 to 0.425 mm	Fine <0.425 to 0.075 mm	Silt, % <0.075 to 0.005 mm	Clay, % <0.005 mm	Colloids, % < 0.001 mm
	0.0	0.0	0.1	0.5	10.7	88.7	NT

Note: Colloids content not tested



J.R.Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4 PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac

SAMPLE I.D.: TH29 at 2 - 2.6 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

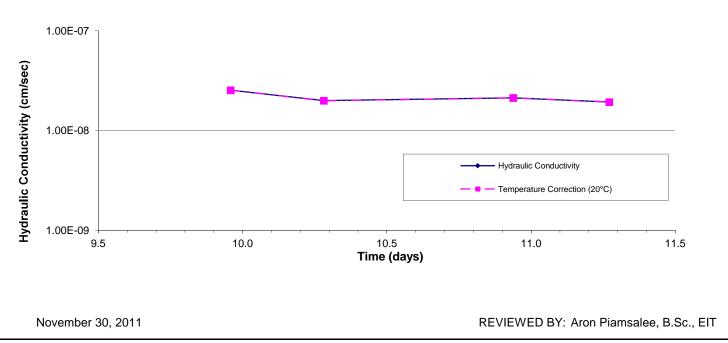
DATE TESTED: November 4 to Nov 15

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 18.3

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 2.1E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 2.1E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	81.1	72.4	638.3	1.475	29.6	95.1
Final Reading	81.4	72.6	646.8	1.449	32.5	100.7





REVIEWED BY: Aron Piamsalee, B.Sc., EIT

J.R.Cousin Consultants Ltd. 91A Scurfield Blvd. Winnipeg, Manitoba R3Y 1G4

November 30, 2011

PROJECT: Mystery Lake Waste Disposal Facility

Attention: Brett McCormac

SAMPLE I.D.: TH36 at 0.4 - 3.1 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

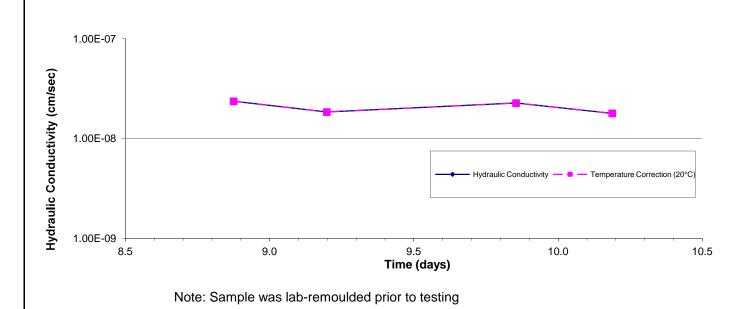
DATE TESTED: November 5 to November 16

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 19.8

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 2.1E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 2.1E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	74.6	70.5	567.9	1.489	31.1	102.0
Final Reading	74.6	70.6	570.9	1.491	31.0	102.0



Phase I Construction Works — Hydraulic Conductivity	Test Results, NTL, September 14, 2012



199 Henlow Bay Winnipeg, MB R3Y 1G4 Phone (204) 488-6999 Fax (204) 488-6947 Email info@nationaltestlabs.com www.nationaltestlabs.com

Smook Contractors. 101 Hayes Road Thompson, Manitoba R8N 1M3 September 14, 2012

Project: LGD of Mystery Lake

Attention: Peter Paulic Phase I

Soil samples were submitted to our laboratory on September 4, 2012. The samples were tested in accordance with ASTM D5084, Measurement of Hydraulic Conductivity of Saturated Porous Materials using a Flexible Wall Permeameter. The test results are summarized in the following table and the attached hydraulic conductivity reports.

Sample ID	Sample Depth (m)	Hydraulic Conductivity, "k ₂₀ "
TH1	1.5-2.1	1.6 x 10 ⁻⁸ cm/s
TH2	0.2-0.8	9.7 x 10 ⁻⁹ cm/s
TH4	4.5-5.1	3.1 x 10 ⁻⁸ cm/s

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Farouk Fourar-Laidi, E.I.T. Geotechnical Engineering



Smook Contractors 101 Hayes Road Thompson, MB R8N 1M3 PROJECT: LGD of Mystery Lake, Phase I

Attention: Peter Paulic

SAMPLE I.D.: TH1 at 1.5-2.1 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

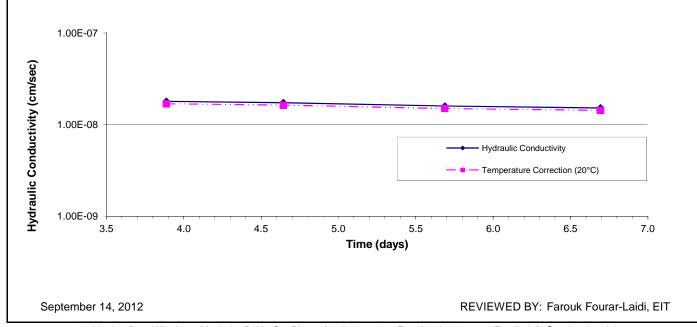
DATE TESTED: September 4th to 11th, 2012

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 19.0

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.7E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 1.6E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	77.4	72.5	632.5	1.530	29.4	103.2
Final Reading	78.1	72.8	640.2	1.510	30.5	104.1





Smook Contractors 101 Hayes Road Thompson, MB R8N 1M3 PROJECT: LGD of Mystery Lake, Phase I

Attention: Peter Paulic

SAMPLE I.D.: TH2 at 0.2-0.8 m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

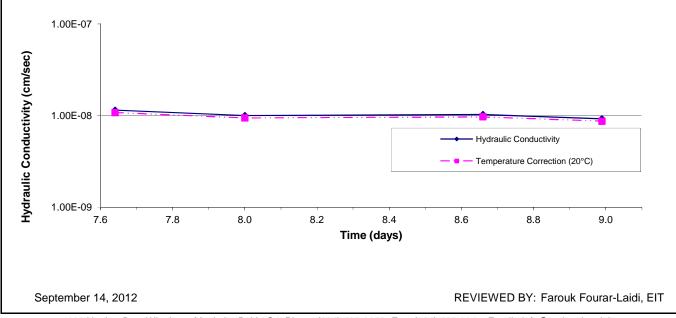
DATE TESTED: September 4th to 13 th, 2012

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 20.1

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.0E-08 HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 9.7E-09

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	74.2	72.6	580.6	1.440	31.2	94.3
Final Reading	73.4	72.6	586.1	1.452	32.9	101.3





Smook Contractors 101 Hayes Road Thompson, MB R8N 1M3 PROJECT: LGD of Mystery Lake, Phase I

Attention: Peter Paulic

SAMPLE I.D.: TH4 at 4.5-5.1m

SOIL TYPE: Brown, stiff, moist, high plasticity clay

trace silt

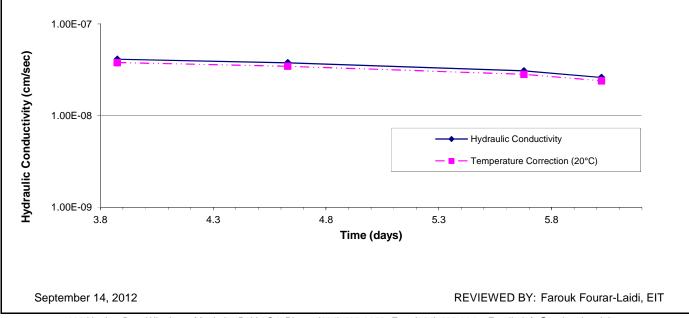
DATE TESTED: September 4th to 10th, 2012

CONFINING PRESSURE (kPa): 137.9
EFFECTIVE SATURATION STRESS (kPa): 34.5
HYDRAULIC GRADIENT: 20.2

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 3.4E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 3.1E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	73.3	72.5	601.9	1.567	27.2	101.0
Final Reading	73.4	72.6	607.8	1.565	27.8	102.9



Phase II Construction Works – Hydraulic Conductivity Test Results, NTL, October 29, 2013



199 Henlow Bay Winnipeg, MB R3Y 1G4 Phone (204) 488-6999 Fax (204) 488-6947 Email info@nationaltestlabs.com www.nationaltestlabs.com



Smook Contractors 101 Hayes Road Thompson, MB R8N 1M3

October 29, 2013

Project: LGD of Mystery Lake

Landfill

Seven Shelby tube samples were submitted to our laboratory on October 4, 2013. The samples were extruded from the Shelby tubes on October 17, 2013 in the presence of Manitoba Conservation Officer and a representative from J.R. Cousin Consultants Ltd. Selected soil samples from the Shelby tubes were tested in accordance with ASTM D5084, Measurement of Hydraulic Conductivity of Saturated Porous Materials using a Flexible Wall Permeameter.

Attention: Peter Paulic

The test results for the soil samples tested are summarized in the following table and in the attached Hydraulic Conductivity Reports.

Testhole	Depth (ft)	Hydraulic Conductivity, "k ₂₀ "
TH5	1-3	3.6 x 10 ⁻⁸ cm/s
TH7	1-3	9.5 x 10 ⁻⁹ cm/s
TH8	1-3	1.9 x 10 ⁻⁸ cm/s

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Farouk Fourar-Laidi, B.Sc., EIT

Geotechnical Engineering



#### HYDRAULIC CONDUCTIVITY **ASTM D5084**

**Smook Contractors** 101 Hayes Road Thompson, MB **R8N 1M3** 

PROJECT: LGD of Mystery Lake Landfill

Attention: Peter Paulic PROJECT NO.: SMO-1304

SAMPLE I.D.: TH5 at 1'-3'

SOIL DESCRIPTION: Brown, stiff, moist, high plasticity silty clay

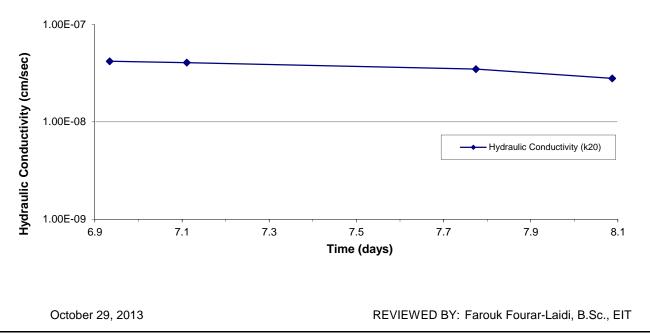
DATE TESTED: October 17th to October 25th, 2013

137.9 CONFINING PRESSURE (kPa): EFFECTIVE SATURATION STRESS (kPa): 34.5 2.71 ASSUMED SPECIFIC GRAVITY: HYDRAULIC GRADIENT: 20.3

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 4.0E-08 HYDRAULIC CONDUCTIVITY, "k20" (cm/s): 3.6E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	73.5	72.1	585.7	1.540	26.8	95.4
Final Reading	73.0	72.0	593.5	1.548	29.0	104.5





#### HYDRAULIC CONDUCTIVITY **ASTM D5084**

**Smook Contractors** 101 Hayes Road Thompson, MB **R8N 1M3** 

PROJECT: LGD of Mystery Lake Landfill

Attention: Peter Paulic PROJECT NO.: SMO-1304

SAMPLE I.D.: TH7 at 1'-3'

SOIL DESCRIPTION: Brown, stiff, moist, high plasticity silty clay

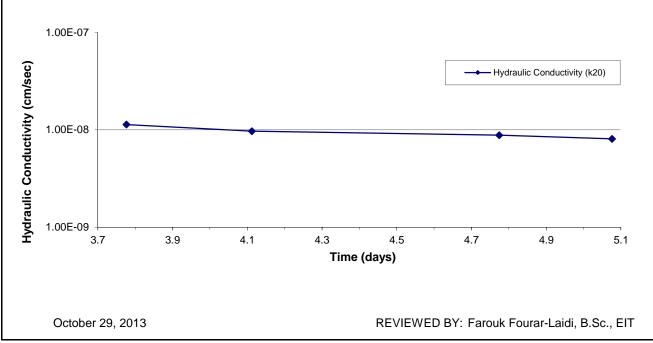
DATE TESTED: October 17th to October 22nd, 2013

137.9 CONFINING PRESSURE (kPa): EFFECTIVE SATURATION STRESS (kPa): 34.5 2.71 ASSUMED SPECIFIC GRAVITY: HYDRAULIC GRADIENT: 19.6

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.0E-08 HYDRAULIC CONDUCTIVITY, "k20" (cm/s): 9.5E-09

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	76.5	71.7	592.9	1.477	30.1	97.6
Final Reading	75.5	71.5	593.7	1.531	28.2	99.1





#### HYDRAULIC CONDUCTIVITY **ASTM D5084**

**Smook Contractors** 101 Hayes Road Thompson, MB **R8N 1M3** 

PROJECT: LGD of Mystery Lake Landfill

Attention: Peter Paulic PROJECT NO.: SMO-1304

SAMPLE I.D.: TH8 at 1'-3'

SOIL DESCRIPTION: Brown, firm, moist, high plasticity silty clay

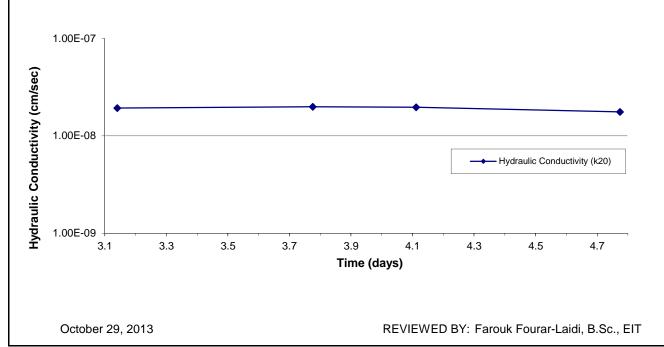
DATE TESTED: October 17th to October 22nd, 2013

137.9 CONFINING PRESSURE (kPa): EFFECTIVE SATURATION STRESS (kPa): 34.5 2.71 ASSUMED SPECIFIC GRAVITY: HYDRAULIC GRADIENT: 20.2

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 2.1E-08 HYDRAULIC CONDUCTIVITY, "k20" (cm/s): 1.9E-08

	Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Initial Reading	73.8	72.6	594.0	1.478	31.6	102.8
Final Reading	73.4	72.3	594.6	1.523	29.6	102.8



Phase III Construction W	orks – Hydraulic Con	ductivity Test Resu	ults, Stantec, Octob	er 23, 201



## Stantec Consulting Ltd. 905 Waverley Street, Winnipeg MB R3T 5P4

October 23, 2014 File: 123311511

Attention: Ken Allard Smook Contractors 101 Hayes Road Thompson, MB, R8N 1M3

Dear Ken,

Reference: Soils Testing for LGD Mystery Lake

Three soil samples, identified as Sample #2, Sample #5 and Sample #6 were submitted to our laboratory on October 3, 2014. The samples were tested in accordance with ASTM D5084, Measurement of Hydraulic Conductivity of Saturated Porous Materials using a Flexible Wall Permeameter. The test results are provided in the attached hydraulic conductivity reports and are summarized in the following table:

Sample ID	Hydraulic Conductivity, "k20"
Sample #2	7.5 x 10 ⁻⁹ cm/s
Sample # 5	2.0 x 10 ⁻⁸ cm/s
Sample # 6	1.2 x 10 ⁻⁸ cm/s

We appreciate the opportunity to assist you in this project. Please call if you have any questions regarding this report.

Regards,

STANTEC CONSULTING LTD.

Jason Thompson, C.E.T.

Associate - Manager, Materials Testing Services

Phone: (204) 928-4004 Fax: (204) 488-6947

Jason.Thompson@stantec.com

Attachment: 3x – Hydraulic Conductivity Test Report.

Design with community in mind



#### **LABORATORY**

199 Henlow Bay Winnipeg MB R3Y 1G4 Tel: (204) 488-6999

# HYDRAULIC CONDUCTIVITY ASTM D5084

PROJECT: LGD of Mystery Lake

Smook Contractors 101 Hayes Road Thompson, Manitoba R8N 1M3

Attention: Ken Allard PROJECT NO.: 123311511

SAMPLE I.D.: Sample #2

SOIL DESCRIPTION: Brown, stiff, moist, high plasticity silty clay

trace fine gravel

DATE TESTED: October 6 to October 17, 2014

CONFINING PRESSURE (kPa): 137.9

EFFECTIVE SATURATION STRESS (kPa): 34.5

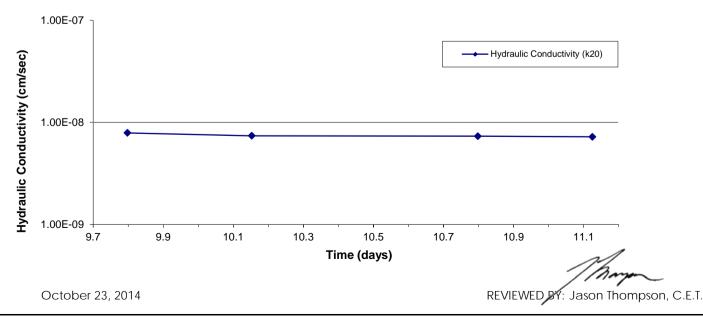
ASSUMED SPECIFIC GRAVITY: 2.71

HYDRAULIC GRADIENT: 19.9

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 8.0E-09
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 7.5E-09

		Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
	Initial Reading	74.3	72.4	605.8	1.544	28.3	101.6
	Final Reading	74.4	72.7	609.7	1.519	29.8	102.9





#### **LABORATORY**

199 Henlow Bay Winnipeg MB R3Y 1G4 Tel: (204) 488-6999

# HYDRAULIC CONDUCTIVITY ASTM D5084

PROJECT: LGD of Mystery Lake

Smook Contractors 101 Hayes Road Thompson, Manitoba R8N 1M3

Attention: Ken Allard PROJECT NO.: 123311511

SAMPLE I.D.: Sample #5

SOIL DESCRIPTION: Brown, stiff, moist, high plasticity silty clay

trace fine gravel

DATE TESTED: October 6 to October 14, 2014

CONFINING PRESSURE (kPa): 137.9

EFFECTIVE SATURATION STRESS (kPa): 34.5

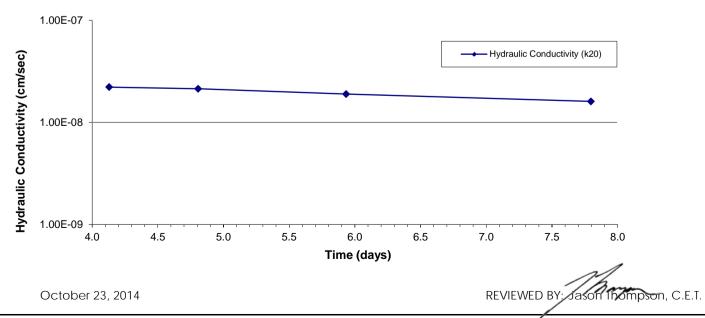
ASSUMED SPECIFIC GRAVITY: 2.71

HYDRAULIC GRADIENT: 20.4

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 2.0E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 2.0E-08

		Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
Ī	Initial Reading	72.4	72.5	572.8	1.454	31.9	100.1
	Final Reading	72.4	72.1	575.6	1.464	33.1	105.4





#### **LABORATORY**

199 Henlow Bay Winnipeg MB R3Y 1G4 Tel: (204) 488-6999

# HYDRAULIC CONDUCTIVITY ASTM D5084

PROJECT: LGD of Mystery Lake

Smook Contractors 101 Hayes Road Thompson, Manitoba R8N 1M3

Attention: Ken Allard PROJECT NO.: 123311511

SAMPLE I.D.: Sample #6

SOIL DESCRIPTION: Brown, stiff, moist, high plasticity silty clay

trace fine gravel

DATE TESTED: October 6 to October 14, 2014

CONFINING PRESSURE (kPa): 137.9

EFFECTIVE SATURATION STRESS (kPa): 34.5

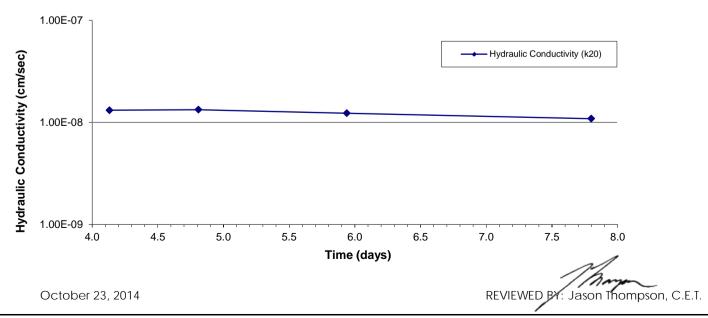
ASSUMED SPECIFIC GRAVITY: 2.71

HYDRAULIC GRADIENT: 20.6

TYPE OF PERMEANT LIQUID: De-aired Water

HYDRAULIC CONDUCTIVITY, "k" (cm/s): 1.3E-08
HYDRAULIC CONDUCTIVITY, "k₂₀" (cm/s): 1.2E-08

		Height (mm)	Diameter (mm)	Wet Mass (g)	Dry Density (g/cm³)	Water Content (%)	Saturation (%)
	Initial Reading	71.9	72.5	578.5	1.506	29.4	99.8
	Final Reading	71.9	72.1	579.8	1.522	29.8	103.2



#### Appendix C

Plan 1: Site Layout with Approximate Location of Property Line

Plan 2: Final Cover Grading Contours and Final Drainage Plan

Phase I Works – Record Drawing Plan Set

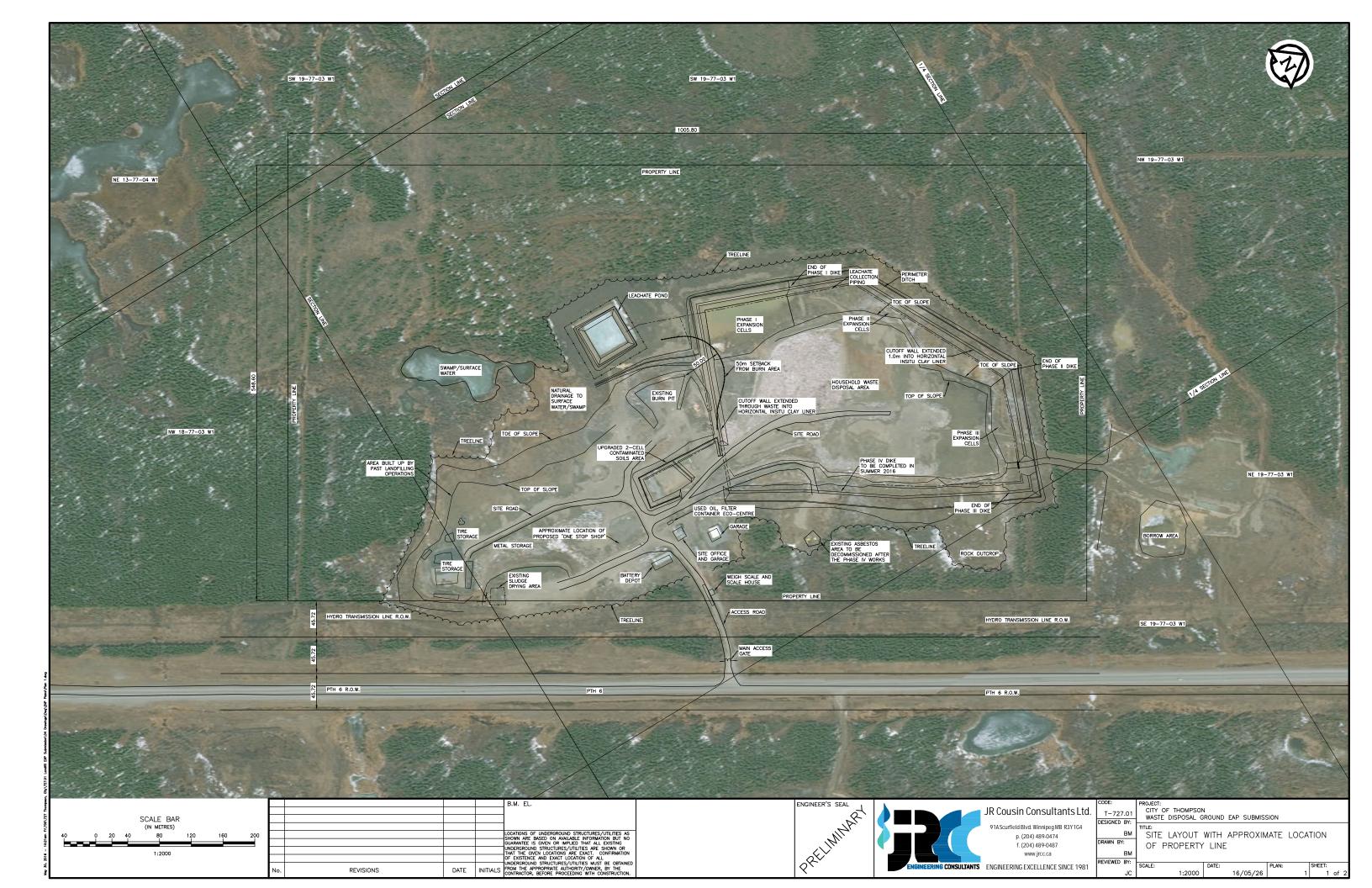
Phase II Works – Record Drawing Plan Set

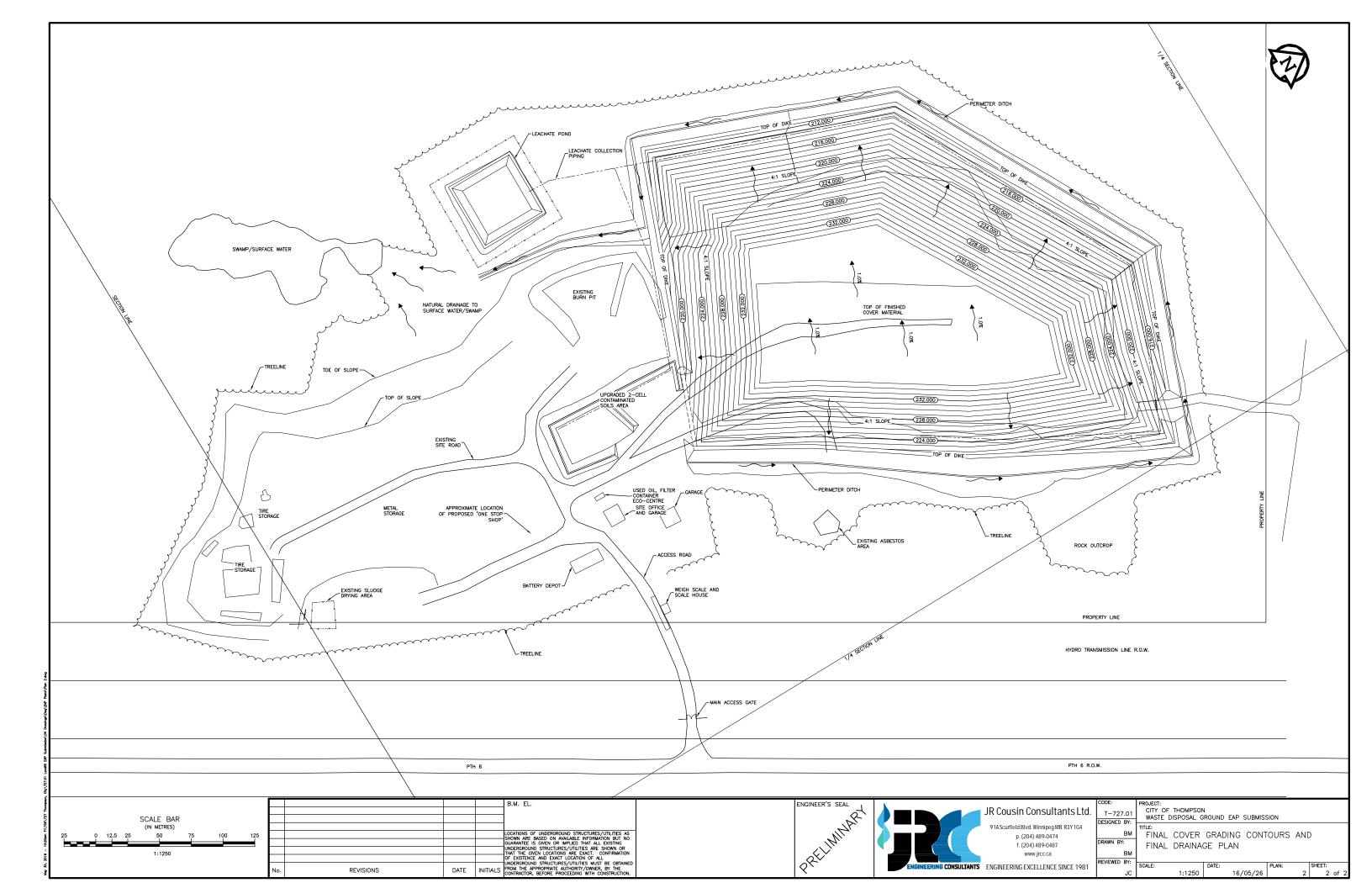
Phase III Works – Record Drawing Plan Set

Phase IV Works – Design Drawing Plan Set

Plan 1: Site Layout with Approximate Location of Property Line

Plan 2: Final Cover Grading Contours and Final Drainage Plan







# LGD of MYSTERY LAKE WASTE DISPOSAL GROUND PHASE I WORKS

# **PLAN INDEX**

PLAN 1. DRAWING LEGEND, ABBREVIATION INDEX AND KEY PLANPLAN 2. EXISTING SITE LAYOUT WITH TEST HOLE LOCATIONS

PLAN 3. EXISTING SITE LAYOUT WITH CONTOUR LINES

**PLAN 4.** OVERALL MASTER PLAN SHOWING ALL DEVELOPMENT PHASES

**PLAN 5.** PHASE I WORKS

PLAN 6. ACTIVE CELL AND LEACHATE POND DIKE DETAILS, LEACHATE COLLECTION

PIPING AND DITCH DETAILS

**PLAN 7.** WDG OPERATIONS PLAN

PLAN 8. FENCE, SIGN, LEACHATE COLLECTION PIPING AND EROSION CONTROL DETAILS

# J.R. Cousin Consultants Ltd. Consulting Engineers and Project Managers

Ph (204) 489-0474 Fax (204) 489-0487 www.jrcc.ca

Record Drawing

Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent

### DRAWING LEGEND:

PIPING:		ROADS AND	D DRAINAGE:	<u>MISCELLAN</u>	EOUS:
	EXISTING WATERMAIN PROPOSED WATERMAIN FUTURE WATERMAIN		EXISTING ROAD CENTERLINE PROPOSED ROAD CENTERLINE FUTURE ROAD CENTERLINE	XX	EXISTING FENCE LINE PROPOSED FENCE LINE
	EXISTING SEWERMAIN PROPOSED SEWERMAIN		EXISTING ROAD SHOULDER PROPOSED ROAD SHOULDER	—H—H— — <b>H—H</b> —	EXISTING HYDRO LINE PROPOSED HYDRO LINE
	FUTURE SEWERMAIN			——G——G—	EXISTING GAS LINE
	EXISTING FORCEMAIN PROPOSED FORCEMAIN		EXISTING ROAD EDGE PROPOSED ROAD EDGE FUTURE ROAD EDGE	——MTS——	EXISTING MTS LINE
	FUTURE FORCEMAIN  EXISTING RAW WATERMAIN		EXISTING SIDEWALK		EXISTING BUILDING PROPOSED BUILDING
	PROPOSED RAW WATERMAIN		PROPOSED SIDEWALK		LEGAL/LOT LINE
	FUTURE RAW WATERMAIN  EXISTING LAND DRAINAGE SEWER		EXISTING DITCH PROPOSED DITCH	++++++++	RAILWAY LINE
	PROPOSED LAND DRAINAGE SEWER FUTURE LAND DRAINAGE SEWER		EXISTING CULVERT		MATCH LINE
FH -∳-	EXISTING FIRE HYDRANT		PROPOSED CULVERT	H₽	HYDRO POLE
FH +	PROPOSED FIRE HYDRANT	4	EXISTING DRAINAGE DIRECTION	W	WATER HOLDING TANK
⊗	EXISTING VALVE	<b>←</b>	PROPOSED DRAINAGE DIRECTION	S	SEPTIC TANK
⊗ <b>⊗</b>	PROPOSED VALVE	<u></u>	CONTOURS - MAJOR INTERVALS	$\Theta$	SEWAGE HOLDING TANK
co	EXISTING CLEANOUT	— _{100.5}	CONTOURS - MINOR INTERVALS	<del>  </del>	SURVEY BAR
co	PROPOSED CLEANOUT	×100.00	EXISTING GROUND ELEVATION	<b>+</b>	SURVEY MONUMENT/BENCHMARK
MH	EXISTING MANHOLE	100.00	PROPOSED GROUND ELEVATION	$\sim$	EXISTING VEGETATION
MH	PROPOSED MANHOLE	(100.00)	EXISTING ROAD ELEVATION	$\sim$	PROPOSED VEGETATION
ð	EXISTING CURBSTOP	100.00	PROPOSED ROAD ELEVATION	<u>(01)</u>	DOOR CONSTRUCTION TYPE
•	PROPOSED CURBSTOP	TOP	EXISTING SLOPE	W1)	WALL CONSTRUCTION TYPE
СВ	EXISTING CATCH BASIN				EASEMENT
СВ	PROPOSED CATCH BASIN	ТТТТТТТ ВОТТОМ	PROPOSED SLOPE		NORTH ARROW

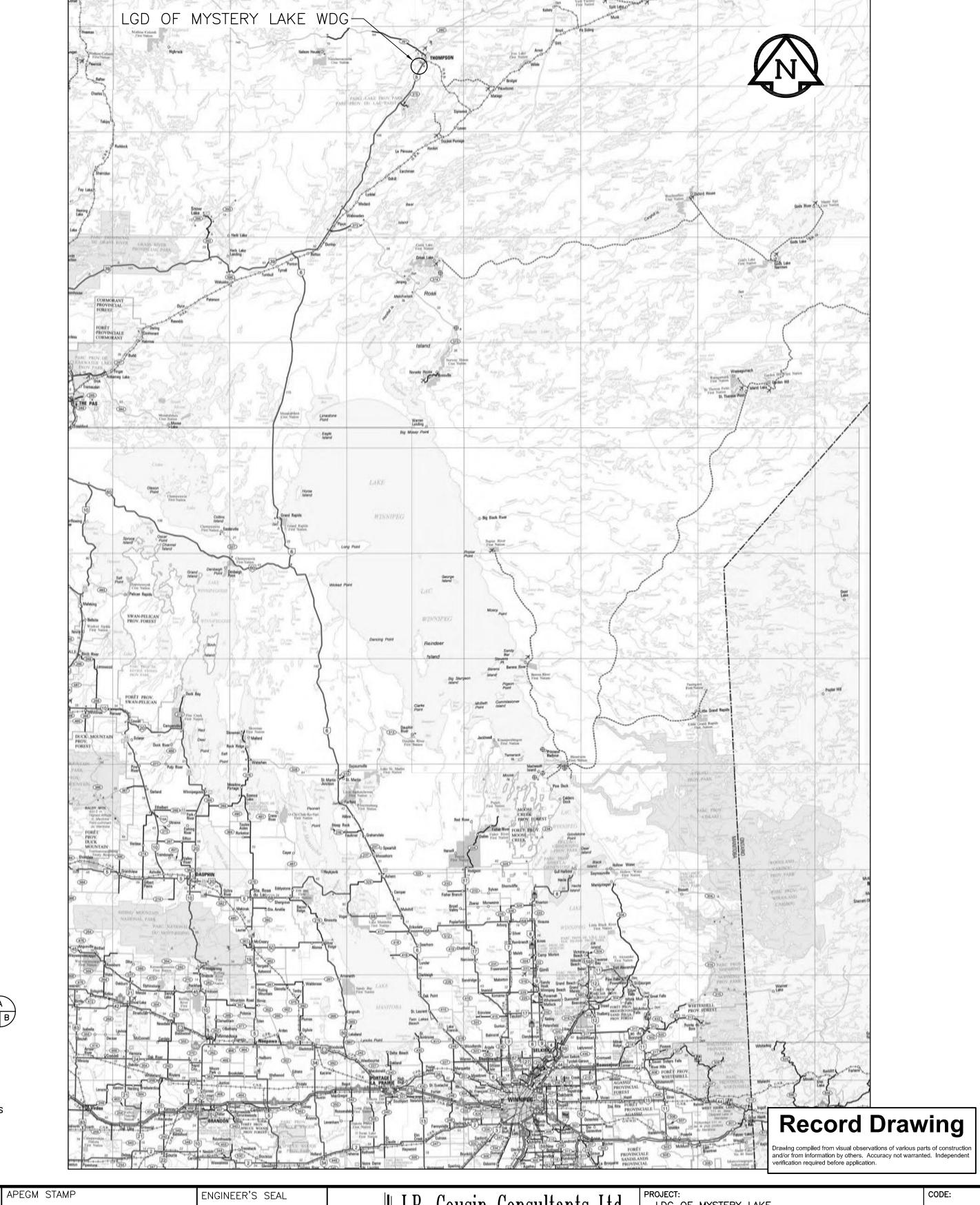
## **ABBREVIATIONS:**

	AT	_	FACT	IOT	HINOTION	DAD	DADUIG
<b>@</b>	AT AND CONDITIONING	E	EAST	JCT JP	JUNCTION	RAD	RADIUS ROAD
A/C	AIR CONDITIONING	EC	END OF CURVE	JP	JOCKEY PUMP	RD	REVISION
ALUM	ALUMINUM	EL ELEC	ELEVATION ELECTRICAL	LAD	LADODATODY	REV	RIGHT OF WAY
ASPH	ASPHALT			LAB	LABORATORY	ROW	
AVE	AVENUE	EP	EDGE OF PAVEMENT	LAM	LAMINATE	RM	ROOM
AVG	AVERAGE	ER	EDGE OF ROAD	LAT	LATITUDE	•	COUTU
		E/W	EACHWAY	LDS	LAND DRAINAGE SEWER	S	SOUTH
BD	BOTTOM OF DITCH	EXT	EXTERIOR	LF ···-	LEVEL FLOAT	SCH	SCHEDULE
BLDG	BUILDING			LLF	LOW LEVEL FLOAT	SECT	SECTION
BLVD	BOULEVARD	FAX	FAX MACHINE STAND	LONG	LONGITUDE	SHT	SHEET
ВМ	BENCHMARK	FC	FILE CABINET	LWL	LOW WATER LEVEL	SIB	STEEL IRON BAR
BOT	ВОТТОМ	FD	FLOOR DRAIN			SPEC	SPECIFICATION
BP	BACKWASH PUMP	F/F	FACE TO FACE	М	METRE	SQ	SQUARE
B/W	BOTHWAYS	FH	FIRE HYDRANT	MAX	MAXIMUM	SS	SOUTH SHORE
		FM	FORCEMAIN	MCC	MOTOR CONTROL CENTER	ST	STREET
		FP	FIRE PUMP	MECH	MECHANICAL	STD	STANDARD
CB	CATCH BASIN	FT	FOOT, FEET	MEMB	MEMBRANE	SUSP	SUSPENDED
CI	CAST IRON		•	MH	MANHOLE	SW	SIDEWALK
CHKD	CHECKED	GA	GAUGE	MIN	MINIMUM		
CNR	CANADIAN NATIONAL RAILWAY	GALV	GALVANIZED	MM	MILLIMETRE	TEL	TELEPHONE
CO	CLEANOUT					TEMP	TEMPORARY
COL	COLUMN	HA	HECTARE	N	NORTH	TP	TRUCKFILL PUMP
CONC	CONCRETE	HB	HOSE BIBB	NAT	NATURAL	TYP	TYPICAL
CONST	CONSTRUCTION	HI	HEIGHT OF INSTRUMENT	NBC	NATIONAL BUILDING CODE		
CONT	CONTINUOUS	HLF	HIGH LEVEL FLOAT	NS	NORTH SHORE	VERT	VERTICAL
COORD	COORDINATE	HPW	HIGH PRESSURE WATER LINE	NTS	NOT TO SCALE	VOL	VOLUME
CPR	CANADIAN PACIFIC RAILWAY	HORIZ	HORIZONTAL	NWL	NORMAL WATER LEVEL		
C/W	COMPLETE WITH	HP	HYDRO POLE			US	ULTRASONICS TRANSDUCER
•		HST	HYDROSTATIC TRANSDUCER	0/C	ON CENTRE		
DCW	DOMESTIC COLD WATER	HR	HOUR	0/D	OUTSIDE DIAMETER	VAR	VARIES
DEG	DEGREE	HVAC	HEATING, VENTILATING AND	•		VB	VAPOUR BARRIER
DHW	DOMESTIC HOT WATER	пуас	AIR CONDITIONING	0/F	OUTSIDE FACE	VERT	VERTICAL
DIA	DIAMETER	1.1547		0/H	OVER HEAD	VFD	VARIABLE FREQUENCY DRIVE
DIM	DIMENSION	HW	HOT WATER TANK	OD	OUTSIDE DIAMETER	<b>VI</b> D	VARIABLE TREGOLITOT DITTE
DIST	DISTANCE	HWL	HIGH WATER LEVEL	ORIG	ORIGINAL	w	WEST
DN	DOWN	15	NODE DIAMETED	OWSJ	OPEN WEB STEEL JOIST		WITHOUT
DP	DUTY PUMP	ID 	INSIDE DIAMETER			w/o	
DR	DRIVE	IL.	ICE LEVEL	PLYWD	PLYWOOD	WL	WATER LEVEL
	DRAWING	INCL	INCLUDE	PS	PRESSURE SEWER	WM	WATERMAIN
DWG	DRAWING	INT	INTERIOR	POLY	POLYETHYLENE	wws	WASTEWATER SEWER
		INV	INVERT	PROP	PROPERTY	WT	WEIGHT

PVC POLY VINYL CHLORIDE

A - DETAIL NUMBER
B - PLAN WHERE DETAIL EXPANDED
C - PLAN WHERE DETAIL ORIGINATES

NOTE: -WHOLE NUMBERS INDICATE MILLIMETERS -DECIMALIZED NUMBERS REPRESENT METERS



B.M. ELEV.

B.M. ELEV.

LOCATIONS OF UNDERGROUND STRUCTURES/UTILITIES AS SHOWN ARE BASED ON AVAILABLE INFORMATION BUT NO GUARANTEE IS GIVEN OR IMPLIED THAT ALL EXISTING UNDERGROUND STRUCTURES/UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION OF EXISTENCE AND EXACT. CONFIRMATION OF EXISTENCE AND EXACT LOCATION OF ALL UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR, BEFORE PROCEEDING WITH CONSTRUCTION.

ORIGINAL DRAWING SIGNED AND SEALED BY G.R. COUSIN 11/10/20

Certificate of Authorization

J.R. Cousin Consultants Ltd.

No. 234 Date: 11/10/20

J.R. COUSIN CONSUITAT

Consulting Engineers and Project

Ph (204) 489-0474 Fax (204) 489-0487

LDG OF MYSTERY LAKE
WASTE DISPOSAL GROUND PHASE I WORKS
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DRAWING LEGEND ABBREVIATION

TITLE:

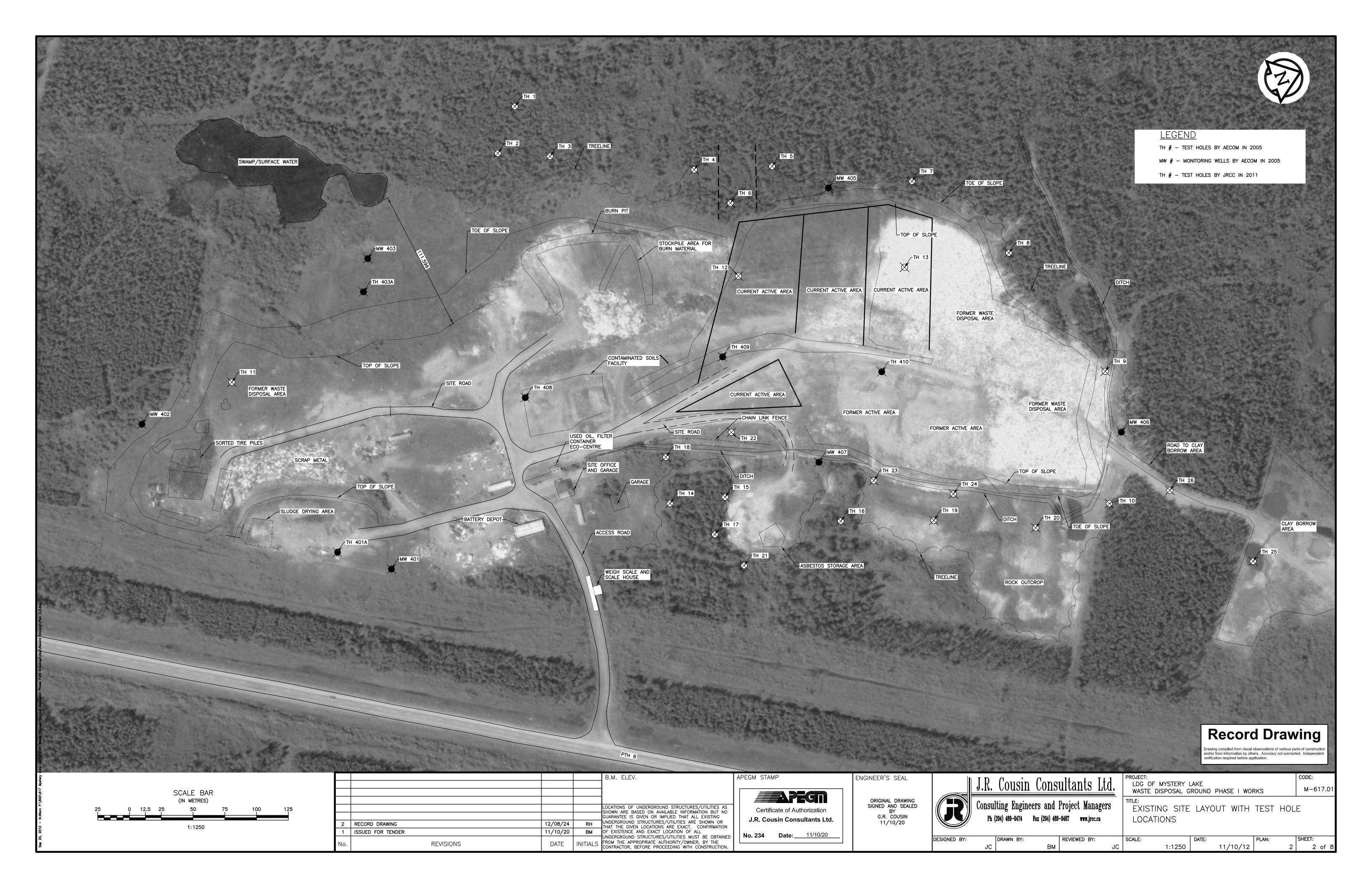
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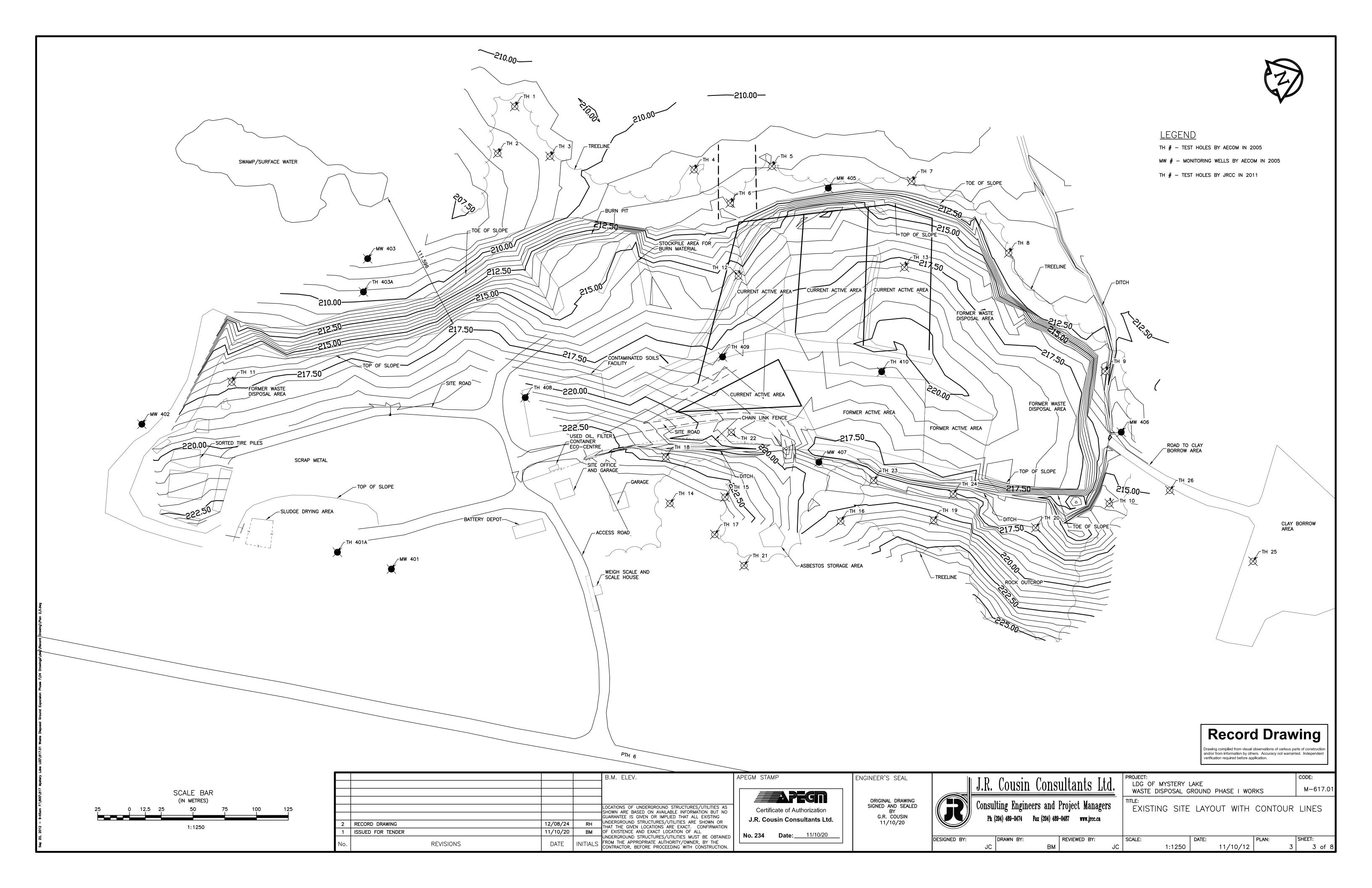
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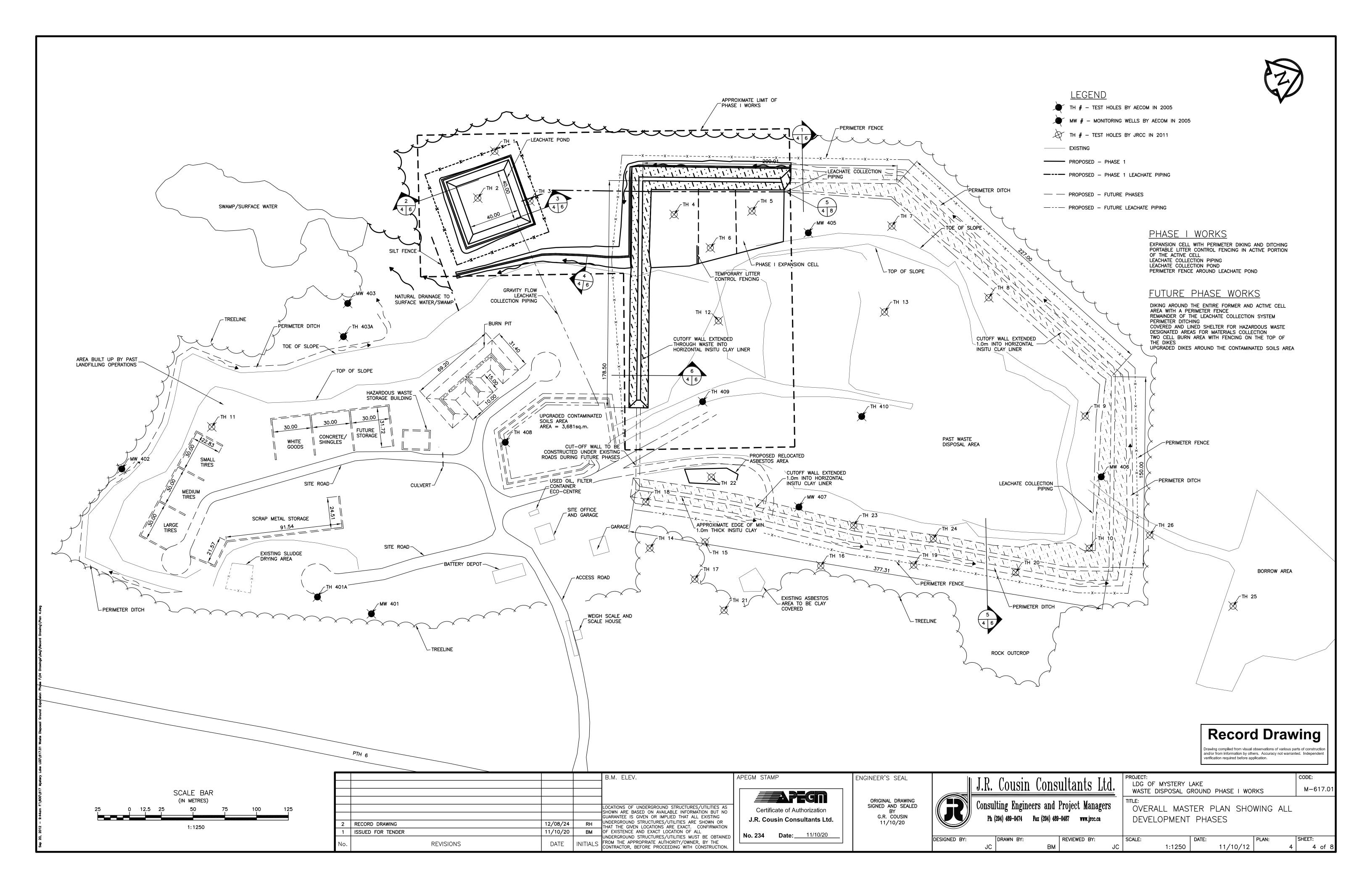
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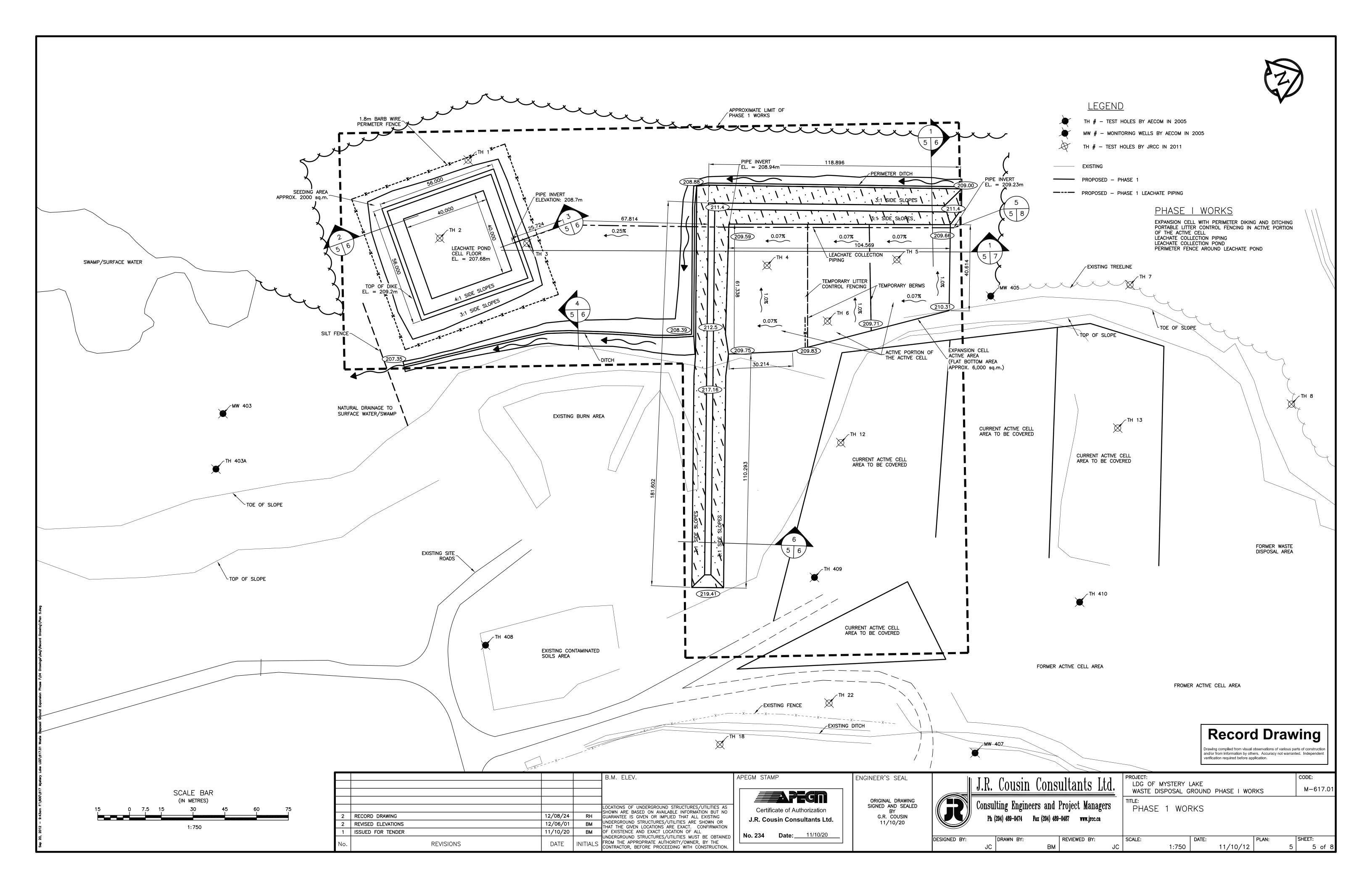
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 DRAWN BY:
 REVIEWED BY:
 SCALE:
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 PLAN:
 SHEET:

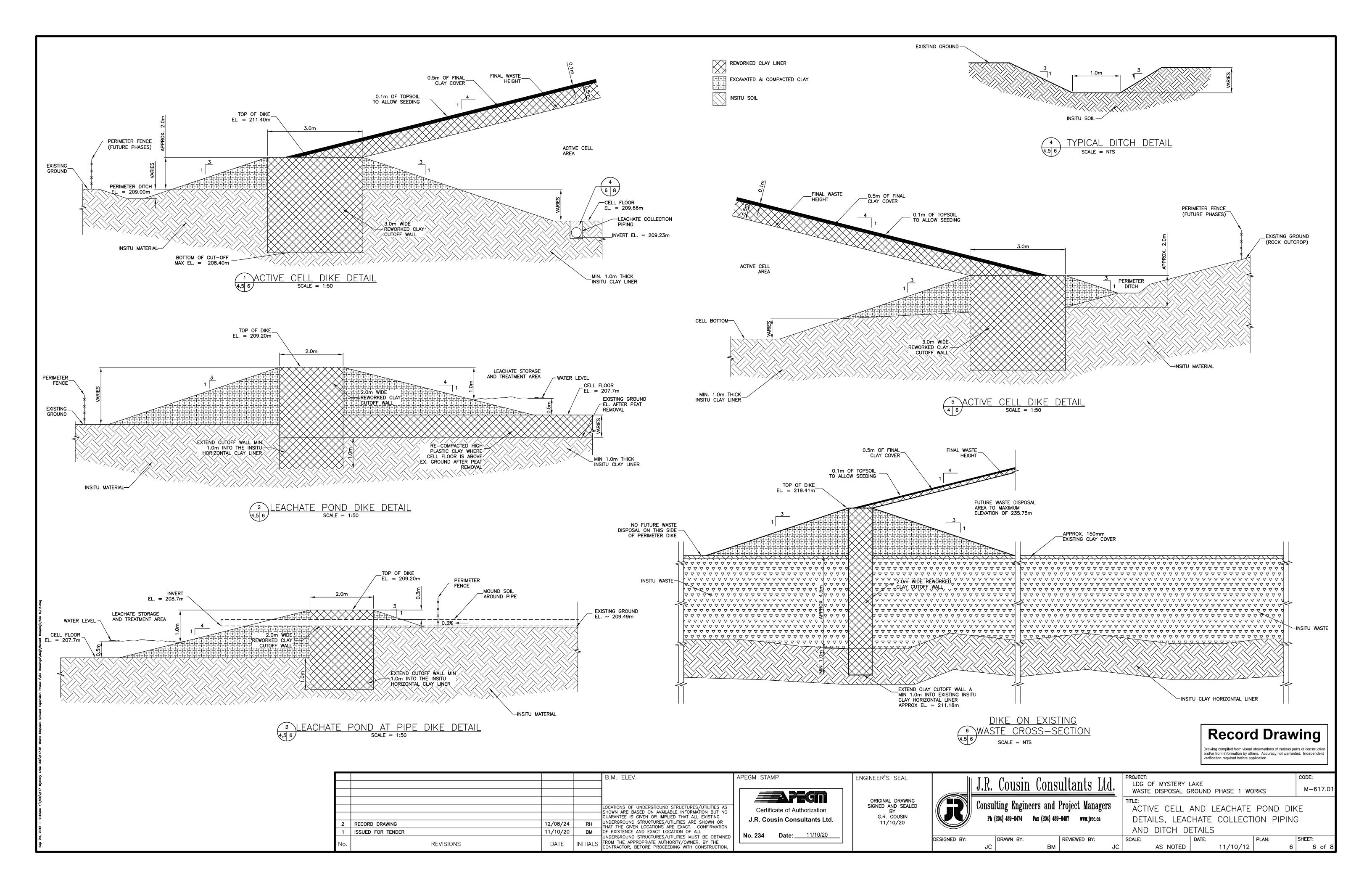
 JC
 BM
 JC
 NTS
 11/10/12
 1
 1 of 8

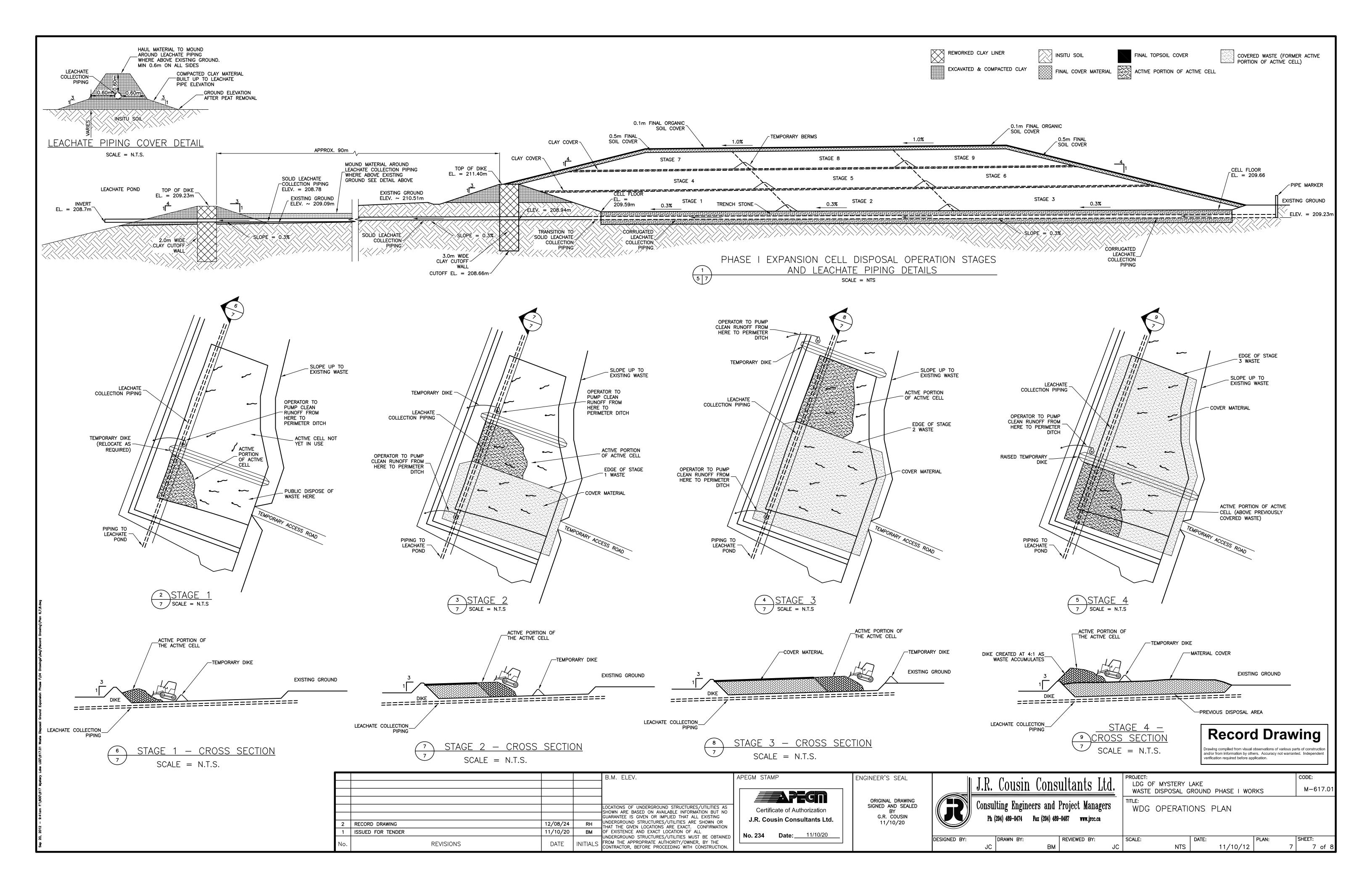


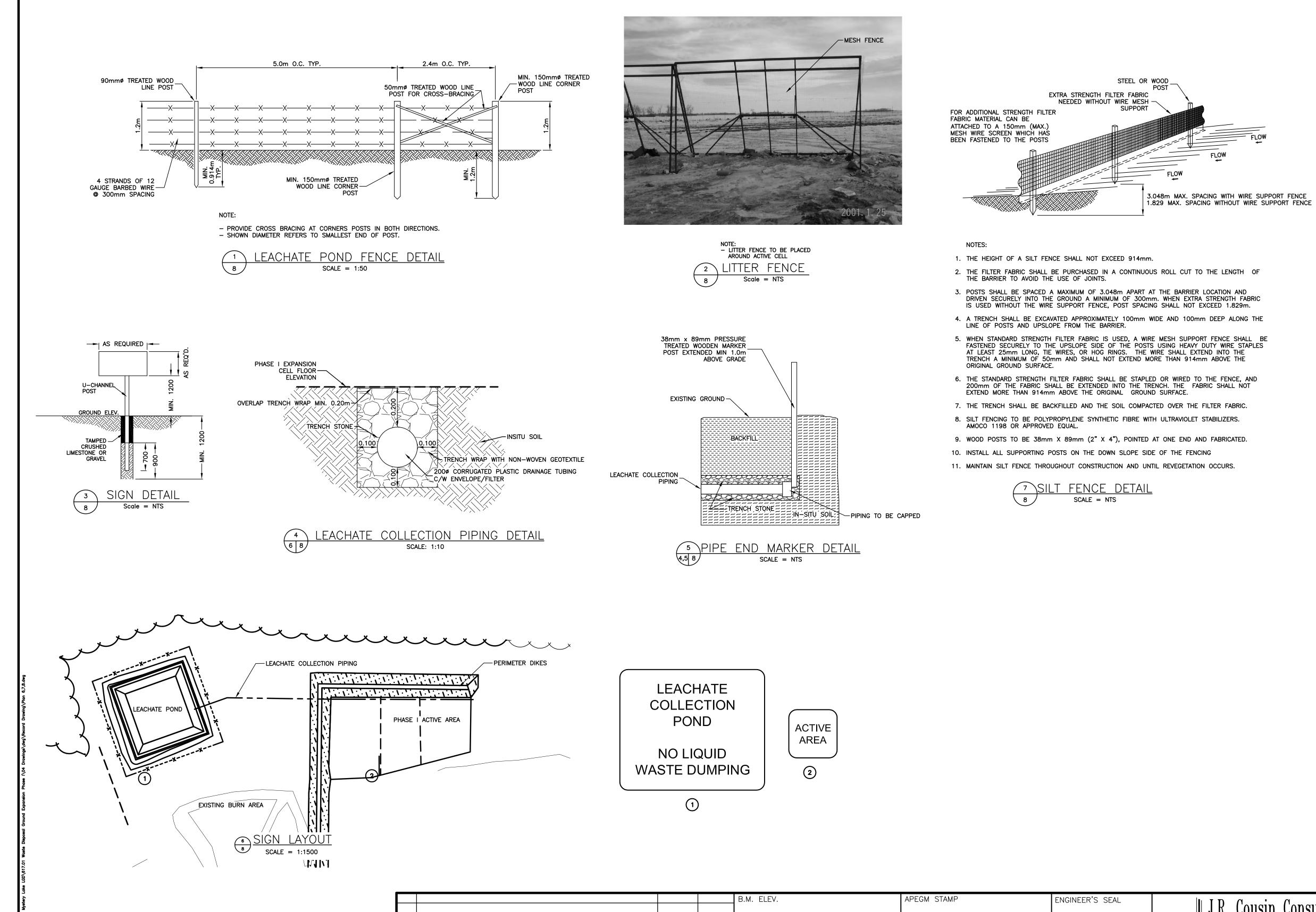


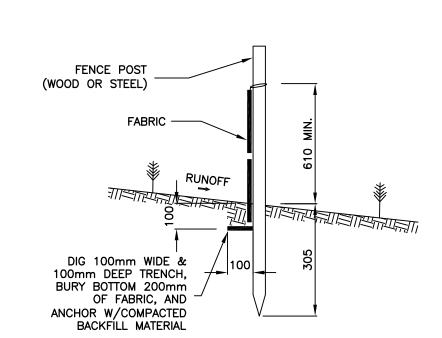




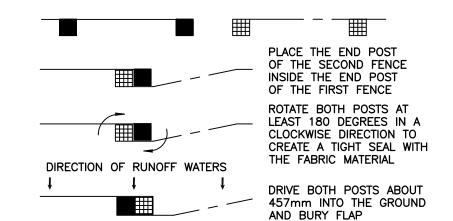








8 SILT FENCE SECTION
SCALE - NTS



9 SILT FENCES 8 SCALE = NTS

# Record Drawing

Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent verification required before application.

				B.M. ELEV.	APEGM STAMP	ENGINEER'S SEAL		J.R. Cousin	Consultants Lt	LDG OF MYSTERY		CODE: M-617.01
				LOCATIONS OF UNDERGROUND STRUCTURES/UTILITIES AS	Certificate of Authorization	ORIGINAL DRAWING SIGNED AND SEALED			s and Project Manager	TITLE:	GROUND PHASE I WORKS  LEACHATE COLLEC	
		/08/24 /10/20	RH BM	SHOWN ARE BASED ON AVAILABLE INFORMATION BUT NO GUARANTEE IS GIVEN OR IMPLIED THAT ALL EXISTING UNDERGROUND STRUCTURES/UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION OF EXISTENCE AND EXACT LOCATION OF ALL	J.R. Cousin Consultants Ltd.	G.R. COUSIN 11/10/20		0 0	x (204) 489-0487 www.jrcc.ca	121102, 01011	N CONTROL DETAIL	
No.	REVISIONS		INITIALS	UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR, BEFORE PROCEEDING WITH CONSTRUCTION.	No. 234 Date: 11/10/20		DESIGNED BY:	JC DRAWN BY:	REVIEWED BY:	SCALE:  JC AS NOTED	DATE: PLA 11/10/12	N: SHEET: 8 of 8



# LGD of MYSTERY LAKE WASTE DISPOSAL GROUND PHASE II WORKS

# **PLAN INDEX**

**PLAN 1.** DRAWING LEGEND, ABBREVIATION INDEX AND KEY PLAN

**PLAN 2.** EXISTING WDG LAYOUT AFTER PHASE I WORKS WITH TEST HOLE LOCATIONS

PLAN 3. OVERALL WASTE DISPOSAL GROUND LAYOUT SHOWING PROPOSED PHASE II WORKS

**PLAN 4.** PHASE II ACTIVE CELL DIKES

PLAN 5. CONTAMINATED SOILS AREA AND LEACHATE COLLECTION PIPE LAYOUT

PLAN 6. LEACHATE COLLECTION PIPE PROFILE

PLAN 7. ACTIVE CELL DIKES, CONTAMINATED SOIL DIKES, LEACHATE COLLECTION PIPING, PIPE END

MARKER AND SILT FENCE DETAILS



# J. R. Cousin Consultants Ltd.

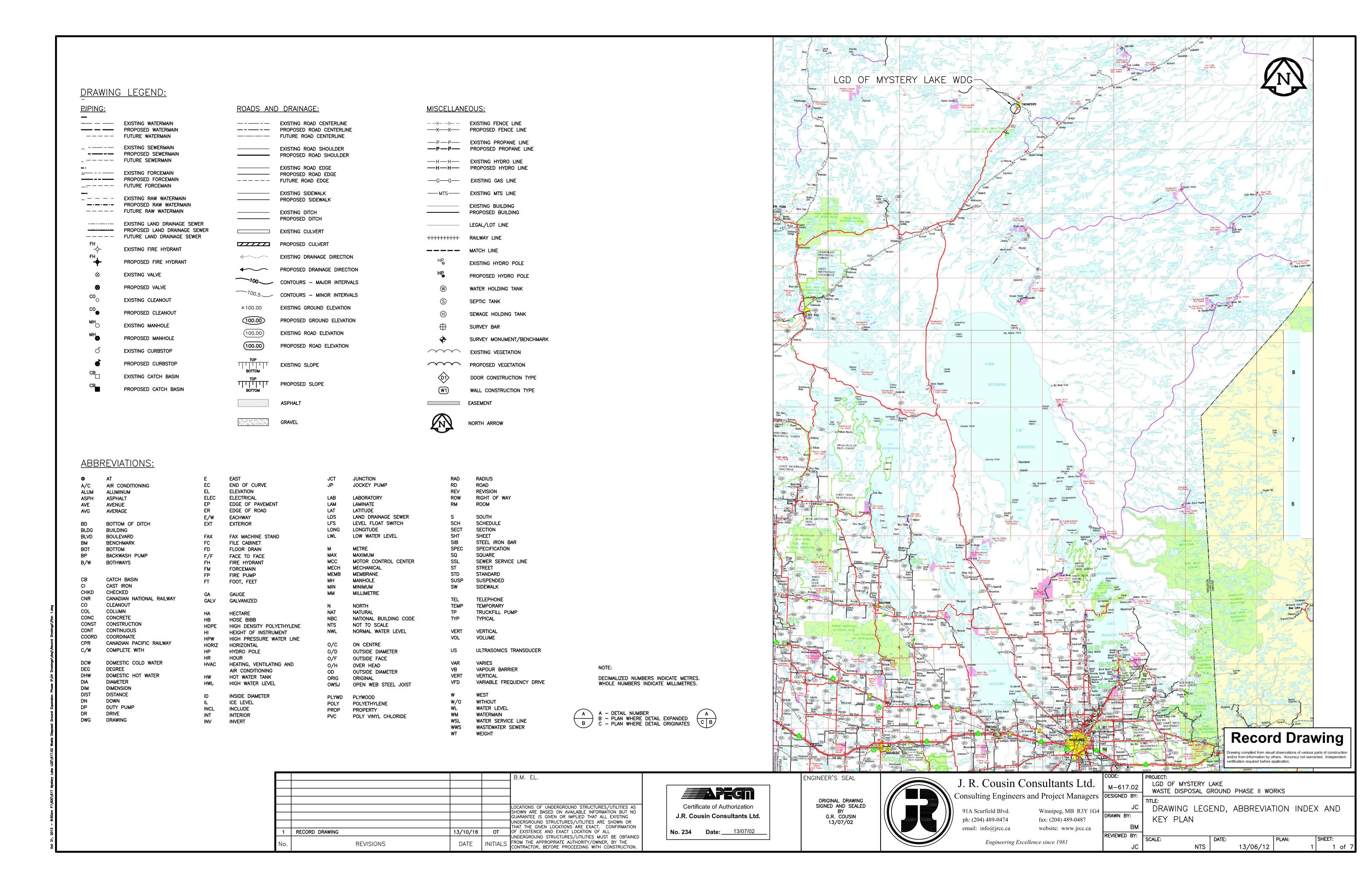
Consulting Engineers and Project Managers

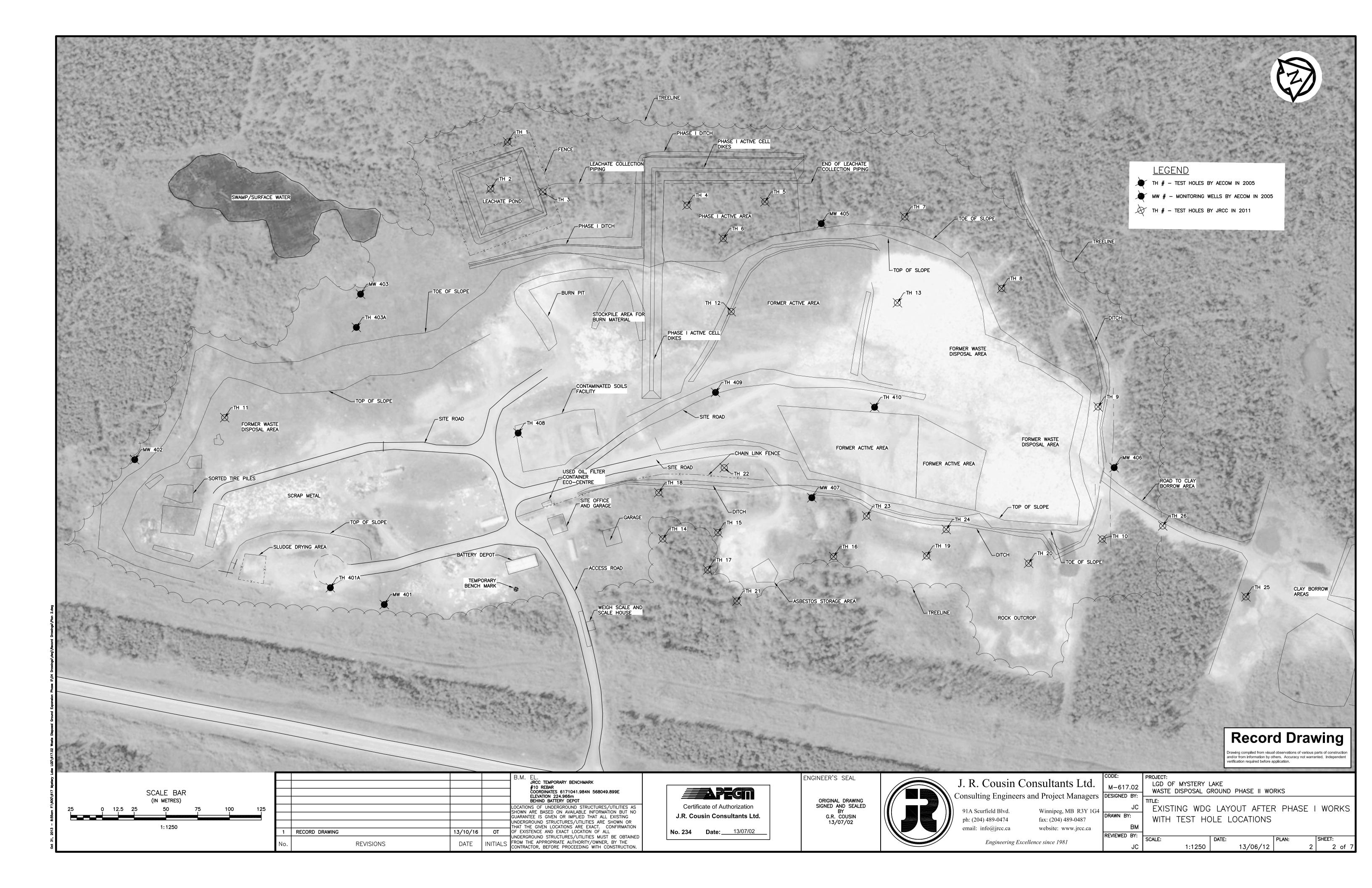
91A Scurfield Blvd. Winnipeg, MB R3Y 1G4 ph: (204) 489-0474 fax: (204) 489-0487 email: info@jrcc.ca website: www.jrcc.ca

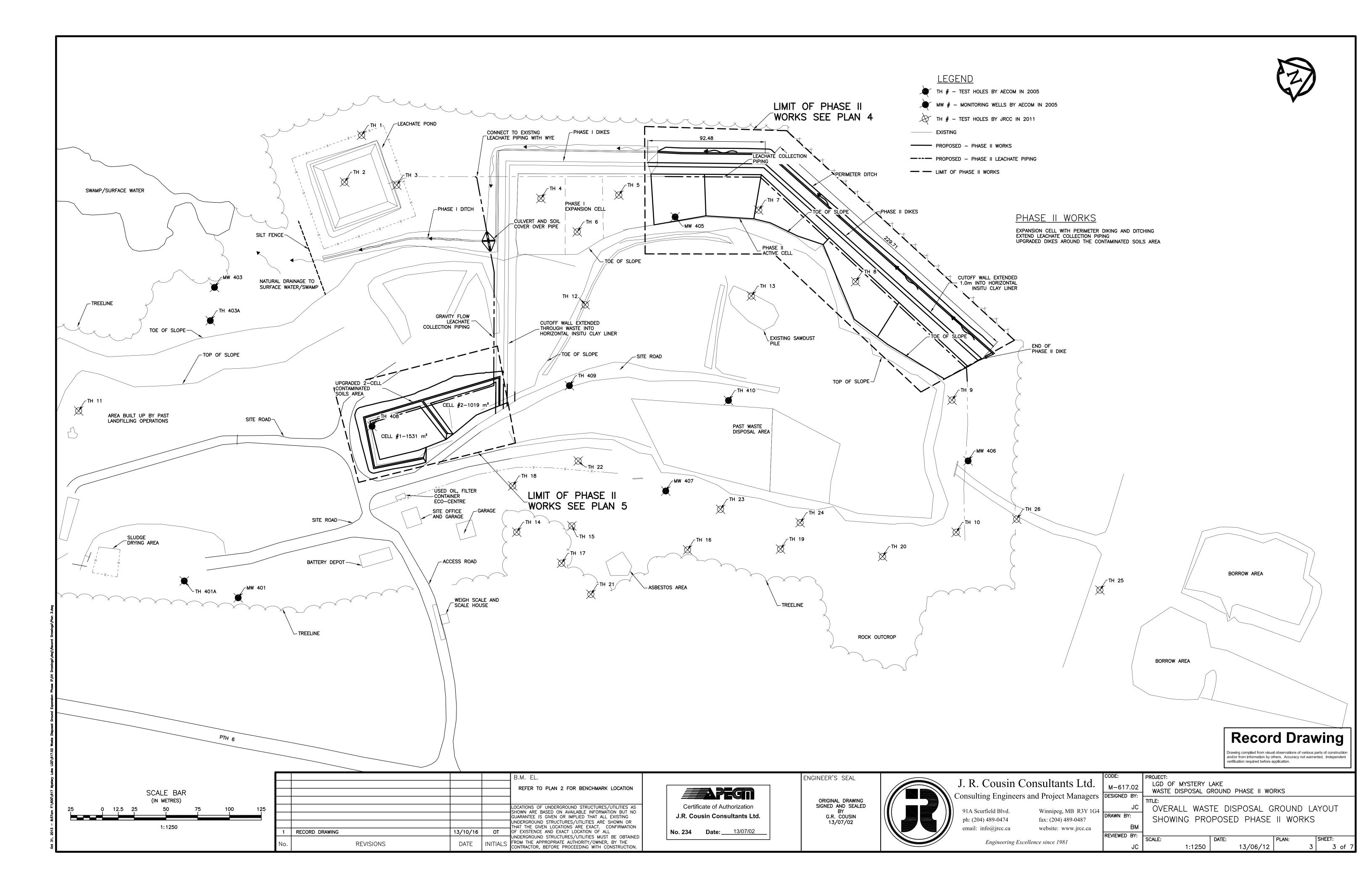
Engineering Excellence since 1981

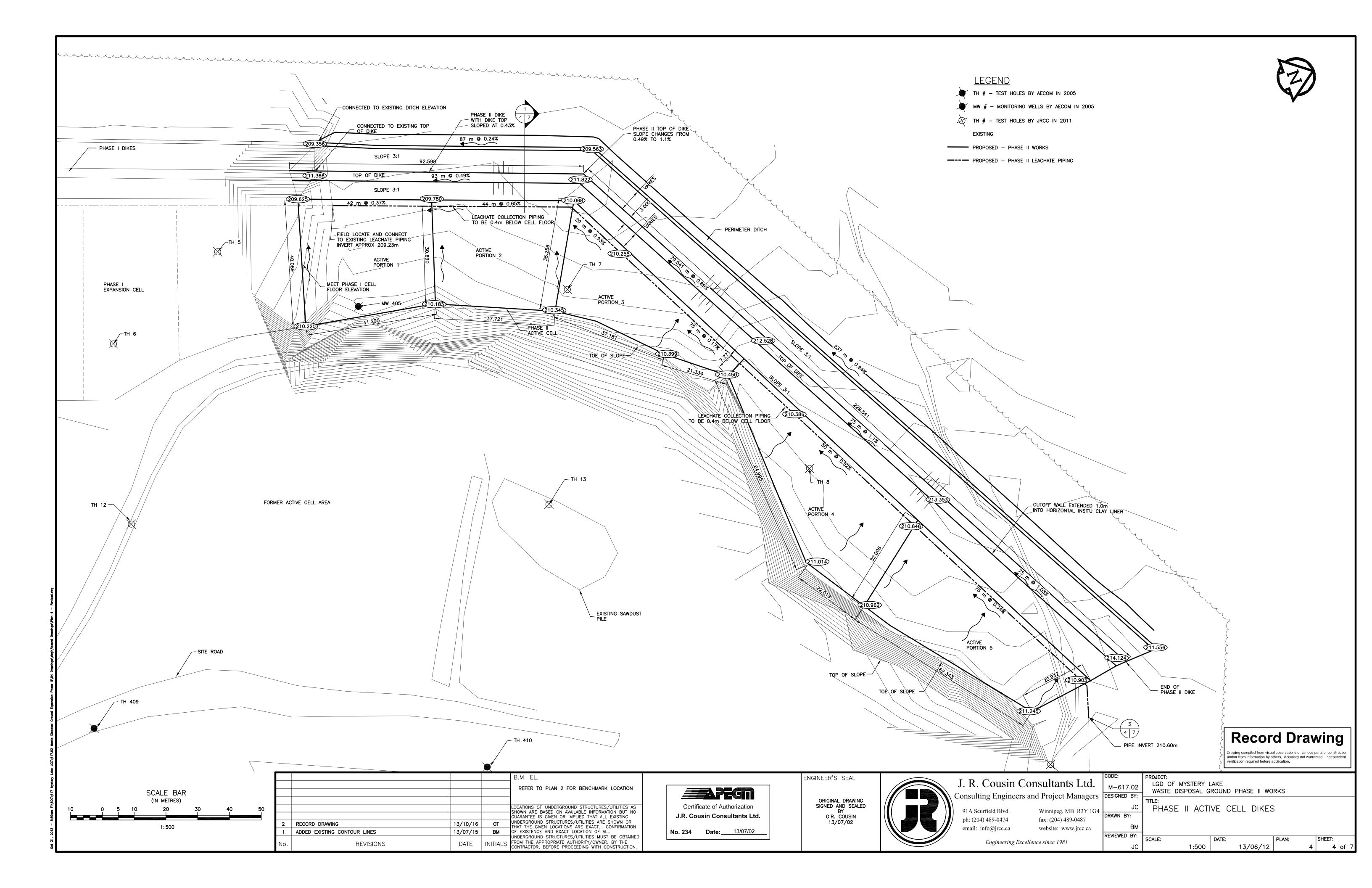
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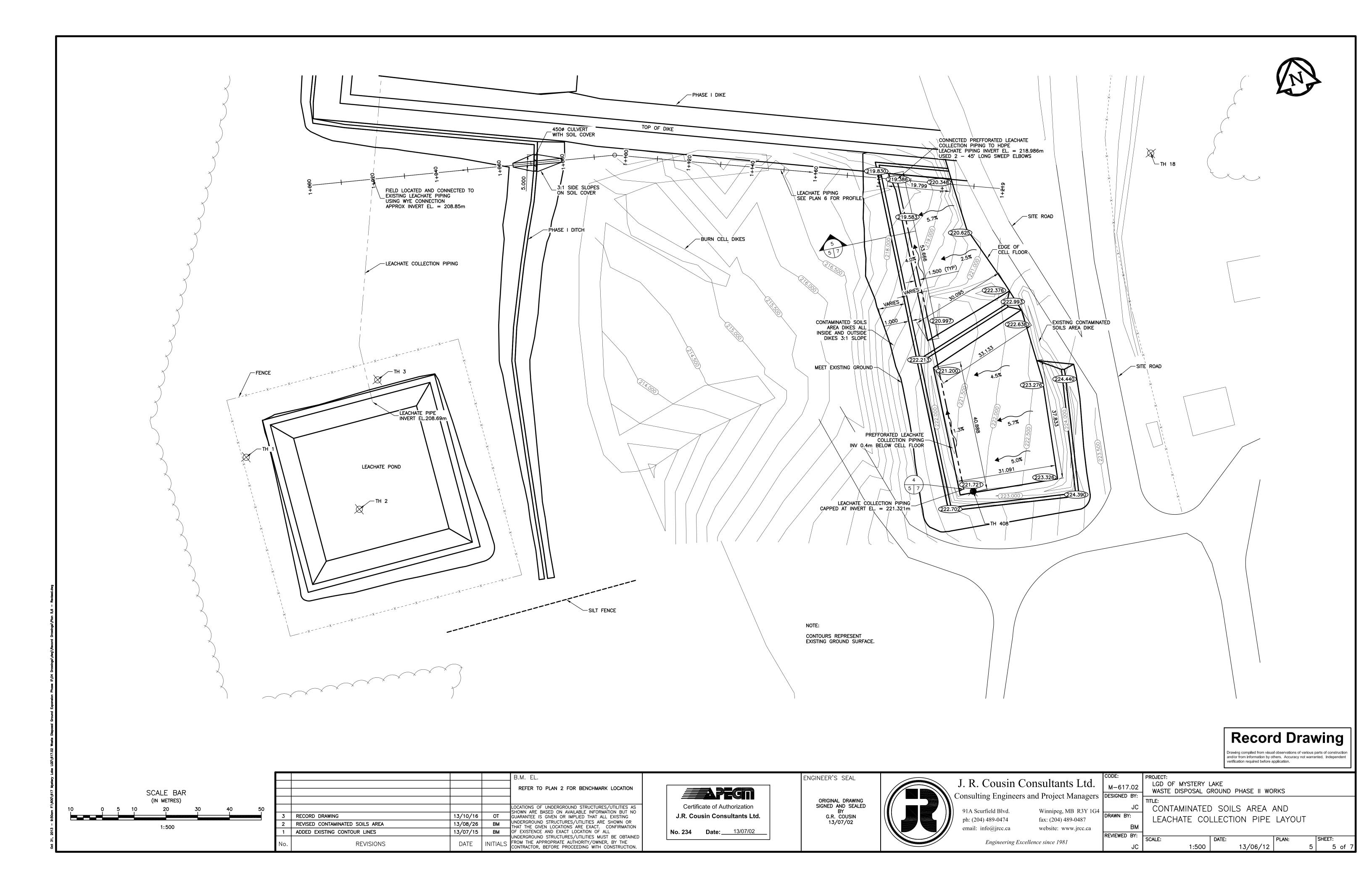
Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent verification required before application.

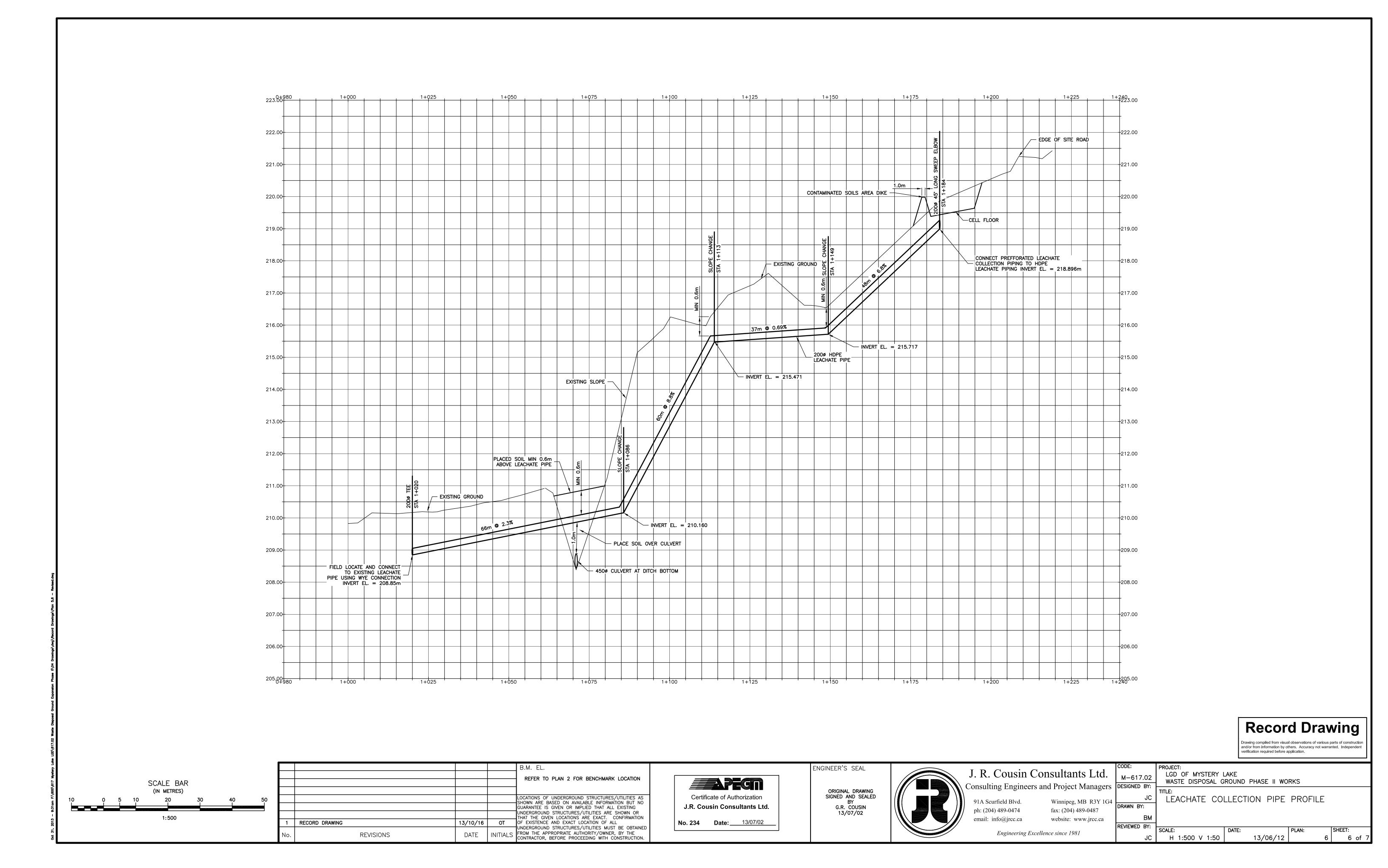


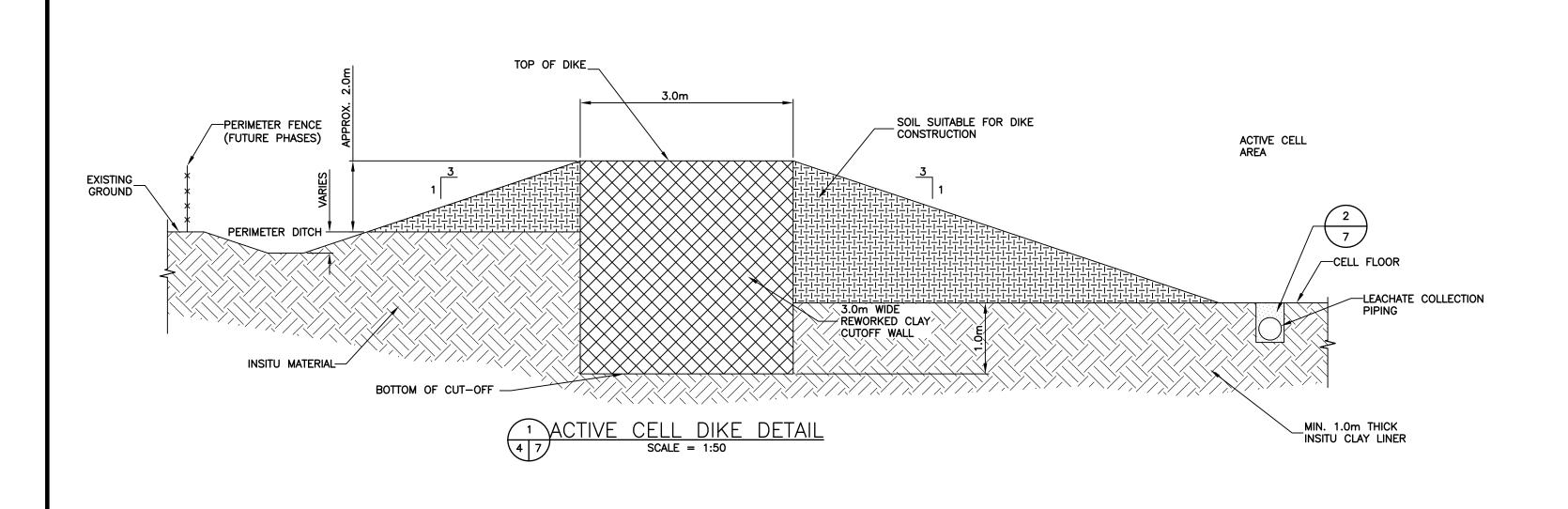


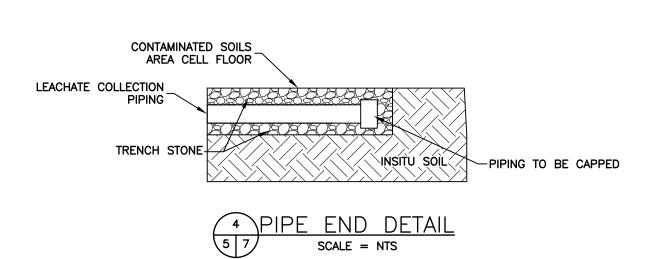


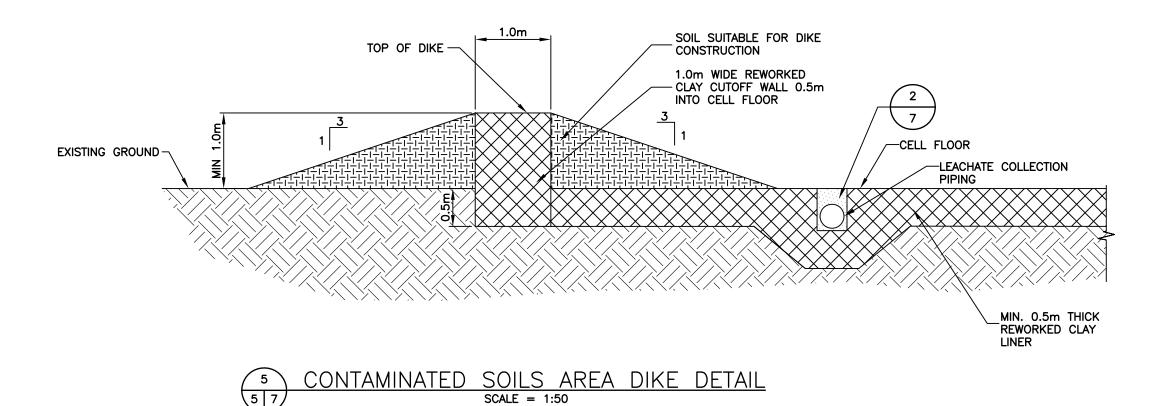


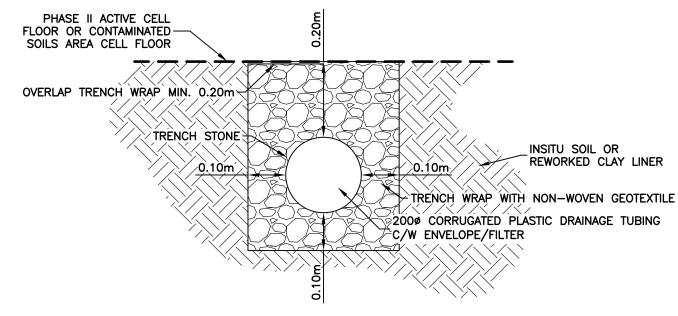




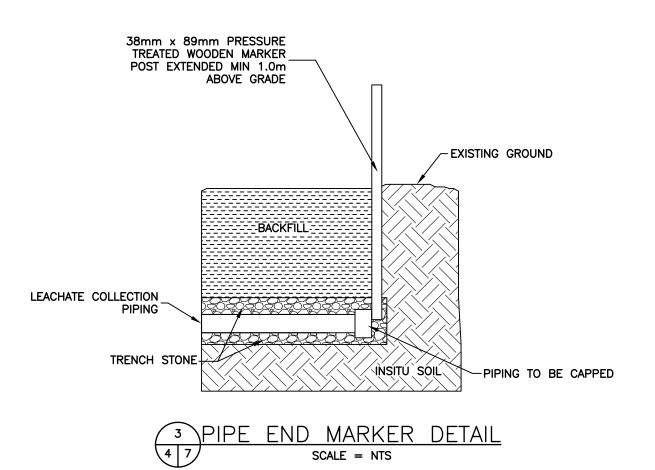


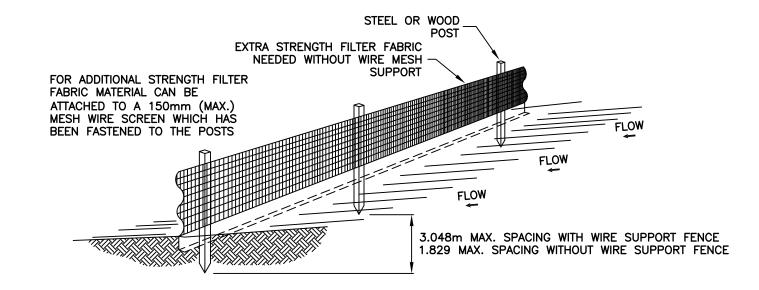






2 LEACHATE COLLECTION PIPING DETAIL
7 SCALE: 1:50

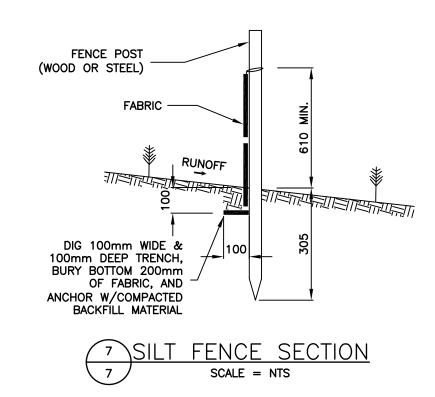


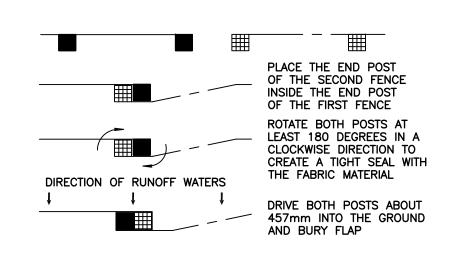


#### NOTES

- 1. THE HEIGHT OF A SILT FENCE SHALL NOT EXCEED 914mm.
- 2. THE FILTER FABRIC SHALL BE PURCHASED IN A CONTINUOUS ROLL CUT TO THE LENGTH OF
- 3. POSTS SHALL BE SPACED A MAXIMUM OF 3.048m APART AT THE BARRIER LOCATION AND DRIVEN SECURELY INTO THE GROUND A MINIMUM OF 300mm. WHEN EXTRA STRENGTH FABRIC IS USED WITHOUT THE WIRE SUPPORT FENCE, POST SPACING SHALL NOT EXCEED 1.829m.
- 4. A TRENCH SHALL BE EXCAVATED APPROXIMATELY 100mm WIDE AND 100mm DEEP ALONG THE LINE OF POSTS AND UPSLOPE FROM THE BARRIER.
- 5. WHEN STANDARD STRENGTH FILTER FABRIC IS USED, A WIRE MESH SUPPORT FENCE SHALL BE FASTENED SECURELY TO THE UPSLOPE SIDE OF THE POSTS USING HEAVY DUTY WIRE STAPLES AT LEAST 25mm LONG, TIE WIRES, OR HOG RINGS. THE WIRE SHALL EXTEND INTO THE TRENCH A MINIMUM OF 50mm AND SHALL NOT EXTEND MORE THAN 914mm ABOVE THE ORIGINAL GROUND SURFACE.
- 6. THE STANDARD STRENGTH FILTER FABRIC SHALL BE STAPLED OR WIRED TO THE FENCE, AND 200mm OF THE FABRIC SHALL BE EXTENDED INTO THE TRENCH. THE FABRIC SHALL NOT EXTEND MORE THAN 914mm ABOVE THE ORIGINAL GROUND SURFACE.
- 7. THE TRENCH SHALL BE BACKFILLED AND THE SOIL COMPACTED OVER THE FILTER FABRIC.
- SILT FENCING TO BE POLYPROPYLENE SYNTHETIC FIBRE WITH ULTRAVIOLET STABILIZERS. AMOCO 1198 OR APPROVED EQUAL.
- 9. WOOD POSTS TO BE 38mm X 89mm (2" X 4"), POINTED AT ONE END AND FABRICATED.
- 10. INSTALL ALL SUPPORTING POSTS ON THE DOWN SLOPE SIDE OF THE FENCING
- 11. MAINTAIN SILT FENCE THROUGHOUT CONSTRUCTION AND UNTIL REVEGETATION OCCURS.









# **Record Drawing**

Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent verification required before application.

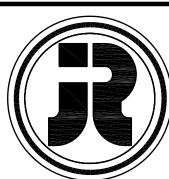
				B.M. EL.	
				LOCATIONS OF UNDERGROUND STRUCTURES/UTILITIES AS SHOWN ARE BASED ON AVAILABLE INFORMATION BUT NO	
				GUARANTEE IS GIVEN OR IMPLIED THAT ALL EXISTING	
				UNDERGROUND STRUCTURES/UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION	
1	RECORD DRAWING	13/10/16	ОТ	OF EXISTENCE AND EXACT LOCATION OF ALL	
No	REVISIONS	DATE		UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR, BEFORE PROCEEDING WITH CONSTRUCTION.	

Certificate of Authorization

J.R. Cousin Consultants Ltd.

No. 234 Date: 13/07/02

ORIGINAL DRAWING
SIGNED AND SEALED
BY
G.R. COUSIN
13/07/02



# J. R. Cousin Consultants Ltd. Consulting Engineers and Project Managers Code: M-61 DESIGNED

91A Scurfield Blvd. Winn ph: (204) 489-0474 fax: (204) 489-0474 websi

Engineering Excellence since 1981

Winnipeg, MB R3Y 1G4 fax: (204) 489-0487 website: www.jrcc.ca

v.jrcc.ca	ВМ	
	REVIEWED BY:	ŀ
	IC.	

17.02	PROJECT: LGD OF MYSTERY LAKE WASTE DISPOSAL GROUND PHASE II WORKS
D BY:	TITLE:
JC	ACTIVE CELL DIKES, CONTAMINATED

JC ACTIVE CELL DIKES, CONTAMINATED SOIL DIKES LEACHATE COLLECTION PIPING, PIPE END

MARKER AND SILT FENCE DETAILS

CALE: DATE: PLAN: SHEET:

AS NOTED 13/06/12 7 7 of 7



# LGD OF MYSTERY LAKE

# WASTE DISPOSAL GROUND REVISED PHASE III WORKS

Record Drawing

Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent verification required before application.

# PLAN INDEX

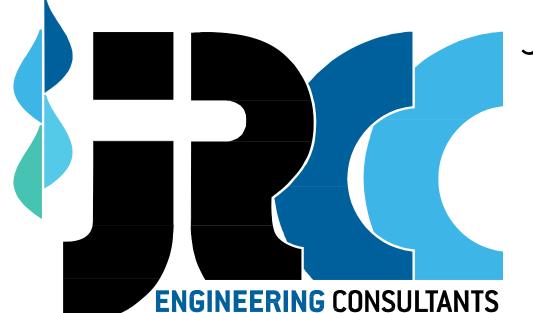
PLAN 1. DRAWING LEGEND, ABBREVIATION INDEX AND KEY PLAN

PLAN 2. EXISTING WDG LAYOUT AFTER PHASE II WORKS WITH TEST HOLE LOCATIONS

PLAN 3. OVERALL WDG LAYOUT SHOWING PROPOSED PHASE III WORKS

PLAN 4. PHASE III ACTIVE CELL AREA LAYOUT

PLAN 5. ACTIVE CELL DIKES, LEACHATE COLLECTION PIPING AND SILT FENCE DETAILS



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REDUCED DRAWING SET DO NOT SCALE

### DRAWING LEGEND:

<u>IPING:</u>		ROADS AND	DRAINAGE:	<u>MISCELLAN</u>	<u>-005:</u>
	EXISTING WATERMAIN PROPOSED WATERMAIN FUTURE WATERMAIN		EXISTING ROAD CENTERLINE PROPOSED ROAD CENTERLINE FUTURE ROAD CENTERLINE		EXISTING FENCE LINE PROPOSED FENCE LINE
	EXISTING SEWERMAIN			—P—P—	EXISTING PROPANE LINE
	PROPOSED SEWERMAIN FUTURE SEWERMAIN		EXISTING ROAD SHOULDER PROPOSED ROAD SHOULDER	—P—P—	PROPOSED PROPANE LII
			EXISTING ROAD EDGE	—н—н— <b>—н—н—</b>	EXISTING HYDRO LINE PROPOSED HYDRO LINE
	EXISTING FORCEMAIN PROPOSED FORCEMAIN FUTURE FORCEMAIN		PROPOSED ROAD EDGE FUTURE ROAD EDGE	—	EXISTING GAS LINE
	EXISTING RAW WATERMAIN		EXISTING SIDEWALK PROPOSED SIDEWALK	——MTS——	EXISTING MTS LINE
	PROPOSED RAW WATERMAIN FUTURE RAW WATERMAIN		EXISTING DITCH PROPOSED DITCH		EXISTING BUILDING PROPOSED BUILDING
	EXISTING LAND DRAINAGE SEWER PROPOSED LAND DRAINAGE SEWER				LEGAL/LOT LINE
	FUTURE LAND DRAINAGE SEWER		EXISTING CULVERT	++++++++	RAILWAY LINE
FH ∳-	EXISTING FIRE HYDRANT		PROPOSED CULVERT		MATCH LINE
FH.	PROPOSED FIRE HYDRANT	<b>4</b>	EXISTING DRAINAGE DIRECTION	H₽	EXISTING HYDRO POLE
⊗	EXISTING VALVE	<b>~~~</b>	PROPOSED DRAINAGE DIRECTION	HP	PROPOSED HYDRO POLE
⊗	PROPOSED VALVE	<u></u>	CONTOURS - MAJOR INTERVALS	(W)	WATER HOLDING TANK
co	EXISTING CLEANOUT	100.5	CONTOURS - MINOR INTERVALS	<u> </u>	SEPTIC TANK
00_	PROPOSED CLEANOUT	×100.00	EXISTING GROUND ELEVATION	$\oplus$	SEWAGE HOLDING TANK
IH _O	EXISTING MANHOLE	100.00	PROPOSED GROUND ELEVATION	₩ #	SURVEY BAR
MH	PROPOSED MANHOLE	100.00	EXISTING ROAD ELEVATION	₩ �	SURVEY MONUMENT/BEN
ර ර	EXISTING CURBSTOP	100.00	PROPOSED ROAD ELEVATION	<b>V</b>	EXISTING VEGETATION
•	PROPOSED CURBSTOP	TOP	EXISTING SLOPE	$\sim\sim$	PROPOSED VEGETATION
СВ	EXISTING CATCH BASIN	воттом тор		<b>(D1)</b>	DOOR CONSTRUCTION T
СВ	PROPOSED CATCH BASIN	воттом	PROPOSED SLOPE	w ₁	WALL CONSTRUCTION TY
			ASPHALT		EASEMENT

### **ABBREVIATIONS:**

DRIVE

DRAWING

DWG

<b>©</b>	AT	Ε	EAST	JCT	JUNCTION	RAD	RADIUS
A/C	AIR CONDITIONING	EC	END OF CURVE	JP	JOCKEY PUMP	RD	ROAD
ALUM	ALUMINUM	EL	ELEVATION			REV	REVISION
ASPH	ASPHALT	ELEC	ELECTRICAL	LAB	LABORATORY	ROW	RIGHT OF WAY
AVE	AVENUE	EP	EDGE OF PAVEMENT	LAM	LAMINATE	RM	ROOM
AVG	AVERAGE	ER	EDGE OF ROAD	LAT	LATITUDE		
		E/W	EACHWAY	LDS	LAND DRAINAGE SEWER	S	SOUTH
BD	BOTTOM OF DITCH	ÉXT	EXTERIOR	LFS	LEVEL FLOAT SWITCH	SCH	SCHEDULE
BLDG	BUILDING			LONG	LONGITUDE	SECT	SECTION
BLVD	BOULEVARD	FAX	FAX MACHINE STAND	LWL	LOW WATER LEVEL	SHT	SHEET
ВМ	BENCHMARK	FC	FILE CABINET			SIB	STEEL IRON BAR
BOT	воттом	FD	FLOOR DRAIN	М	METRE	SPEC	SPECIFICATION
BP	BACKWASH PUMP	F/F	FACE TO FACE	MAX	MAXIMUM	SQ	SQUARE
B/W	BOTHWAYS	FH	FIRE HYDRANT	MCC	MOTOR CONTROL CENTER	SSL	SEWER SERVICE LINE
<b>-/</b>	20	FM	FORCEMAIN	MECH	MECHANICAL	ST	STREET
		FP	FIRE PUMP	MEMB	MEMBRANE	STD	STANDARD
CB	CATCH BASIN	FT	FOOT, FEET	MH	MANHOLE	SUSP	SUSPENDED
CI	CAST IRON		, , , , , , , , , , , , , , , , , , , ,	MIN	MINIMUM	SW	SIDEWALK
CHKD	CHECKED	GA	GAUGE	MM	MILLIMETRE		
CNR	CANADIAN NATIONAL RAILWAY	GALV	GALVANIZED			TEL	TELEPHONE
CO	CLEANOUT	5		N	NORTH	TEMP	TEMPORARY
COL	COLUMN	HA	HECTARE	NAT	NATURAL	TP	TRUCKFILL PUMP
CONC	CONCRETE	НВ	HOSE BIBB	NBC	NATIONAL BUILDING CODE	TYP	TYPICAL
CONST	CONSTRUCTION	HDPE	HIGH DENSITY POLYETHYLENE	NTS	NOT TO SCALE		
CONT	CONTINUOUS	HI	HEIGHT OF INSTRUMENT	NWL	NORMAL WATER LEVEL	VERT	VERTICAL
COORD	COORDINATE	HPW	HIGH PRESSURE WATER LINE			VOL	VOLUME
CPR	CANADIAN PACIFIC RAILWAY	HORIZ	HORIZONTAL	0/C	ON CENTRE		
C/W	COMPLETE WITH	HP	HYDRO POLE	O/D	OUTSIDE DIAMETER	US	ULTRASONICS TRANSDUCER
•		HR	HOUR	0/F	OUTSIDE FACE		
DCW	DOMESTIC COLD WATER	HVAC	HEATING, VENTILATING AND	0/H	OVER HEAD	VAR	VARIES
DEG	DEGREE		AIR CONDITIONING	OD	OUTSIDE DIAMETER	VB	VAPOUR BARRIER
DHW	DOMESTIC HOT WATER	HW	HOT WATER TANK	ORIG	ORIGINAL	VERT	VERTICAL
DIA	DIAMETER	HWL	HIGH WATER LEVEL	OWSJ	OPEN WEB STEEL JOIST	VFD	VARIABLE FREQUENCY DRIVE
DIM	DIMENSION	2	THOSE WATER LEVEL	OWSU	OPEN WEB STEEL JUIST		
DIST	DISTANCE	ID	INSIDE DIAMETER	DIXWD	BLYMOOD	W	WEST
DN	DOWN	IL	ICE LEVEL	PLYWD POLY	PLYWOOD POLYETHYLENE	w/o	WITHOUT
DP	DUTY PUMP	INCL	INCLUDE			WL	WATER LEVEL
DR	DRIVE	INT	INTERIOR	PROP	PROPERTY	WM	WATERMAIN

INTERIOR

INVERT

REVISIONS

PRESSURE SEWER

POLY VINYL CHLORIDE

DECIMALIZED NUMBERS INDICATE METRES. WHOLE NUMBERS INDICATE MILLIMETRES.





B.M. EL. LOCATIONS OF UNDERGROUND STRUCTURES/UTILITIES AS SHOWN ARE BASED ON AVAILABLE INFORMATION BUT NO GUARANTEE IS GIVEN OR IMPLIED THAT ALL EXISTING UNDERGROUND STRUCTURES/UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION OF EXISTENCE AND EXACT LOCATION OF ALL UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR, BEFORE PROCEEDING WITH CONSTRUCTION. RECORD DRAWING OCT/14

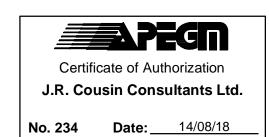
WATER SERVICE LINE

WASTEWATER SEWER

WATERMAIN

WEIGHT

WM WSL WWS WT



ENGINEER'S SEAL ORIGINAL DRAWING SIGNED AND SEALED BY G. R. COUSIN 14/08/18

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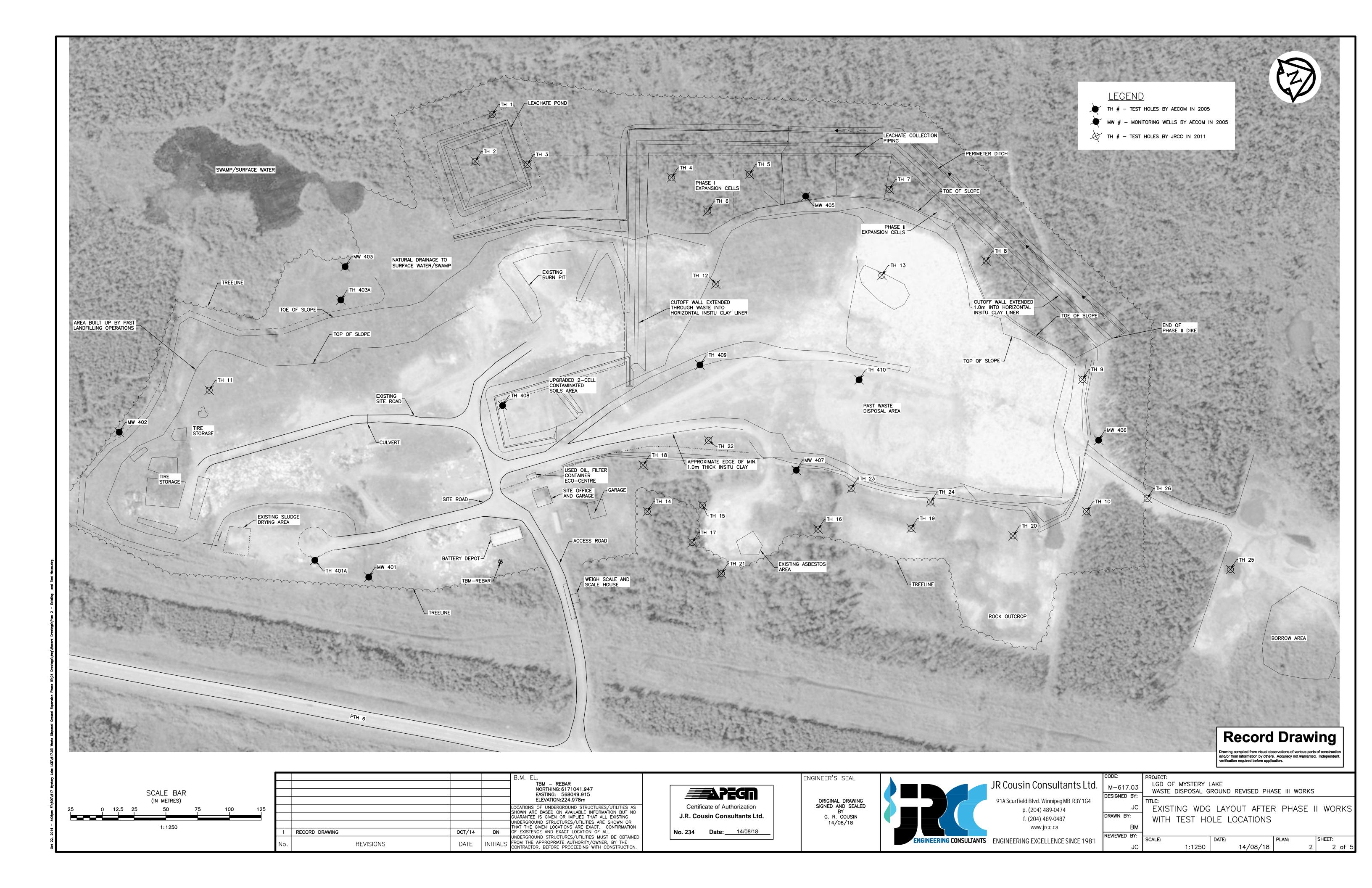
LGD OF MYSTERY LAKE
WASTE DISPOSAL GROUND REVISED PHASE III WORKS DESIGNED BY: AND KEY PLAN

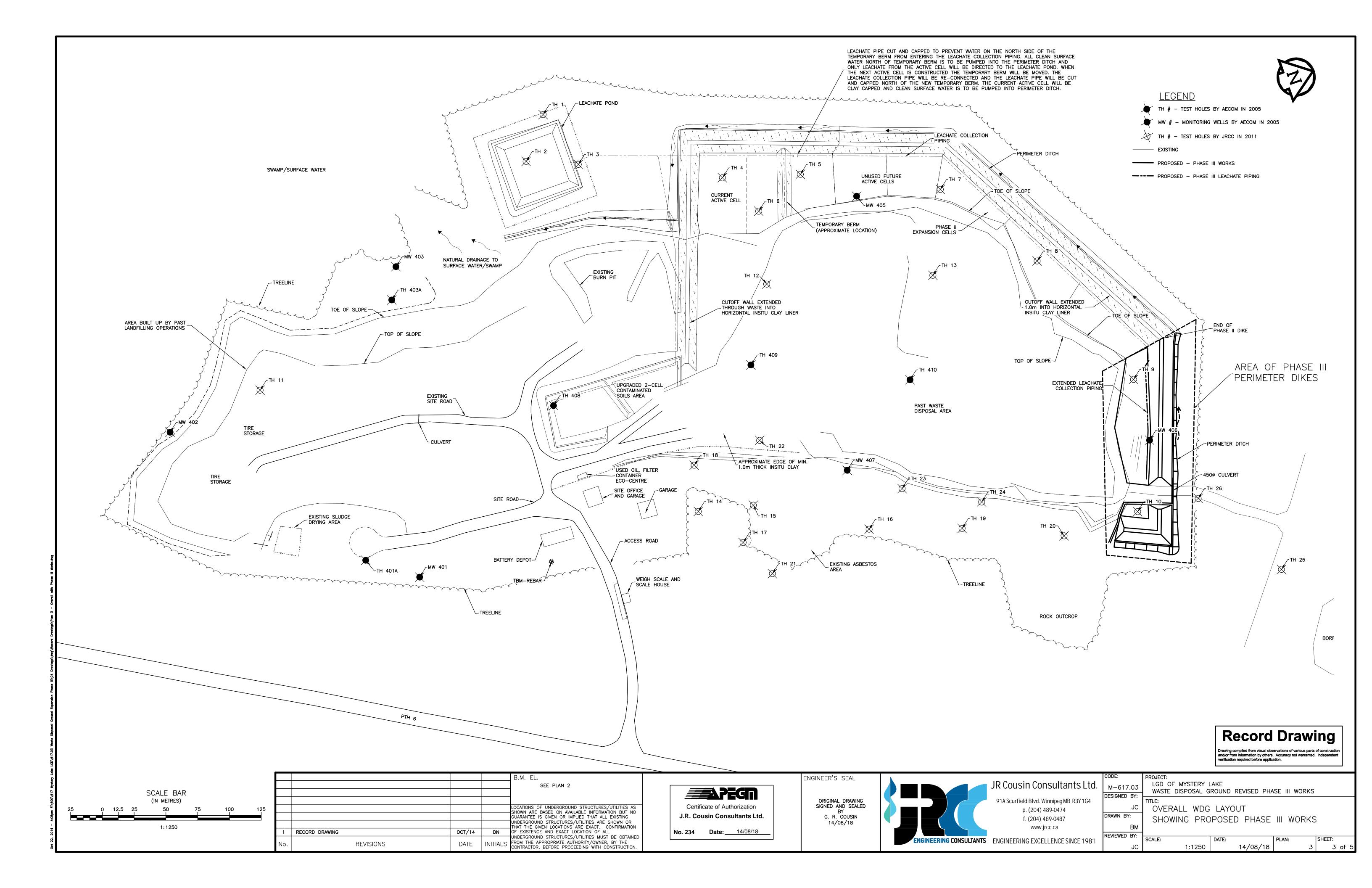
LGD OF MYSTERY LAKE WDG

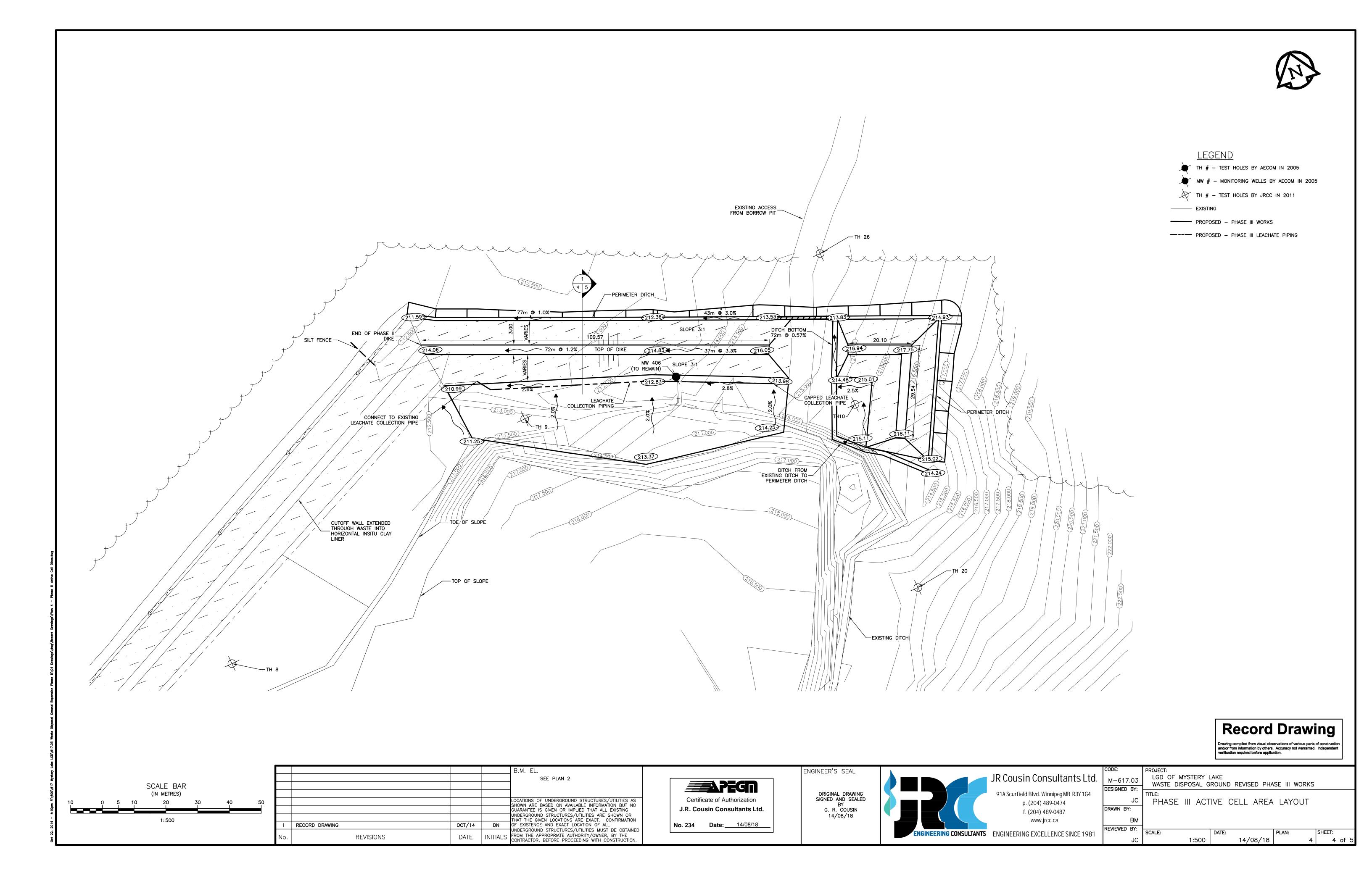
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DRAWING LEGEND, ABBREVIATION INDEX REVIEWED BY: 14/08/18

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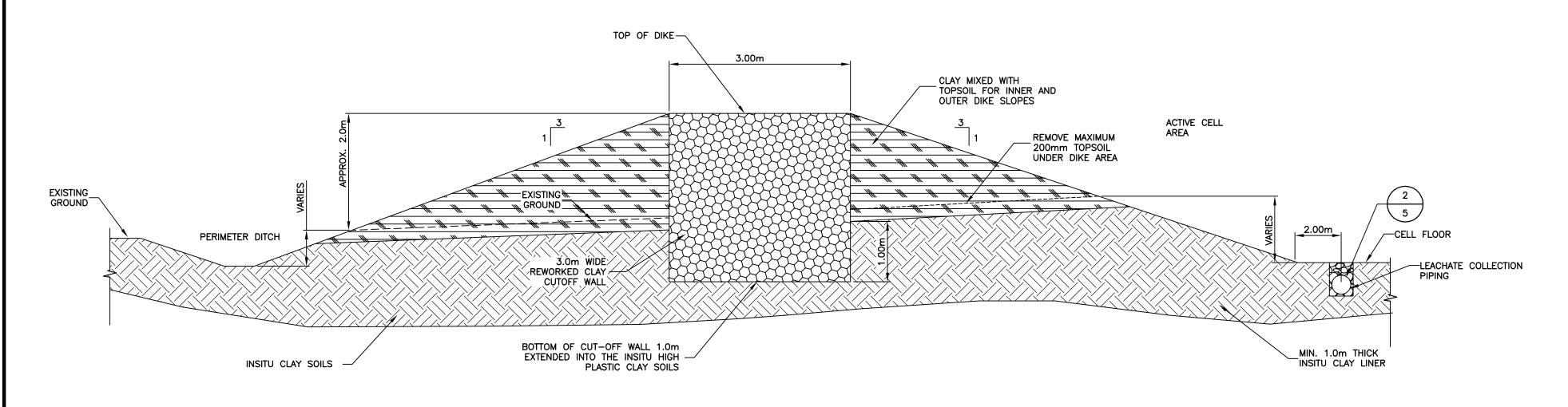
EXCAVATED AND COMPACTED

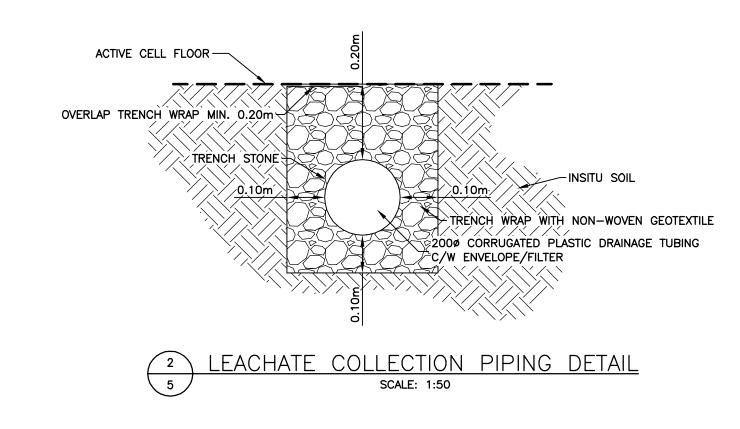
MEDIUM-HIGH PLASTIC CLAY CLAY MIXED WITH CLEAN

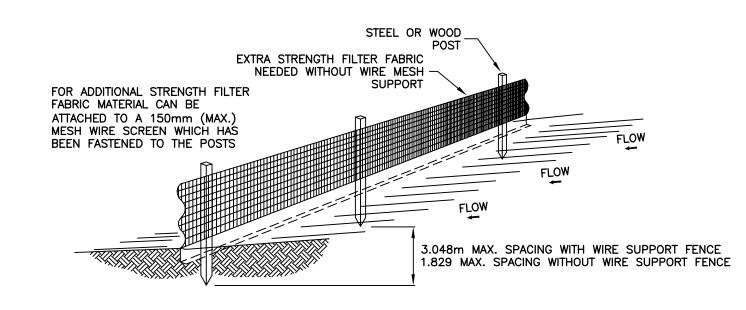
TOPSOIL/PEAT

INSITU SOIL

STONE



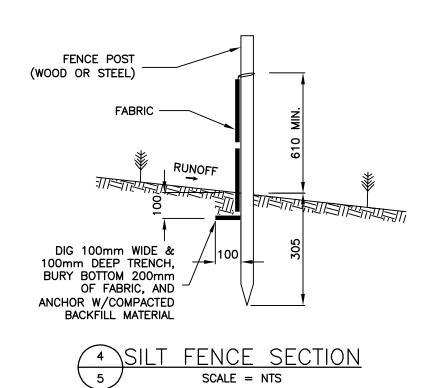


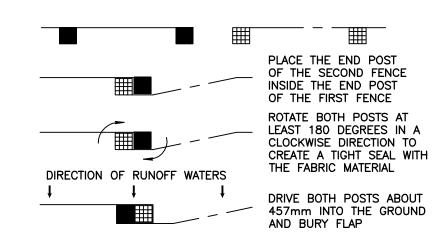


- 1. THE HEIGHT OF A SILT FENCE SHALL NOT EXCEED 914mm.
- 2. THE FILTER FABRIC SHALL BE PURCHASED IN A CONTINUOUS ROLL CUT TO THE LENGTH OF THE BARRIER TO AVOID THE USE OF JOINTS.
- 3. POSTS SHALL BE SPACED A MAXIMUM OF 3.048m APART AT THE BARRIER LOCATION AND DRIVEN SECURELY INTO THE GROUND A MINIMUM OF 300mm. WHEN EXTRA STRENGTH FABRIC IS USED WITHOUT THE WIRE SUPPORT FENCE, POST SPACING SHALL NOT EXCEED 1.829m.
- 4. A TRENCH SHALL BE EXCAVATED APPROXIMATELY 100mm WIDE AND 100mm DEEP ALONG THE LINE OF POSTS AND UPSLOPE FROM THE BARRIER.
- 5. WHEN STANDARD STRENGTH FILTER FABRIC IS USED, A WIRE MESH SUPPORT FENCE SHALL BE FASTENED SECURELY TO THE UPSLOPE SIDE OF THE POSTS USING HEAVY DUTY WIRE STAPLES AT LEAST 25mm LONG, TIE WIRES, OR HOG RINGS. THE WIRE SHALL EXTEND INTO THE TRENCH A MINIMUM OF 50mm AND SHALL NOT EXTEND MORE THAN 914mm ABOVE THE ORIGINAL GROUND SURFACE.
- 6. THE STANDARD STRENGTH FILTER FABRIC SHALL BE STAPLED OR WIRED TO THE FENCE, AND 200mm OF THE FABRIC SHALL BE EXTENDED INTO THE TRENCH. THE FABRIC SHALL NOT EXTEND MORE THAN 914mm ABOVE THE ORIGINAL GROUND SURFACE.
- 7. THE TRENCH SHALL BE BACKFILLED AND THE SOIL COMPACTED OVER THE FILTER FABRIC.
- 8. SILT FENCING TO BE POLYPROPYLENE SYNTHETIC FIBRE WITH ULTRAVIOLET STABILIZERS. AMOCO 1198 OR APPROVED EQUAL.
- 9. WOOD POSTS TO BE 38mm X 89mm (2" X 4"), POINTED AT ONE END AND FABRICATED.
- 10. INSTALL ALL SUPPORTING POSTS ON THE DOWN SLOPE SIDE OF THE FENCING
- 11. MAINTAIN SILT FENCE THROUGHOUT CONSTRUCTION AND UNTIL REVEGETATION OCCURS.



ENGINEER'S SEAL







# **Record Drawing** Drawing compiled from visual observations of various parts of construction and/or from information by others. Accuracy not warranted. Independent verification required before application.

14/08/18

				B.M. EL.
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1	RECORD DRAWING	OCT/14	DN	OF EXISTENCE AND EXACT LOCATION OF ALL
No.	REVISIONS	DATE	PIAITIAI	UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR, BEFORE PROCEEDING WITH CONSTRUCTION.

Certificate of Authorization J.R. Cousin Consultants Ltd. No. 234 Date: 14/08/18

ORIGINAL DRAWING SIGNED AND SEALED BY G. R. COUSIN 14/08/18

1	EN	GINEE	RING C	ONSUL	TANTS

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JR Cousin Consultants Ltd.	M-61
91A Scurfield Blvd. Winnipeg MB R3Y 1G4	DESIGNE
p. (204) 489-0474	
f. (204) 489-0487	DRAWN E
www.jrcc.ca	
ENGINEERING EXCELLENCE SINCE 1981	REVIEWE

CODE:	PROJECT:
M-617.03	LGD OF MYSTERY LAKE WASTE DISPOSAL GROUND REVISED PHASE III WORKS
DESIGNED BY:	WHOTE BISI GOVE CINCOUND INEVIOLED IT INCC. III WORKING
	TITLE:
JC	ACTIVE CELL DIKES, LECHATE COLLECTION
DRAWN BY:	PIPING AND SILT FENCE DETAILS
	FIFING AND SILI FENCE DETAILS
OT	

AS NOTED



# LGD OF MYSTERY LAKE

# WASTE DISPOSAL GROUND PHASE IV WORKS

ISSUED FOR **TENDER** 

# PLAN INDEX

DRAWING LEGEND, ABBREVIATION INDEX AND KEY PLAN

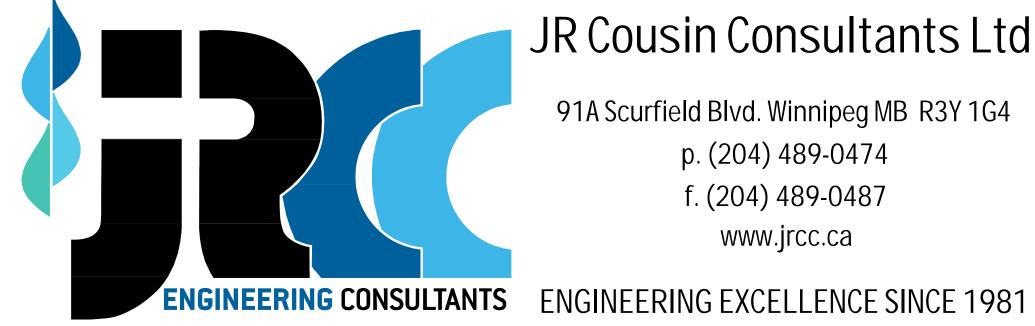
EXISTING WDG LAYOUT AFTER PHASE III WORKS WITH TEST HOLE LOCATIONS

OVERALL WDG LAYOUT SHOWING PROPOSED PHASE IV WORKS

PHASE IV PERIMETER DIKE LAYOUT

PERIMETER DIKE, MOVEABLE CHAIN LINK FENCE, LEACHATE COLLECTION PIPING

AND SILT FENCE DETAILS



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REDUCED DRAWING SET DO NOT SCALE

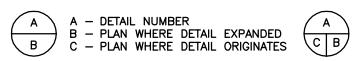
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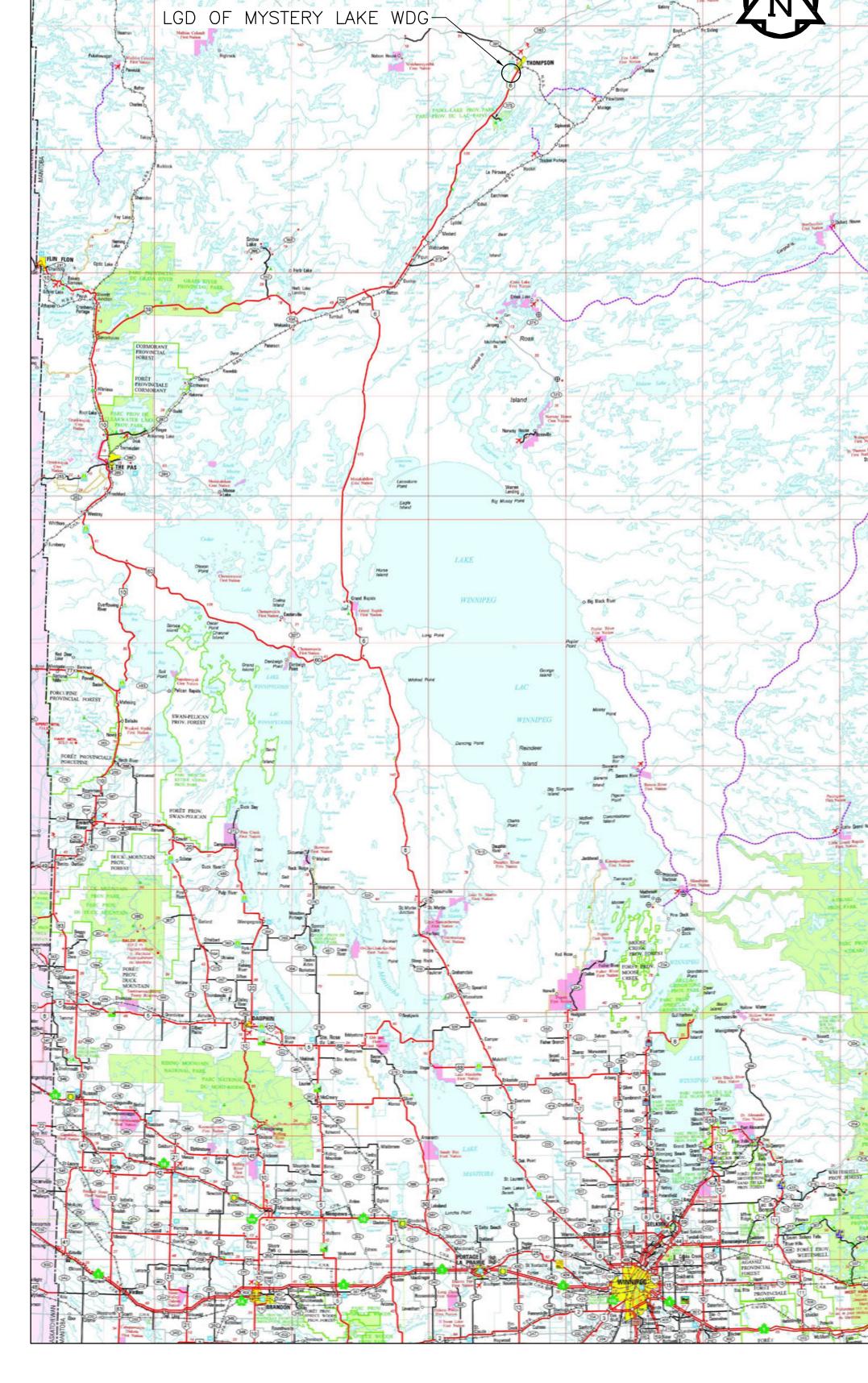
			ASPHALT		EASEMENT
CB	PROPOSED CATCH BASIN	воттом	PROPOSED SLOPE	W1	WALL CONSTRUCTION TYPE
СВ	EXISTING CATCH BASIN	BOTTOM TOP	DDODOGED CLODE	<b>(D1)</b>	DOOR CONSTRUCTION TYPE
Ğ	PROPOSED CURBSTOP	TOP	EXISTING SLOPE	$\sim\sim$	PROPOSED VEGETATION
ð	EXISTING CURBSTOP	(100.00)	PROPOSED ROAD ELEVATION	$\sim\sim$	EXISTING VEGETATION
MH	PROPOSED MANHOLE	(100.00)	EXISTING ROAD ELEVATION	<b>•</b>	SURVEY MONUMENT/BENCHMAR
MH _O	EXISTING MANHOLE	(100.00)	PROPOSED GROUND ELEVATION	<del>-</del>	SURVEY BAR
CO	PROPOSED CLEANOUT	×100.00	EXISTING GROUND ELEVATION	$\oplus$	SEWAGE HOLDING TANK
co	EXISTING CLEANOUT	— _{100.5}	CONTOURS - MINOR INTERVALS	<u>s</u>	SEPTIC TANK
8	PROPOSED VALVE	<u></u>	CONTOURS - MAJOR INTERVALS	W	WATER HOLDING TANK
$\otimes$	EXISTING VALVE		PROPOSED DRAINAGE DIRECTION	HP	PROPOSED HYDRO POLE
FH +	PROPOSED FIRE HYDRANT	<b>4</b>	EXISTING DRAINAGE DIRECTION	HP	EXISTING HYDRO POLE
FH - <b>수</b> -	EXISTING FIRE HYDRANT		PROPOSED CULVERT		MATCH LINE
	PROPOSED LAND DRAINAGE SEWER FUTURE LAND DRAINAGE SEWER		EXISTING CULVERT	+++++++	RAILWAY LINE
	EXISTING LAND DRAINAGE SEWER		PROPOSED DITCH		LEGAL/LOT LINE
	PROPOSED RAW WATERMAIN FUTURE RAW WATERMAIN		EXISTING DITCH		EXISTING BUILDING PROPOSED BUILDING
	EXISTING RAW WATERMAIN		EXISTING SIDEWALK PROPOSED SIDEWALK	——MTS——	EXISTING MTS LINE
	PROPOSED FORCEMAIN FUTURE FORCEMAIN		FUTURE ROAD EDGE	—G—G—-	EXISTING GAS LINE
	EXISTING FORCEMAIN		EXISTING ROAD EDGE PROPOSED ROAD EDGE	—н—н— <b>—н—н—</b>	EXISTING HYDRO LINE PROPOSED HYDRO LINE
	EXISTING SEWERMAIN PROPOSED SEWERMAIN FUTURE SEWERMAIN		EXISTING ROAD SHOULDER PROPOSED ROAD SHOULDER	—P—P—	PROPOSED PROPANE LINE
	FUTURE WATERMAIN		FUTURE ROAD CENTERLINE	—P—P—	EXISTING PROPANE LINE
	EXISTING WATERMAIN PROPOSED WATERMAIN	<u>-</u> -	EXISTING ROAD CENTERLINE PROPOSED ROAD CENTERLINE	<del></del>	EXISTING FENCE LINE PROPOSED FENCE LINE
<u>PIPING:</u>		RUADS ANI	D DRAINAGE:	<u>MISCELLAN</u>	<u> </u>

# ABBREVIATIONS:

0	AT	Ε	EAST	JCT	JUNCTION	RAD	RADIUS
A/C	AIR CONDITIONING	EC	END OF CURVE	JP	JOCKEY PUMP	RD	ROAD
ÁLUM	ALUMINUM	EL	ELEVATION			REV	REVISION
ASPH	ASPHALT	ELEC	ELECTRICAL	LAB	LABORATORY	ROW	RIGHT OF WAY
AVE	AVENUE	EP	EDGE OF PAVEMENT	LAM	LAMINATE	RM	ROOM
AVG	AVERAGE	ER	EDGE OF ROAD	LAT	LATITUDE		
		E/W	EACHWAY	LDS	LAND DRAINAGE SEWER	S	SOUTH
BD	BOTTOM OF DITCH	EXT	EXTERIOR	LFS	LEVEL FLOAT SWITCH	SCH	SCHEDULE
BLDG	BUILDING			LONG	LONGITUDE	SECT	SECTION
BLVD	BOULEVARD	FAX	FAX MACHINE STAND	LWL	LOW WATER LEVEL	SHT	SHEET
ВМ	BENCHMARK	FC	FILE CABINET			SIB	STEEL IRON BAR
BOT	воттом	FD	FLOOR DRAIN	М	METRE	SPEC	SPECIFICATION
BP	BACKWASH PUMP	F/F	FACE TO FACE	MAX	MAXIMUM	SQ	SQUARE
B/W	BOTHWAYS	FH	FIRE HYDRANT	MCC	MOTOR CONTROL CENTER	SSL	SEWER SERVICE LINE
-,		FM	FORCEMAIN	MECH	MECHANICAL	ST	STREET
		FP	FIRE PUMP	MEMB	MEMBRANE	STD	STANDARD
CB	CATCH BASIN	FT	FOOT, FEET	MH	MANHOLE	SUSP	SUSPENDED
CI	CAST IRON			MIN	MINIMUM	SW	SIDEWALK
CHKD	CHECKED	GA	GAUGE	MM	MILLIMETRE		
CNR	CANADIAN NATIONAL RAILWAY	GALV	GALVANIZED			TEL	TELEPHONE
CO	CLEANOUT	J. 1_1		N	NORTH	TEMP	TEMPORARY
COL	COLUMN	HA	HECTARE	NAT	NATURAL	TP	TRUCKFILL PUMP
CONC	CONCRETE	НВ	HOSE BIBB	NBC	NATIONAL BUILDING CODE	TYP	TYPICAL
CONST	CONSTRUCTION	HDPE	HIGH DENSITY POLYETHYLENE	NTS	NOT TO SCALE		
CONT	CONTINUOUS	HI	HEIGHT OF INSTRUMENT	NWL	NORMAL WATER LEVEL	VERT	VERTICAL
COORD	COORDINATE	HPW	HIGH PRESSURE WATER LINE			VOL	VOLUME
CPR	CANADIAN PACIFIC RAILWAY	HORIZ	HORIZONTAL	0/C	ON CENTRE		
C/W	COMPLETE WITH	HP	HYDRO POLE	O/D	OUTSIDE DIAMETER	US	ULTRASONICS TRANSDUCER
		HR	HOUR	O/F	OUTSIDE FACE		
DCW	DOMESTIC COLD WATER	HVAC	HEATING, VENTILATING AND	0/H	OVER HEAD	VAR	VARIES
DEG	DEGREE		AIR CONDITIONING	OD	OUTSIDE DIAMETER	VB	VAPOUR BARRIER
DHW	DOMESTIC HOT WATER	HW	HOT WATER TANK	ORIG	ORIGINAL	VERT	VERTICAL
DIA	DIAMETER	HWL	HIGH WATER LEVEL	OWSJ	OPEN WEB STEEL JOIST	VFD	VARIABLE FREQUENCY DRIVE
DIM	DIMENSION			01130	OF LIN WEB STEEL BOIST		
DIST	DISTANCE	ID	INSIDE DIAMETER	PLYWD	PLYWOOD	W	WEST
DN	DOWN	iL	ICE LEVEL	POLY	POLYETHYLENE	W/O	WITHOUT
DP	DUTY PUMP	INCL	INCLUDE	PROP	PROPERTY	wĹ	WATER LEVEL
DR	DRIVE	INT	INTERIOR	PS PS	PRESSURE SEWER	WM	WATERMAIN
DWG	DRAWING	INV	INVERT	PVC	POLY VINYL CHLORIDE	WSL	WATER SERVICE LINE
		,,,,,		770	FOLI VIINIL CHLORIDE	WWC	WACTEWATER CEWER

DECIMALIZED NUMBERS INDICATE METRES. WHOLE NUMBERS INDICATE MILLIMETRES.





				B.M. EL.	
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				LOCATIONS OF UNDERGROUND STRUCTURES/UTILITIES AS SHOWN ARE BASED ON AVAILABLE INFORMATION BUT NO	l
				GUARANTEE IS GIVEN OR IMPLIED THAT ALL EXISTING	l
				UNDERGROUND STRUCTURES/UTILITIES ARE SHOWN OR THAT THE GIVEN LOCATIONS ARE EXACT. CONFIRMATION	l
				OF EXISTENCE AND EXACT LOCATION OF ALL	l
No.	REVISIONS	DATE	PIAITIMI	UNDERGROUND STRUCTURES/UTILITIES MUST BE OBTAINED FROM THE APPROPRIATE AUTHORITY/OWNER, BY THE CONTRACTOR. BEFORE PROCEEDING WITH CONSTRUCTION.	

WATER SERVICE LINE WASTEWATER SEWER WEIGHT







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CODE:	PROJECT:
M-617.04	LGD OF MYSTERY LAKE WASTE DISPOSAL GROUND PHASE IV WORKS
DESIGNED BY:	TITLE:
JC	DRAWING LEGEND, ABBREVIATION INDEX
DRAWN BY:	AND KEY PLAN
ВМ	
REVIEWED BY:	SCALE: DATE: PLAN: SHEET:
JC	NTS 15/07/07 1 1 of 5

