

PROPOSED GOODLANDS UNIT NO. 3

Application for Enhanced Oil Recovery Waterflood Project

Lower Amaranth Formation

Lower Amaranth I Pool (03 29I)

Waskada Field, Manitoba

October 28, 2016
Tundra Oil and Gas Partnership

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INTRODUCTION

The Waskada Oil Field is located in Townships 1 and 2, Ranges 23-26 W1 (Figure 1). The Waskada Lower Amaranth Oil pool was discovered in June 1980 when Omega Hydrocarbons recompleted a former Mississippian producer in the stratigraphically higher Lower Member of the Amaranth Formation. Secondary recovery through waterflood has been initiated throughout much of the pool. Tundra Oil and Gas (Tundra) currently operates Waskada Lower Amaranth Unit 1, 2, 3, 4, 5, 6, 7, 8, 13, 14, 15, 16, 17, 18 and 19.

In the eastern part of the Waskada field, potential exists for incremental production and reserves from a Waterflood EOR project in the Lower Amaranth oil reservoirs. The following represents an application by Tundra to establish Goodlands Unit No. 3 (LSDs 1-14 Section 9, LSDs 1-6, 11-14 Section 10, LSDs 3-4 Section 11, LSDs 5-6, 11-16 Section 14 and LSDs 3-16 Section 15-001-24W1) and implement a Secondary Waterflood (WF) EOR scheme within the Lower Amaranth Formation as outlined on Figure 2.

The proposed project area falls within the existing designated 03-29A Lower Amaranth A Pool and 03-29I Lower Amaranth I Pool of the Waskada Oilfield (Figure 3).

SUMMARY

1. The proposed Goodlands Unit No. 3 will include 74 horizontal wells, 3 deviated wells and 35 vertical wells within 50 Legal Sub Divisions (LSD) of the Lower Amaranth producing reservoir. The project is located west of Goodlands Unit No. 1 (Figure 2).
2. Total Net Original Oil in Place (OOIP) in Goodlands Unit No. 3 has been calculated to be **6,130 e³m³** (38,559 Mbbbl) for an average of **122.6 net e³m³** (771.2 Mbbbl) OOIP per 40 acre LSD.
3. Cumulative allocated production to the end of July 2016 from the 112 wells within the proposed Goodlands Unit No. 3 project area was **473.6 e³m³** (2,979 Mbbbl) of oil, and **950.1 e³m³** (5,976 Mbbbl) of water, representing a **7.7% Recovery Factor (RF)** of the Net OOIP.
4. Estimated Ultimate Recovery (EUR) of Primary Proved Producing oil reserves in the proposed Goodlands Unit No. 3 project area has been calculated to be **597.1 e³m³** (3,757 Mbbbl), with **123.4 e³m³** (776.6 Mbbbl) remaining as of the end of July 2016.
5. Ultimate oil recovery of the proposed Goodlands Unit No. 3 OOIP, under the current Primary Production method, is forecasted to be **9.7%**.
6. The production from the Goodlands Unit No. 3 peaked in September 2013 at 299.8 m³ (OPD) as shown in Figure 4. As of July 2016, production was 64.0 m³ OPD, 396.9 m³ of water per day (WPD) and an 86.1% watercut.
7. In September 2013, production averaged 3.5 m³ OPD per well in Goodlands Unit No. 3. As of July 2016, average per well production has declined to 0.9 m³ OPD. Decline analysis of the group primary production data forecasts total oil to continue declining at an annual rate of approximately **30.0%** in the project area.
8. Estimated Ultimate Recovery (EUR) of proved oil reserves under Secondary WF EOR for the proposed Goodlands Unit No. 3 has been calculated to be **799.9 e³m³** (**5,033 Mbbbl**), with **326.3 e³m³** (**2,052 Mbbbl**) remaining. An incremental **202.8 e³m³** (**1,275 Mbbbl**) of proved oil reserves, or **3.3%**, are forecasted to be recovered under the proposed Unitization and Secondary EOR production vs the existing Primary Production method.
9. Total RF under Secondary EOR WF in the proposed Goodlands Unit No. 3 is estimated to be **13.0%**.
10. Based on the waterflood response in the adjacent main portion of the Waskada field, the Lower Amaranth Formation in the proposed project area is believed to be a suitable reservoir for WF EOR operations.
11. Existing horizontal wells, with multi-stage hydraulic fractures will be converted to injection to provide waterflood support to existing horizontal/vertical producing wells (Figure 5) within the proposed Goodlands Unit No. 3 to complete waterflood patterns.

Geology

Stratigraphy:

The Triassic aged Lower Amaranth formation is the oil producing reservoir that is the subject of this unit application. The stratigraphy of the reservoir section for the proposed unit is shown on the structural cross section attached as Appendix 1. The section runs N to S approximately through the mid-point of the proposed unit. The Lower Amaranth is bounded on top by the Amaranth Evaporite and by the Mississippian Unconformity at the base.

Stratigraphic nomenclature has been modeled after previous operator's (EOG Resources) conventions. The producing sequence in descending order consists of the Lower Amaranth A Unit, Lower Amaranth Green Sand, Lower Amaranth Blue Sand, Lower Amaranth Purple Sand, Lower Amaranth Brown Sand, Lower Amaranth Red Sand, and the Lower Amaranth Lower Sand. The reservoir units are primarily represented by the Green, Blue, Purple, Brown, and Red Sands. The Upper portion of the Lower Amaranth A unit is considered tight, and represents the top seal for the reservoir.

Sedimentology:

The Lower Amaranth reservoir units (top of Green through to base of Red Sand) comprise interlaminated shale, siltstone, and fine grained sandstone. The laminations tend to range from > 1 cm up to 20 cm in thickness, often show signs of scouring at the base of each laminae, and tend to fine upwards. There are anhydrite beds capping each sub-unit within the producing sequence; these anhydrite layers are generally correlatable over the entire Pierson / Waskada / Goodlands area. These anhydrite layers are the basis for the stratigraphic framework that is being used to describe the reservoir within the proposed unit.

The units within the producing sequence have very similar characteristics. Color tends to vary with grain size in that the finer grained material tends to be brick red, while the courser grained material generally tends to be grey to light brown. All of the sub units have a varying component of anhydrite cement, which will appear as mm sized nodules in heavily cemented areas. Finally, well rounded, floating, coarse, frosted quartz grains are common throughout the entire productive interval.

Lower Amaranth reservoir is interpreted as having been deposited in an arid tidal flat (Sabkha) setting. The stratigraphic divisions (Green, Blue, Purple, Brown, Red, and Lower Sands) are interpreted as representing individual evaporitic cycles, each exhibiting relatively higher depositional energy at the base, grading into very low energy towards the top.

Since each cycle is bound by an erosive surface on the top and bottom, there can be lateral variability in sediment preservation within each cycle. Occasional preservation of high angled cross stratification suggests periods of very high energy during deposition which are interpreted as channel deposits, which help support a tidal flat setting depositional model.

The Upper portion of the Upper Amaranth A unit is made up of brick red shale that is generally not bedded and does not tend to exhibit any sedimentary structures. It is a low permeability zone that represents the top seal to the Lower Amaranth reservoir.

The Lower Sand portion of the Lower Amaranth (immediately beneath the Red Sand), has a lot of the same characteristics as the productive interval, but tends to have much less effective porosity due to abundant anhydrite cement.

Structure:

Structure contour maps are provided for the top and base of the reservoir interval (Appendices 2 and 3). The reservoir units dip to the southwest, which is consistent with the regional dip. Structural mapping based on well control does not indicate the presence of large scale structural features that would indicate an increased risk of faulting within the proposed unit boundary.

Reservoir Continuity:

There are limited barriers to reservoir continuity that are apparent from the data available. Available data from well logs do not show any apparent lateral facies changes within the proposed unit that would result in significant lateral permeability barriers. An isopach map of the reservoir interval (Appendix 4) shows that the reservoir thickness remains consistent at about 10.0 meters.

Also, as mentioned above, there are no indications of any structural features that could set up any lateral permeability barriers within the proposed unit. The lack of lateral permeability barriers suggests this pool is well suited for secondary oil recovery.

Reservoir Quality:

Net pay determination within the proposed unit was done by using a sonic porosity cut off. There are a number of steps that were undertaken in order to determine net pay from sonic log data:

- Core data from the entire Waskada / Goodlands area (Appendix 5) was used to determine a relationship between porosity and permeability. Based on a best fit line through the available core analysis it was determined that a core porosity of 10% represents 0.5 md of permeability (Appendix 6).
- Sonic porosity was calculated for wells in which digital sonic data was available (Appendix 7) using the following formula:

$$\text{Sonic Porosity} = \frac{Dt - Dt_{\text{matrix}}}{Dt_{\text{water}} - Dt_{\text{matrix}}}$$

Where

Dt = Sonic travel time (ms/m)

Dt_{matrix} = Sonic travel time of the rock matrix (198 ms/m)

Dt_{water} = Sonic travel time of the formation water (681 ms/m)

- In order to translate this relationship to well logs, a comparison between sonic porosity and core porosity was undertaken. A total of 52 wells were found in the Waskada / Goodlands area that had digital sonic curves along with core analysis over the Lower Amaranth reservoir interval (Appendix 8). Sonic porosity from logs was compared to core porosity from core analysis (Appendix 9) and the data suggests that there is a good relationship between porosity from core and porosity from Sonic data.

From this relationship, a sonic log porosity cut of 10% was used as a pay determination for each logged well. In this way, the porosity / permeability relationship as determined from core can be translated into wells where there is log data available. In turn, this increases the control points for OOIP determination, which increases the resolution of OOIP mapping.

OOIP Estimates

OOIP values were calculated using the following volumetric equation:

$$OOIP = \frac{Area * Net Pay * Porosity * (1 - Water Saturation)}{Initial Formation Volume Factor of Oil}$$

or

$$OOIP(m3) = \frac{A * h * \phi * (1 - Sw)}{Bo} * \frac{10,000m2}{ha}$$

or

$$OOIP(Mbbl) = \frac{A * h * \phi * (1 - Sw)}{Bo} * 3.28084 \frac{ft}{m} * 7,758.367 \frac{bbl}{acre * ft} * \frac{1Mbbl}{1,000bbl}$$

where

| | |
|------------|---|
| OOIP | = Original Oil in Place by LSD (Mbbbl, or m3) |
| A | = Area (40acres, or 16.187 hectares, per LSD) |
| h * ϕ | = Net Pay * Porosity, or Phi * h (ft, or m) |
| Bo | = Formation Volume Factor of Oil (stb/rb, or sm ³ /rm ³) |
| Sw | = Water Saturation (decimal) |

For the purposes of this unit application, Bo and Sw were held constant at 1.17 and 40% respectively. The initial oil formation volume factor was adopted from a PVT taken from the 8-26-1-26W1, thought to be representative of the fluid characteristics in the reservoir. Sw determination was set at 40% based on analysis of capillary pressure data from six different locations in the Waskada / Goodlands area (6-21-1-25W1, 7-28-1-25W1, 13-10-1-24W1, 15-1-1-25W1, and 14-14-2-25W1).

Average sonic porosity for the proposed Unit area has been included as Appendix 10.

Phi * h maps were created from sonic porosity log data (Appendix 11). The average phi * h value within each LSD was calculated using IHS Petra software, this provided the final input into the OOIP calculation.

Total volumetric OOIP for the Lower Amaranth within the proposed unit has been calculated to be 6,130 e³m³ (38,559 Mbbbls). Tabulated parameters for each LSD from the calculations can be found in Table 4.

Original Oil in Place (OOIP) calculations and geologic summary were prepared by Todd Neely and reviewed by Bill Ward, P. Geologist.

Historical Production

A historical group production history plot for the proposed Goodlands Unit No. 3 is shown as Figure 4. Oil production commenced from the proposed Unit area in January 1997 and peaked during September 2013 at 299.8 m³ OPD. As of April 2016, production was 85.0 m³ OPD, 395.2 m³ of water per day (WPD) and an 82.3% watercut.

From peak production in September 2013 to date, oil production is declining at an annual rate of approximately **30%** under the current Primary Production method.

The remainder of the field's production and decline rates indicate the need for pressure restoration and maintenance. Waterflooding is deemed to be the most efficient means of secondary recovery to introduce energy back into the system and provide a real sweep between wells.

UNITIZATION

Unitization and implementation of a Waterflood EOR project is forecasted to increase overall recovery of OOIP from the proposed project area.

Unit Name

Tundra proposes that the official name of the new Unit shall be Goodlands Unit No. 3.

Unit Operator

Tundra Oil and Gas Partnership (Tundra) will be the Operator of record for Goodlands Unit No. 3.

Unitized Zone

The Unitized zone(s) to be waterflooded in the Goodlands Unit No. 3 will be the Lower Amaranth formation.

Unit Wells

The 74 horizontal wells, 3 deviated wells and 35 vertical wells to be included in the proposed Goodlands Unit No. 3 are outlined in Table 3.

Unit Lands

The Goodlands Unit No. 3 will consist of 50 LSDs as follows:

- LSDs 1-14 Section 9 of Township 1, Range 24, W1M
- LSDs 1-6, 11-14 Section 10 of Township 1, Range 24, W1M
- LSDs 3-4 Section 11 of Township 1, Range 24, W1M
- LSDs 5-6, 11-16 Section 14 of Township 1, Range 24, W1M
- LSDs 3-16 Section 15 of Township 1, Range 24, W1M

The lands included in the 40 acre tracts are outlined in Table 1.

Tract Factors

The proposed Goodlands Unit No. 3 will consist of 50 Tracts based on the 40 acre LSDs containing the existing 74 horizontal, 3 deviated and 35 vertical wells.

The Tract Factor contribution for each of the LSD's within the proposed Goodlands Unit No. 3 was calculated as follows:

- Gross OOIP by LSD, minus cumulative production to date for the LSD as distributed by the LSD specific Production Allocation (PA) % in the applicable producing horizontal or vertical well (to yield Remaining Gross OOIP)

- Last twelve (12) months production to date for the LSD as distributed by the LSD specific PA % in the applicable producing horizontal or vertical well.
- Tract Factor by LSD = Fifty percent (50%) of the product of Remaining Gross OOIP by LSD as a % of total proposed Unit Remaining Gross OOIP, and fifty percent (50%) of the product of the Last 12 Months Production as a % of total proposed Unit Last 12 Months Production.

Tract Factor calculations for all individual LSDs based on the above methodology are outlined within Table 2. In the past, multiple methods of assigning tract participation factors have been used in the Waskada area. Tundra believes that the above given method provides the most equitable assignment of tract participation factors to all mineral owners, given the geological, reservoir and well completion risks associated with waterflooding horizontal to horizontal wellbores in Lower Amaranth formation.

Working Interest Owners

Table 1 outlines the working interest (WI) for each recommended Tract within the proposed Goodlands Unit No. 3. Tundra Oil and Gas Partnership holds a 100% WI ownership in all the proposed Tracts.

Tundra Oil and Gas Partnership will have a 100% WI in the proposed Goodlands Unit No. 3.

WATERFLOOD EOR DEVELOPMENT

Technical Studies

The waterflood performance predictions for the proposed Goodlands Unit No. 3 Lower Amaranth project are based on internal engineering assessments, as well as empirically observed waterflood performance in nearby Waskada Units 16 and 17, which employed a vertical to vertical waterflood. Utilizing project area specific reservoir and geological parameters, a Black oil simulation model using Exodus software was created by Tundra to evaluate the potential waterflood response using horizontal injectors to flood horizontal producers, which is the configuration that Tundra proposes in Goodlands Unit No. 3. While the model was created using geological and historical production data from Waskada Unit 19, in section 34-1-25W1, the results observed in the model were similar to those observed empirically in Units 16 and 17, and deemed representative of what Tundra would expect in Goodlands Unit 3.

Horizontal Injection Wells and EOR Development

Primary production from the original vertical/horizontal producing wells in the proposed Goodlands Unit No. 3 has declined significantly from peak rate indicating a need for secondary pressure support. Through the process of developing similar waterfloods, Tundra has measured a significant variation in reservoir pressure depletion by the existing primary producing wells. Placing new horizontal wells immediately on water injection in areas without significant reservoir pressure depletion has been problematic in similar low permeability formations, and has a negative impact on the ultimate total recovery of oil.

Tundra proposes to convert up to 29 horizontal producing wells to water injection wells (WIW) over a 3 year period, as shown in Figure 5. This conversion scheme would allow for approximately 30 acre effective spacing between offsetting injection wells. Alternative injection configurations may be considered depending on results from offset pilot areas in the Lower Amaranth formation, within the Waskada field. These configurations could result in the conversion of more or less wells to injection than what is shown in Figure 5. Additionally, new horizontal injectors may be considered to be drilled if they are deemed to be essential to improving recovery in the unit. If new injection wells are drilled in this area, Tundra believes an initial period of producing all new horizontal wells prior to placing them on permanent water injection is essential and all Unit mineral owners will benefit.

Tundra will continue to monitor reservoir pressure, fluid production and decline rates in each pattern to determine when the well will be converted to water injection.

Reserves Recovery Profiles and Production Forecasts

The primary waterflood performance predictions for the proposed Goodlands Unit No. 3 are based on oil production decline curve analysis. The secondary predictions are based primarily on internal engineering analysis performed by the Tundra reservoir engineering group, utilizing an Exodus simulation model generated in Waskada Unit 19 (described previously), and simulating horizontal injectors offsetting horizontal producers for waterflood development. These results were then compared and contrasted to empirically observed data in Waskada Unit 16 and 17 to ensure proper calibration of data and results.

Primary Production Forecast

Cumulative allocated production in the Goodlands Unit No. 3 project area, to the end of July 2016 from 112 wells, was 473.6 e³m³ of oil and 950.1 e³m³ of water for a recovery factor of **7.7%** of the calculated Net OOIP.

Ultimate Primary Proved Producing oil reserves recovery for Goodlands Unit No. 3 has been estimated to be **597.1 e³m³**, or a **9.7%** Recovery Factor (RF) of OOIP. Remaining Producing Primary Reserves has been estimated to be **123.4 e³m³** to the end of July 2016.

The expected production decline and forecasted cumulative oil recovery under continued Primary Production is shown in Figures 7 and 8.

Pre-Production Schedule/Timing for Conversion of Horizontal Wells to Water Injection

Tundra proposes to implement an initial phase which consists of 8 Horizontal conversions throughout 2017 to test the efficiency of the Goodlands Unit No. 3 Waterflood.

Criteria for Conversion to Water Injection Well

Tundra will monitor the following parameters to assess the best timing for each individual horizontal well to be converted from primary production to water injection service.

- Measure reservoir pressures through primary production
- Fluid production rates and any changes in decline rate
- Any observed production interference effects with adjacent vertical and horizontal wells
- Pattern mass balance and/or oil recovery factor estimates
- Reservoir pressure relative to bubble point pressure

The above schedule allows for the proposed Goodlands Unit No. 3 project to be developed equitably, efficiently, and moves the project to the best condition for the start of waterflood as quickly as possible. It also provides the Unit Operator flexibility to manage the reservoir conditions and response to help ensure maximum ultimate recovery of reserves.

Secondary EOR Production Forecast

The proposed project oil production profile under Secondary Waterflood has been developed based on the response observed to date in Waskada Unit 16 and 17, as well as internal Black Oil Simulation model of section 34-1-25W1 in Waskada 19, which simulates a horizontal to horizontal waterflood. (Figure 6).

Secondary Waterflood plots of the expected oil production forecast over time and the expected oil production vs. cumulative oil are plotted in Figures 9 and 10, respectively. Total Secondary EUR for the proposed Goodlands Unit No. 3 is estimated to be **799.9 e³m³** with **326.3 e³m³** remaining representing a total secondary recovery factor of **13.0%** for the proposed Unit area. An incremental **202.8 e³m³** of oil, or a **3.3%** recovery factor, are forecasted to be recovered under the proposed Unitization and Secondary EOR production scheme vs. the existing Primary Production method.

Estimated Fracture Pressure

Completion data from the existing producing wells within the project area indicate an actual fracture pressure gradient range of 17.0 to 18.0 kPa/m true vertical depth (TVD).

WATERFLOOD OPERATING STRATEGY

Water Source

The injection water for the proposed Goodlands Unit No. 3 will be supplied from the existing Goodlands 16-10-001-24W1 Battery source and injection water system. All injection water will be obtained from the Swan River formation in the 100/04-15-001-24W1 well, which Tundra intends to have licensed as a water source well. Swan River water from the source well is pumped to an injection facility at 16-10-001-24W1, filtered, and pumped up to injection system pressure. A diagram of the Goodlands water injection system and new pipeline connection to the proposed Goodlands Unit No. 3 project area injection wells is shown as Figure 11.

Based on past experience, Tundra does not believe that the produced water can be cleaned to the required specifications feasibly. Therefore, Tundra plans to use source water from a Swan River well as a source supply for Goodlands Unit No. 3.

A mixture of produced waters from the Lower Amaranth has been extensively tested for compatibility with 100/05-09-001-25W1 source Swan River water (which is expected to be of similar composition to the 100/04-15-001-24W1 source water well), by a highly qualified third party, prior to implementation by Tundra. All potential mixture ratios between the two waters, under a range of temperatures, have been simulated and evaluated for scaling and precipitate producing tendencies. Testing of multiple scale inhibitors has also been conducted and minimum inhibition concentration requirements for the source water volume determined. Continuous scale inhibitor application will be maintained into the source water stream out of the Goodlands injection water facility, as it is in our neighboring Waskada facilities. Review and monitoring of the source water scale inhibition system is also part of an existing routine maintenance program.

Injection Wells

New water injection wells for the proposed Goodlands Unit No. 3 will be cleaned out and configured downhole for injection as shown in Figure 12. The horizontal injection well will be stimulated by multiple hydraulic fracture treatments to obtain suitable injection. Tundra has extensive experience with horizontal fracturing in the area, and all jobs are rigorously programmed and monitored during execution. This helps ensure optimum placement of each fracture stage to prevent, or minimize, the potential for out-of-zone fracture growth and thereby limit the potential for future out-of-zone injection.

The new water injection wells will be placed on injection after the pre-production period and approval to inject. Wellhead injection pressures will be maintained below the least value of either:

- the area specific known and calculated fracture gradient, or
- the licensed surface injection Maximum Allowable Pressure (MOP)

Tundra has a thorough understanding of area fracture gradients. A management program will be utilized to set and routinely review injection target rates and pressures vs. surface MOP and the known area formation fracture pressures.

All new water injection wells are surface equipped with injection volume metering and rate/pressure control. An operating procedure for monitoring water injection volumes and meter balancing will also be utilized to monitor the entire system measurement and integrity on a daily basis.

The proposed Goodlands Unit No. 3 horizontal water injection well rate is forecasted to average **10 - 30** m³ WPD, based on expected reservoir permeability and pressure.

Reservoir Pressure

No representative initial pressure surveys are available for the proposed Goodlands Unit No. 3 project area in the Lower Amaranth producing zone. Tundra assumed operatorship of these properties in late 2015 and has been unable to recover any pressure surveys from the original operators.

Reservoir Pressure Management during Waterflood

Tundra expects it will take 2-4 years to re-pressurize the reservoir due to cumulative primary production voidage and pressure depletion. Initial monthly Voidage Replacement Ratio (VRR) is expected to be approximately 1.25 to 2.00 within the patterns during the fill up period. As the cumulative VRR approaches 1, target reservoir operating pressure for waterflood operations will be 75-90% of original reservoir pressure.

Waterflood Surveillance and Optimization

Goodlands Unit No. 3 EOR response and waterflood surveillance will consist of the following:

- Regular production well rate and WCT testing
- Daily water injection rate and pressure monitoring vs target
- Water injection rate/pressure/time vs. cumulative injection plot
- Reservoir pressure surveys as required to establish pressure trends
- Pattern VRR
- Potential use of chemical tracers to track water injector/producer responses
- Use of some or all of: Water Oil Ratio (WOR) trends, Log WOR vs Cum Oil, Hydrocarbon Pore Volumes Injected, Conformance Plots

The above surveillance methods will provide an ever increasing understanding of reservoir performance, and provide data to continually control and optimize the Goodlands Unit No. 3 waterflood operation. Controlling the waterflood operation will significantly reduce or eliminate the potential for out-of-zone injection, undesired channeling or water breakthrough, or out-of-Unit migration. The monitoring and surveillance will also provide early indicators of any such issues so that waterflood operations may be altered to maximize ultimate secondary reserves recovery from the proposed Goodlands Unit No. 3.

On Going Reservoir Pressure Surveys

Any pressures taken during the operation of the proposed unit will be reported within the Annual Progress Reports for Goodlands Unit No. 3 as per Section 73 of the Drilling and Production Regulation.

Economic Limits

Under the current Primary recovery method, existing wells within the proposed Goodlands Unit No. 3 will be deemed uneconomic when the net oil rate and net oil price revenue stream becomes less than the current producing operating costs. With any positive oil production response under the proposed Secondary recovery method, the economic limit will be significantly pushed out into the future. The actual economic cut off point will then again be a function of net oil price, the magnitude and duration of production rate response to the waterflood, and then current operating costs. Waterflood projects generally become uneconomic to operate when Water Oil Ratios (WOR's) exceed 100.

WATER INJECTION FACILITIES

The Goodlands Unit No. 3 waterflood operation will utilize the existing Tundra operated source well supply and water plant (WP) facilities located at 16-10-001-25 W1M Battery. Injection wells will be connected to the existing high pressure water pipeline system supplying other Tundra-operated Waterflood Units.

A complete description of all planned system design and operational practices to prevent corrosion related failures is shown in Figure 13.

NOTIFICATION OF MINERAL AND SURFACE RIGHTS OWNERS

Tundra is in the process of notifying all mineral rights and surface rights owners of this proposed EOR project and formation of Goodlands Unit No. 3. Copies of the notices and proof of service, to all surface and mineral rights owners will be forwarded to the Petroleum Branch when available to complete the Goodlands Unit No. 3 Application.

Goodlands Unit No. 3 Unitization, and execution of the formal Goodlands Unit No. 3 Agreement by affected Mineral Owners, is expected during Q1 2017. Copies of same will be forwarded to the Petroleum Branch, when available, to complete the Goodlands Unit No. 3 Application.

Should the Petroleum Branch have further questions or require more information, please contact Jennifer Abel at 204.748.4427 or by email at jennifer.abel@tundraoilandgas.com.

TUNDRA OIL & GAS PARTNERSHIP

Original Signed by Jennifer Abel, October 28, 2016, in Virden, AB

Proposed Goodlands Unit No. 3
Application for Enhanced Oil Recovery Waterflood Project

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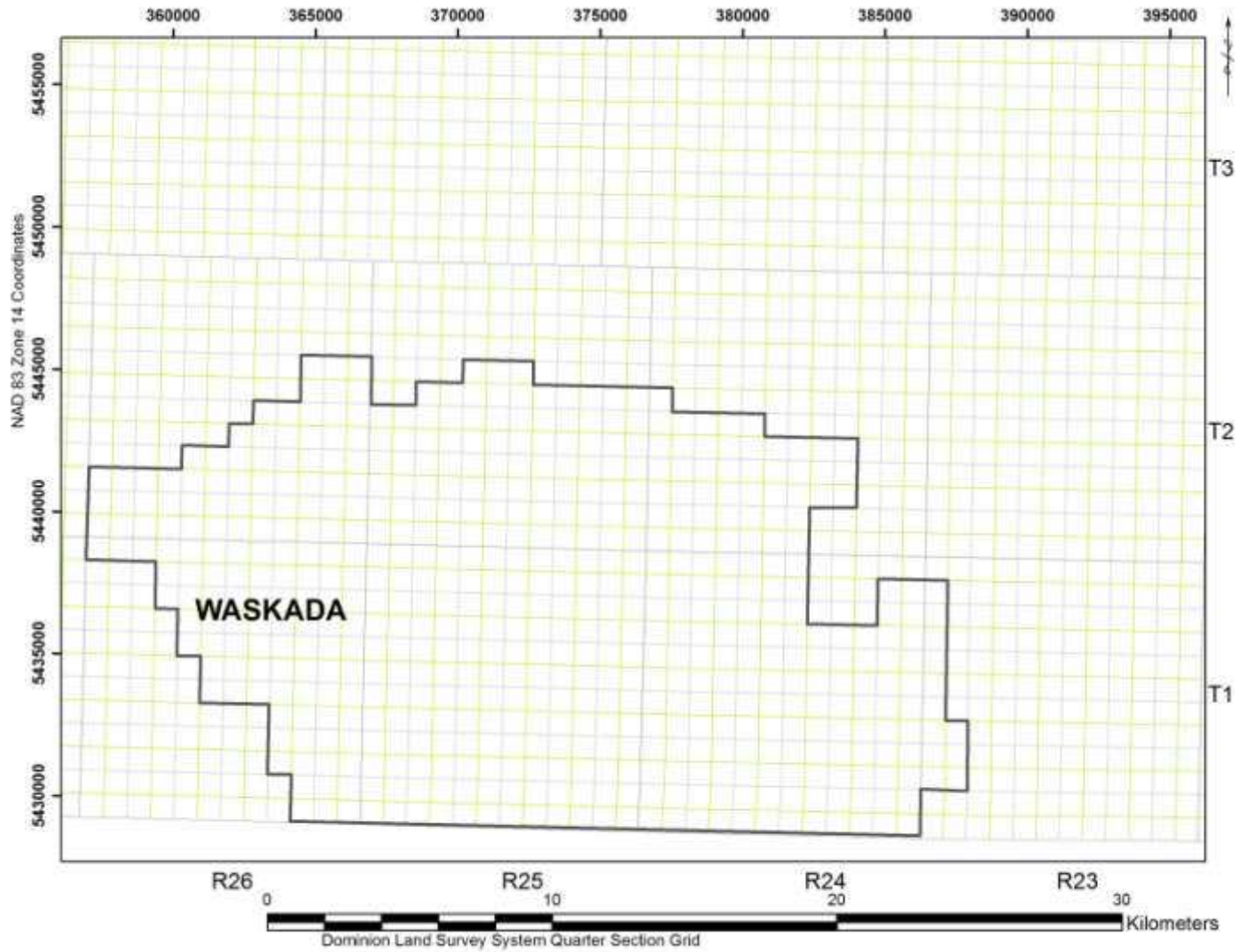


Figure 4 - Waskada Field (03)



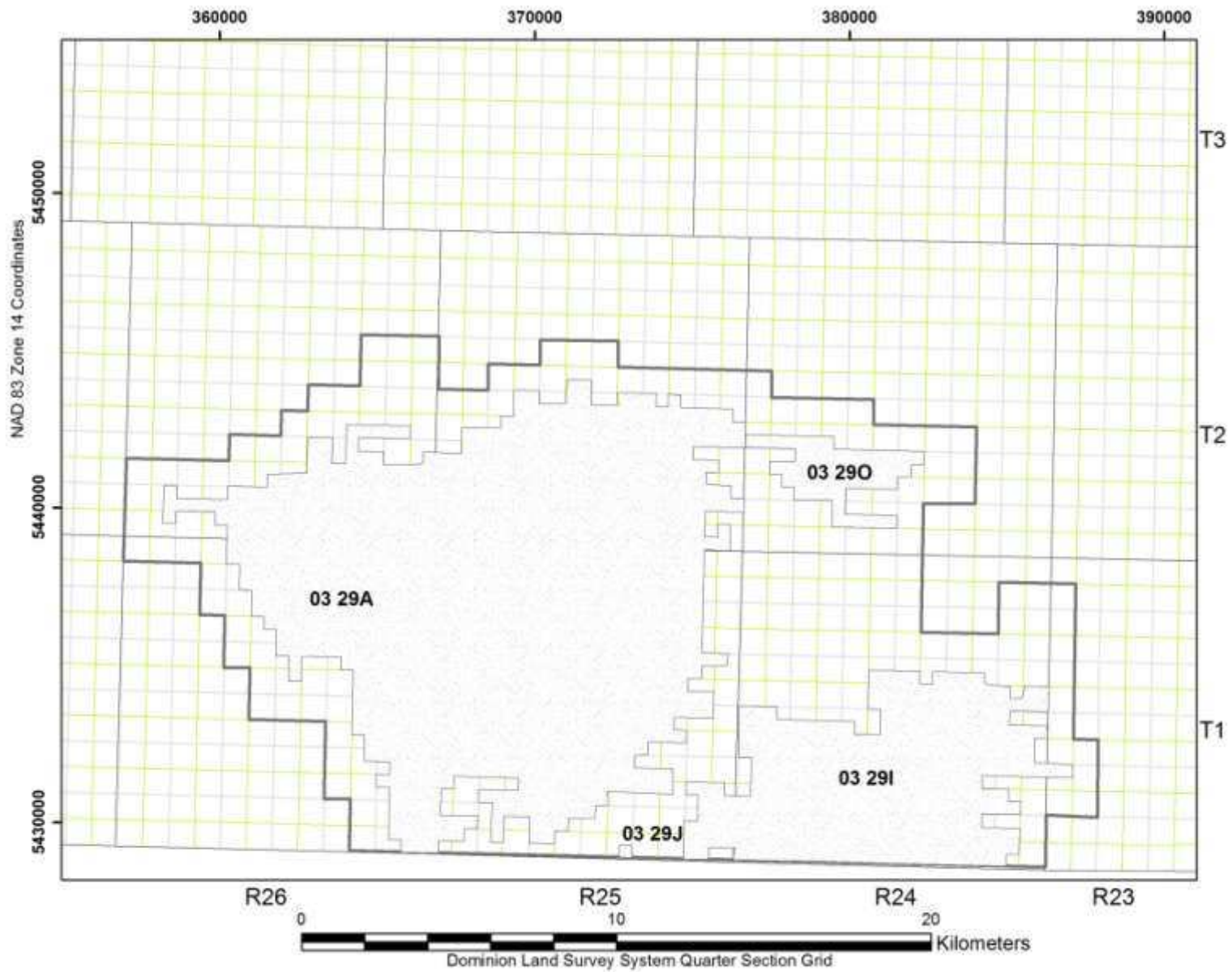
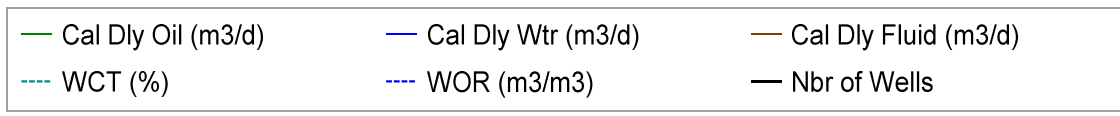
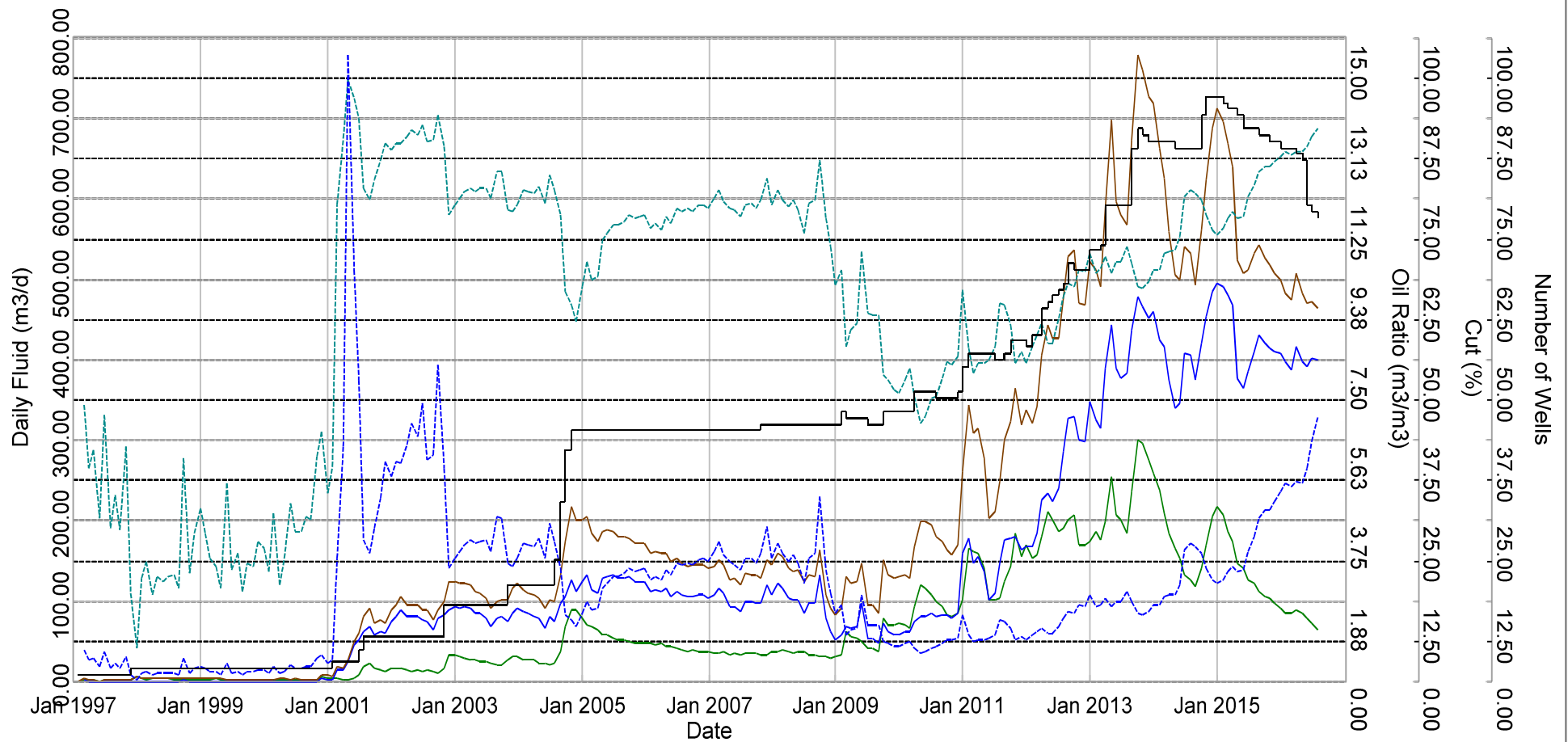


Figure 18 - Waskada Lower Amaranth Pools (03 29A, I, J, K & O)

Well Information as of 10/6/2016 - Group Well Report

Production Graph

| | | | | | |
|--------------------|------------------------------------|-------------------|--------------------|---------------------|--------------|
| Group: | 113 wells | On Prod: | 1997-01 to 2016-07 | Cum Oil: | 487018.3 m3 |
| # of Wells: | 113 | Prod Form: | AMRNTHL; AMRNTH | Cum Gas: | 13534.8 E3m3 |
| Fluid: | Oil | Field: | WASKADA (3) | Cum Wtr: | 1015839.5 m3 |
| Mode: | Producing; Pumping; Abandoned Zone | Pool Code: | 29I | Cum Inj Oil: | 0.0 m3 |
| | | Unit Code: | | Cum Inj Gas: | 0.0 E3m3 |
| | | | | Cum Inj Wtr: | 0.0 m3 |



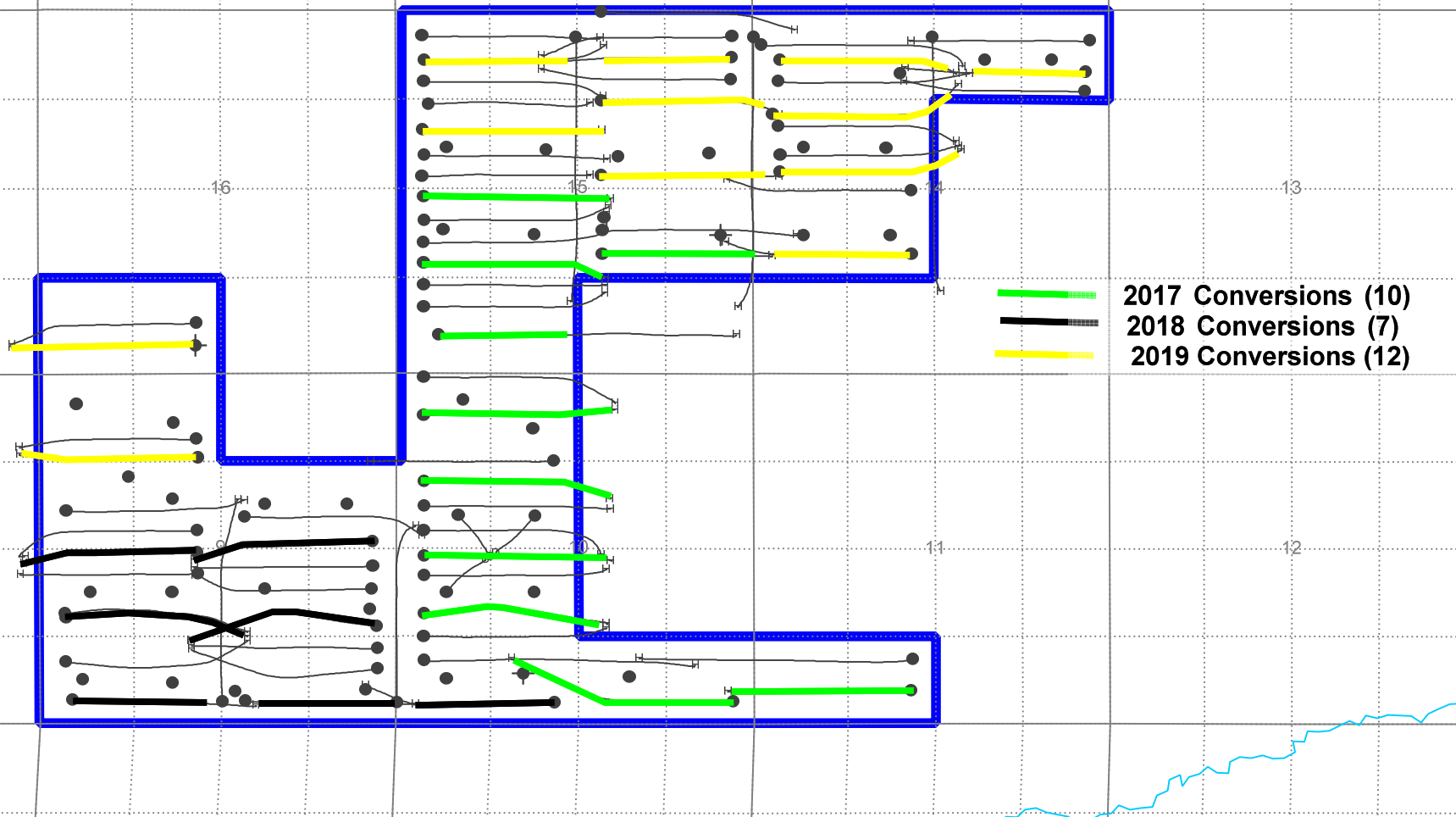
R24W1

FIGURE NO. 5

GOODLANDS UNIT 3 - DEVELOPMENT PLAN

T1

T1



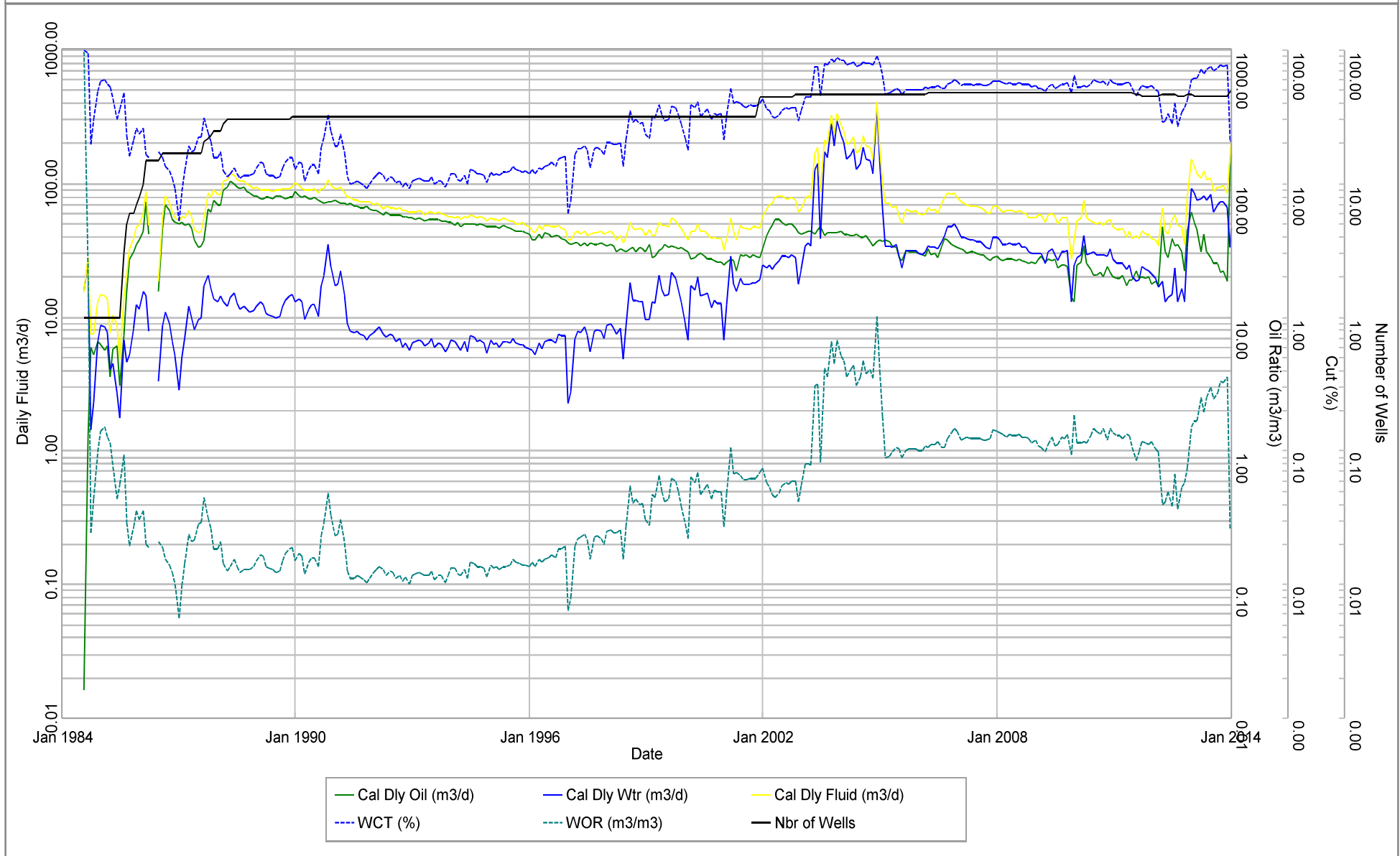
R24W1



Well Information as of 12/4/2015 - Group Well Report

Production Graph

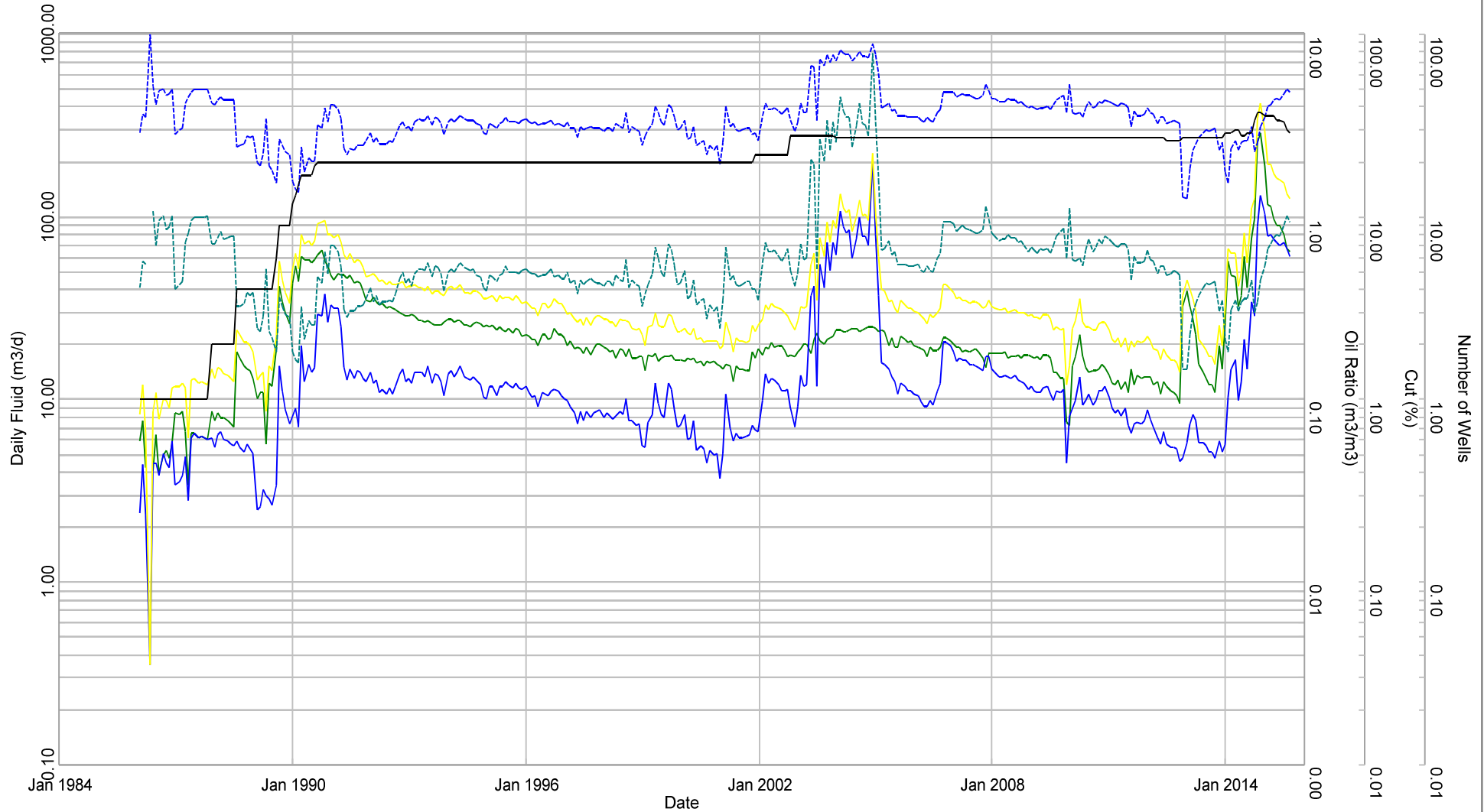
| | | | | | |
|--------------------|---|-------------------|------------------|-----------------|--------------------|
| Group: | waskada unit 16.lwell | Prod Form: | AMRNTHL; WINNPGS | On Prod: | 1984-07 to 2015-08 |
| # of Wells: | 69 | Field: | WASKADA (3) | Cum Oil: | 537510.3 m3 |
| Fluid: | Oil; Water Injection; Salt Water | Pool Code: | 29A; 76 | Cum Gas: | 2169.9 E3m3 |
| Mode: | Producing; Injection; Abandoned Zone; Pumping; Disposal | Unit Code: | 329A16; 329A17 | Cum Wtr: | 408882.7 m3 |



Well Information as of 12/4/2015 - Group Well Report

Production Graph

| | | | | | |
|--------------------|---|-------------------|-------------|-----------------|--------------------|
| Group: | waskada unit 17.lwell | Prod Form: | AMRNTHL | On Prod: | 1986-01 to 2015-08 |
| # of Wells: | 41 | Field: | WASKADA (3) | Cum Oil: | 270643.6 m3 |
| Fluid: | Oil; Water Injection | Pool Code: | 29A | Cum Gas: | 1105.9 E3m3 |
| Mode: | Producing; Pumping; Injection; Abandoned Zone | Unit Code: | 329A17 | Cum Wtr: | 178020.3 m3 |



— Cal Dly Oil (m3/d) — Cal Dly Wtr (m3/d) — Cal Dly Fluid (m3/d)
- - - WCT (%) - - - WOR (m3/m3) — Nbr of Wells

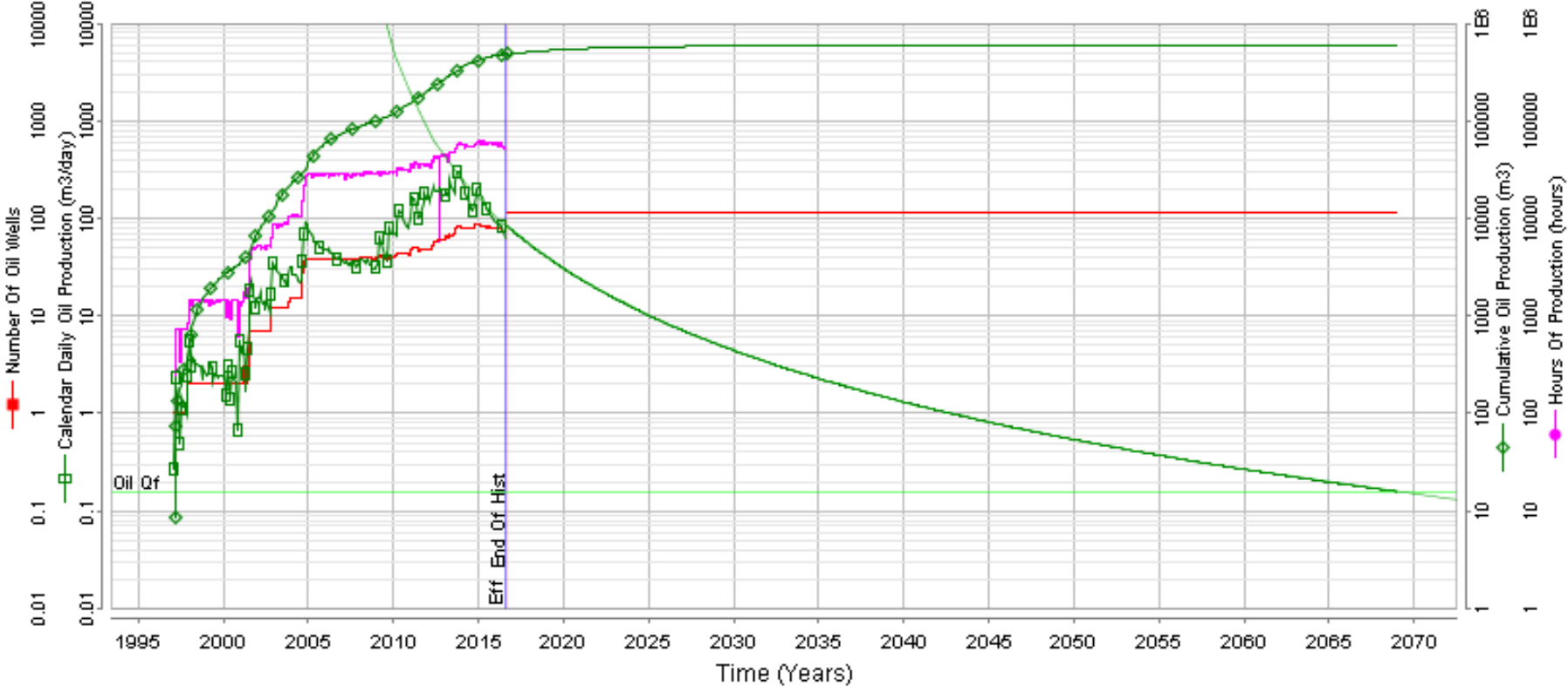
Figure No. 7

PRODUCTION AND FORECAST

Effective August 01, 2016

Operator: TUNDRA OIL & GAS LIMITED
 Province: Manitoba
 Field: multi zone (113)
 Pool: multi zone (113)
 Unit: multi zone (113)
 Status: Oil Prod

Goodlands Unit 3
 Goodlands U3- GROUP-113
 Base



| | | | | | | | |
|----------------------------|------------|-------------------------|-----------|------------------------|-----------|----------------------|-------|
| Oil Cum (m3) | 473,597 | Gas Cum (E3m3) | 13,408 | Water Cum (m3) | 1,011,357 | FCond Cum (m3) | 0 |
| Oil Rem Rec (m3) | 123,467 | Gas Rem Rec (E3m3) | 0 | Water Rem Rec (m3) | 0 | FCond Rem Rec (m3) | 0 |
| Oil Ult Rec (m3) | 597,064 | Gas Ult Rec (E3m3) | 13,408 | Water Ult Rec (m3) | 1,011,357 | FCond Ult Rec (m3) | 0 |
| Forecast Start (T0) | 08/01/2016 | Calculation Type | Undefined | Est Cum Prod (m3) | 473,597 | Decline Exp | 0.300 |
| Forecast End (Tf) | 11/12/2068 | OVIP (Volumetric) (m3) | 0 | Remaining Rec (m3) | 123,467 | Initial Decline (De) | 30.0 |
| Initial Rate (qi) (m3/day) | 84.2 | Rec Factor (Volumetric) | 0.000 | Gas Surface Loss | 0.0 | Reserve Life Index | 4.68 |
| Final Rate (qf) (m3/day) | 0.2 | Ult Recoverable (m3) | 597,064 | Gas Total Sales (E3m3) | 0 | Reserve Half Life | 3.20 |

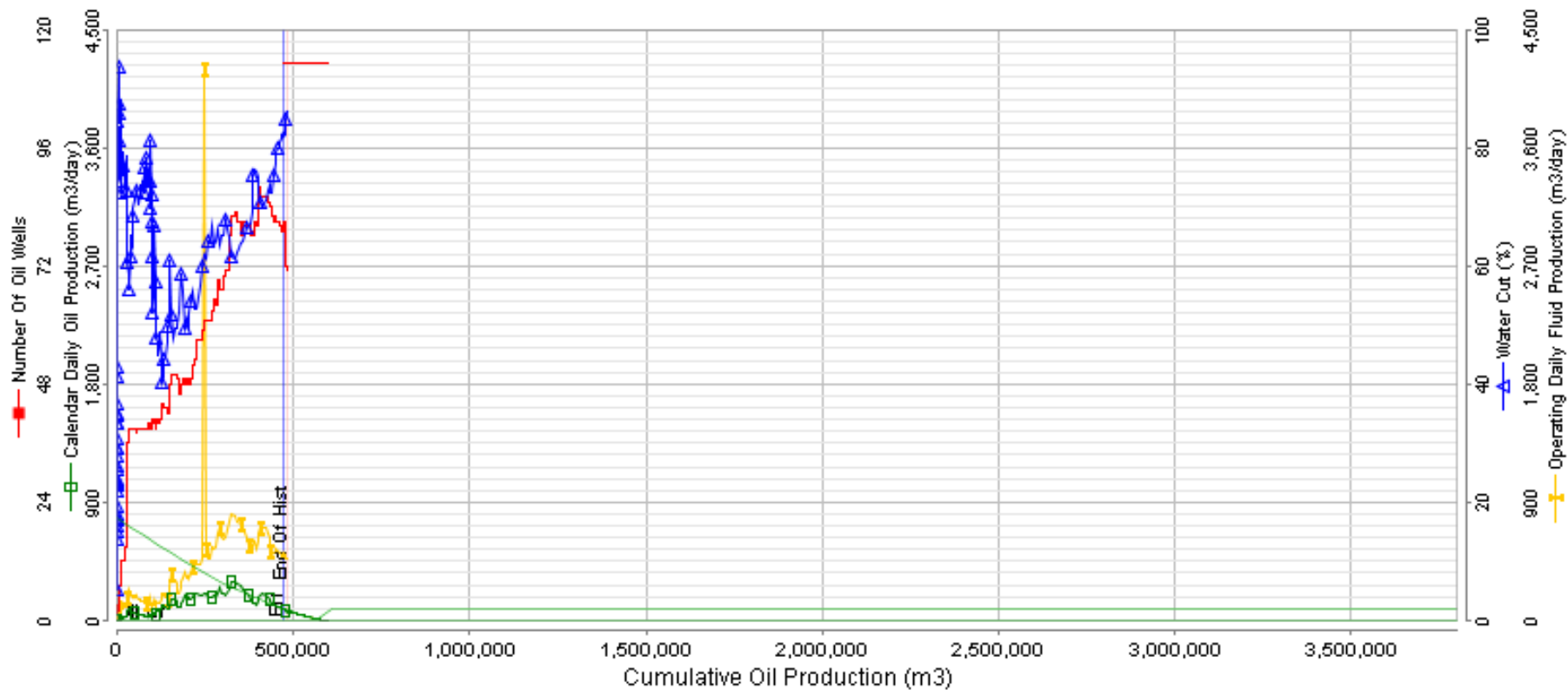
Figure No. 8

PRODUCTION AND FORECAST

Effective August 01, 2016

Operator: TUNDRA OIL & GAS LIMITED
 Province: Manitoba
 Field: multi zone (113)
 Pool: multi zone (113)
 Unit: multi zone (113)
 Status: Oil Prod

Goodlands Unit 3
 Goodlands U3- GROUP-113
 Base



| | | | | | | | |
|----------------------------|------------|-------------------------|-----------|------------------------|-----------|----------------------|-------|
| Oil Cum (m3) | 473,597 | Gas Cum (E3m3) | 13,408 | Water Cum (m3) | 1,011,357 | FCond Cum (m3) | 0 |
| Oil Rem Rec (m3) | 123,467 | Gas Rem Rec (E3m3) | 0 | Water Rem Rec (m3) | 0 | FCond Rem Rec (m3) | 0 |
| Oil Ult Rec (m3) | 597,064 | Gas Ult Rec (E3m3) | 13,408 | Water Ult Rec (m3) | 1,011,357 | FCond Ult Rec (m3) | 0 |
| Forecast Start (T0) | 08/01/2016 | Calculation Type | Undefined | Est Cum Prod (m3) | 473,597 | Decline Exp | 0.300 |
| Forecast End (Tf) | 11/12/2068 | OVIP (Volumetric) (m3) | 0 | Remaining Rec (m3) | 123,467 | Initial Decline (De) | 30.0 |
| Initial Rate (qi) (m3/day) | 84.2 | Rec Factor (Volumetric) | 0.000 | Gas Surface Loss | 0.0 | Reserve Life Index | 4.68 |
| Final Rate (qf) (m3/day) | 0.2 | Ult Recoverable (m3) | 597,064 | Gas Total Sales (E3m3) | 0 | Reserve Half Life | 3.20 |

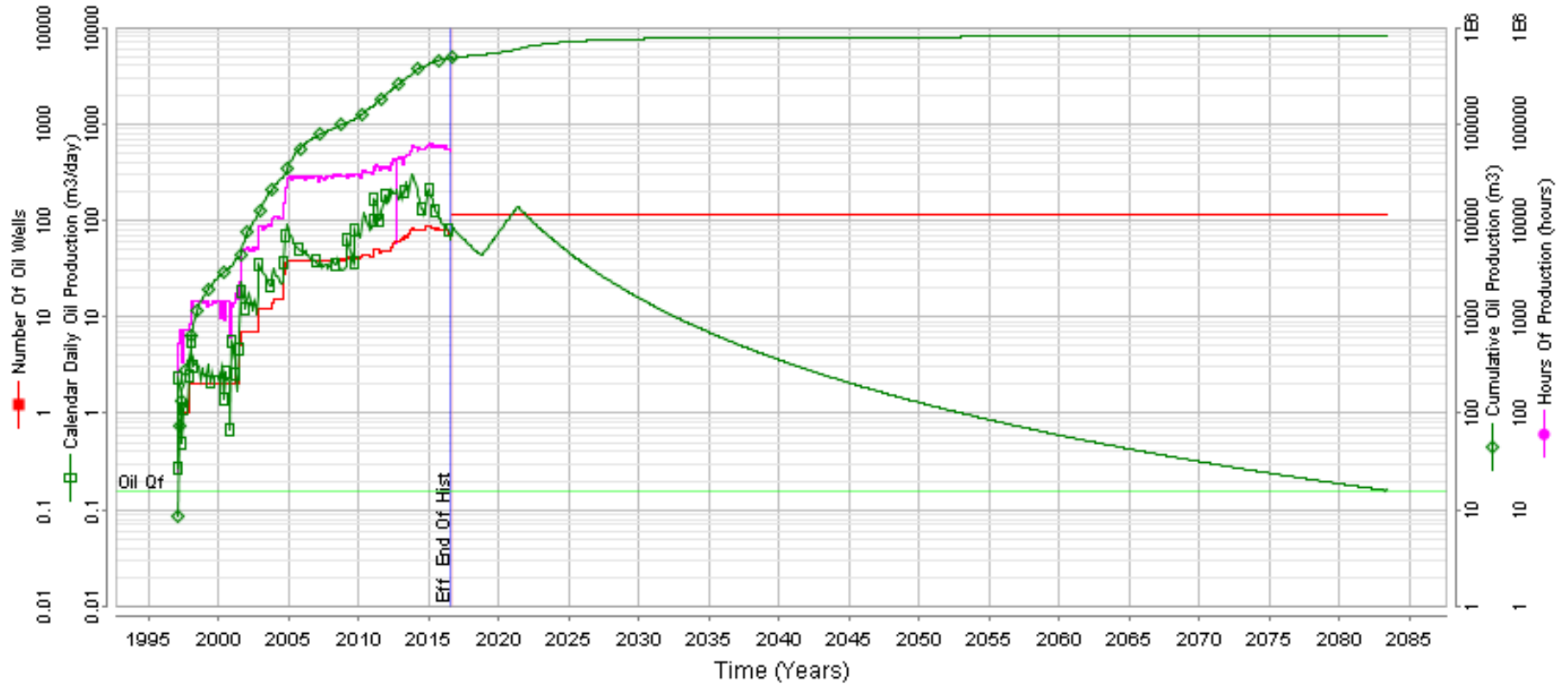
Figure No. 9

PRODUCTION AND FORECAST

Effective August 01, 2016

Operator: TUNDRA OIL & GAS LIMITED
 Province: Manitoba
 Field: multi zone (113)
 Pool: multi zone (113)
 Unit: multi zone (113)
 Status: Oil Prod

Goodlands Unit 3
 Goodlands U3- GROUP-113
 Base + Growth 1



| | | | | | | | |
|----------------------------|------------|-------------------------|-----------|------------------------|-----------|----------------------|-------|
| Oil Cum (m3) | 473,597 | Gas Cum (E3m3) | 13,408 | Water Cum (m3) | 1,011,357 | FCond Cum (m3) | 0 |
| Oil Rem Rec (m3) | 326,296 | Gas Rem Rec (E3m3) | 0 | Water Rem Rec (m3) | 0 | FCond Rem Rec (m3) | 0 |
| Oil Ult Rec (m3) | 799,893 | Gas Ult Rec (E3m3) | 13,408 | Water Ult Rec (m3) | 1,011,357 | FCond Ult Rec (m3) | 0 |
| Forecast Start (T0) | 08/01/2016 | Calculation Type | Undefined | Est Cum Prod (m3) | 473,597 | Decline Exp | 0.300 |
| Forecast End (Tf) | 04/10/2083 | OVIP (Volumetric) (m3) | 0 | Remaining Rec (m3) | 326,296 | Initial Decline (De) | 30.0 |
| Initial Rate (qi) (m3/day) | 84.2 | Rec Factor (Volumetric) | 0.000 | Gas Surface Loss | 0.0 | Reserve Life Index | 12.37 |
| Final Rate (qf) (m3/day) | 0.2 | Ult Recoverable (m3) | 799,893 | Gas Total Sales (E3m3) | 0 | Reserve Half Life | 5.66 |

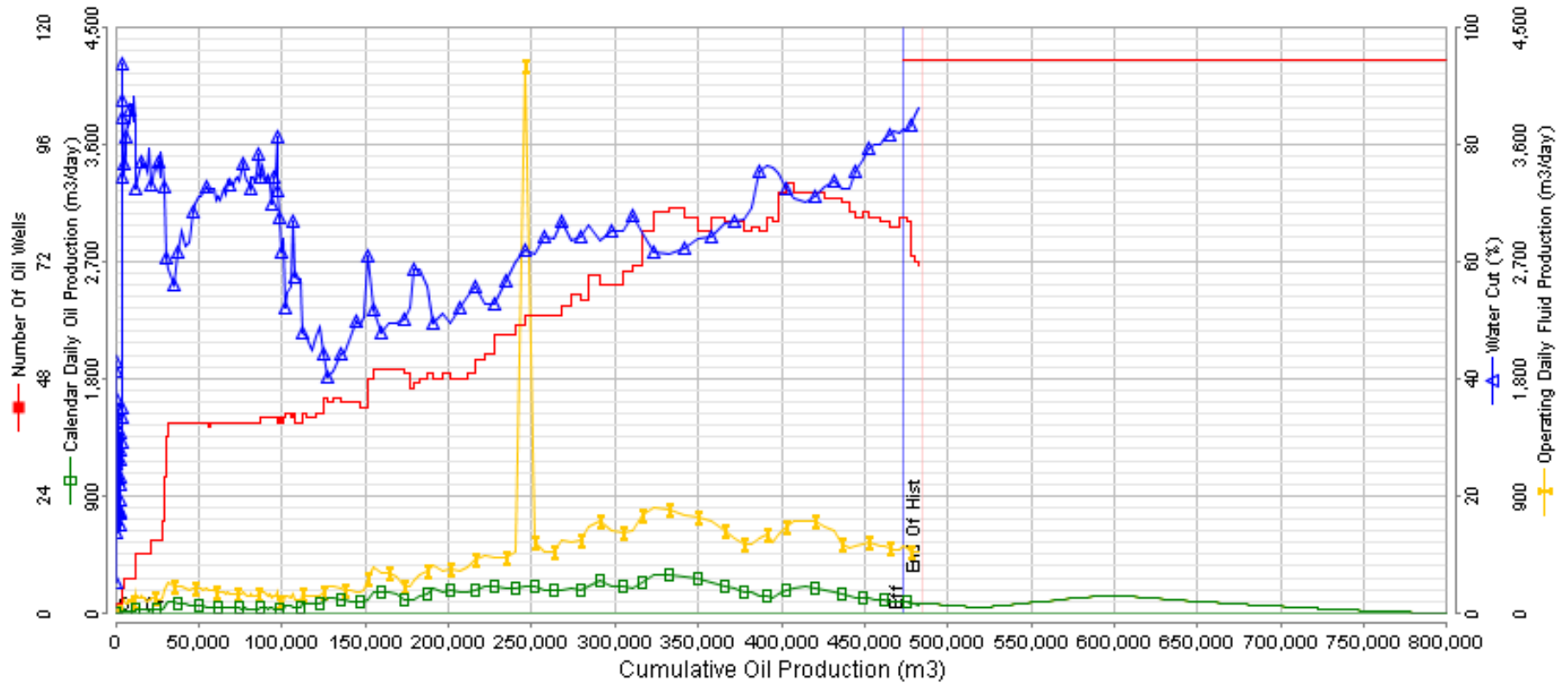
Figure No. 10

PRODUCTION AND FORECAST

Effective August 01, 2016

Operator: TUNDRA OIL & GAS LIMITED
 Province: Manitoba
 Field: multi zone (113)
 Pool: multi zone (113)
 Unit: multi zone (113)
 Status: Oil Prod

Goodlands Unit 3
 Goodlands U3- GROUP-113
 Base + Growth 1



| | | | | | | | |
|----------------------------|------------|-------------------------|-----------|------------------------|-----------|----------------------|-------|
| Oil Cum (m3) | 473,597 | Gas Cum (E3m3) | 13,408 | Water Cum (m3) | 1,011,357 | FCond Cum (m3) | 0 |
| Oil Rem Rec (m3) | 326,296 | Gas Rem Rec (E3m3) | 0 | Water Rem Rec (m3) | 0 | FCond Rem Rec (m3) | 0 |
| Oil Ult Rec (m3) | 799,893 | Gas Ult Rec (E3m3) | 13,408 | Water Ult Rec (m3) | 1,011,357 | FCond Ult Rec (m3) | 0 |
| Forecast Start (T0) | 08/01/2016 | Calculation Type | Undefined | Est Cum Prod (m3) | 473,597 | Decline Exp | 0.300 |
| Forecast End (Tf) | 04/10/2083 | OVIP (Volumetric) (m3) | 0 | Remaining Rec (m3) | 326,296 | Initial Decline (De) | 30.0 |
| Initial Rate (qi) (m3/day) | 84.2 | Rec Factor (Volumetric) | 0.000 | Gas Surface Loss | 0.0 | Reserve Life Index | 12.37 |
| Final Rate (qf) (m3/day) | 0.2 | Ult Recoverable (m3) | 799,893 | Gas Total Sales (E3m3) | 0 | Reserve Half Life | 5.66 |

K-600
AIR COMPRESSORS
 MODEL: Campbell Hausfeld
 CAPACITY: 30 Gal
 2HP MOTOR
 600V/3P/60HZ

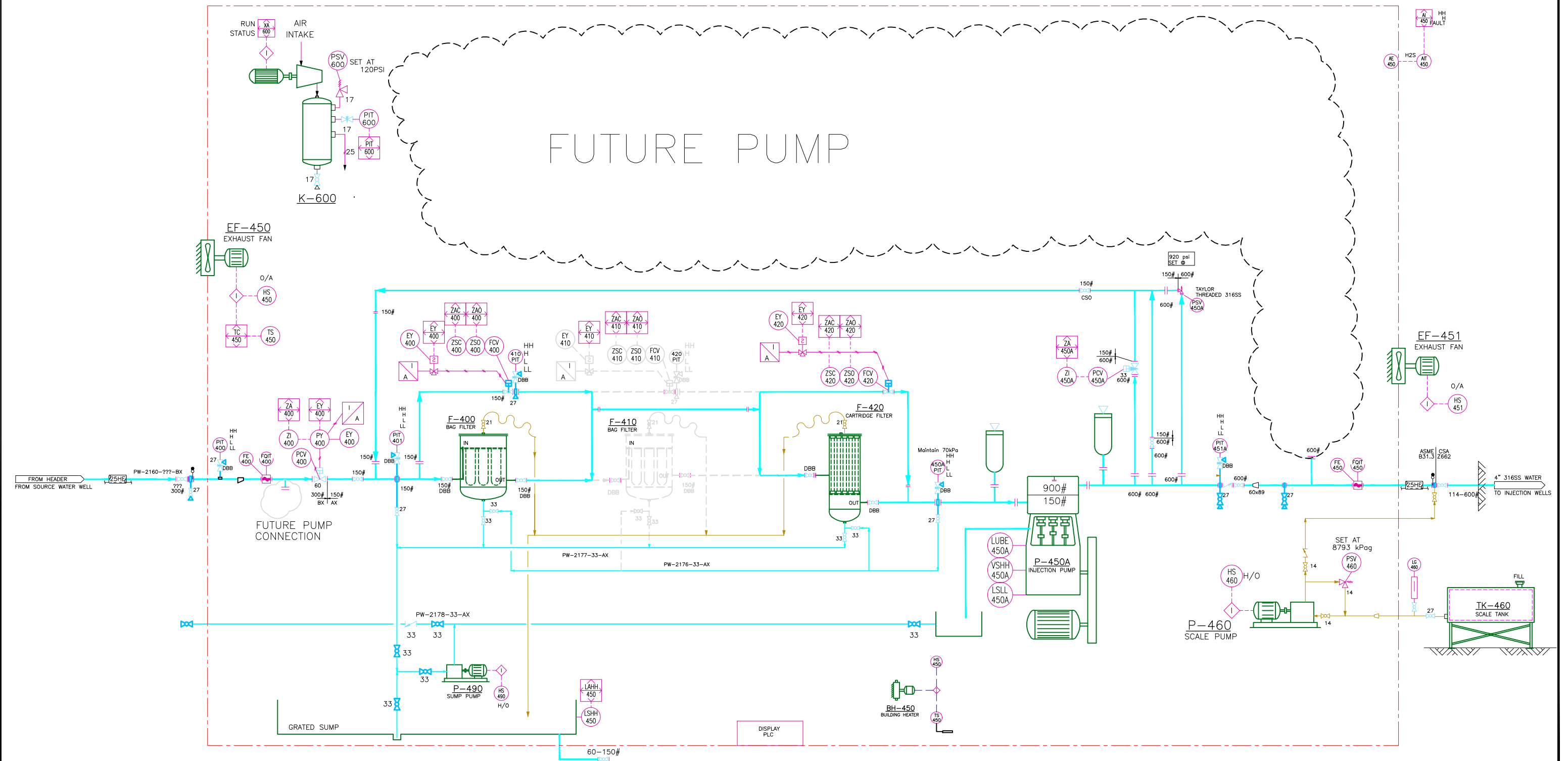
P-490
SUMP PUMP
 MAKE: MOYNO
 MODEL: 34401 3913440100 S/N: 09100
 5 USGPM @ 15PSI
 .75 HP 230/3/460 VOLT BALDOR RELIANCE MOTOR
 MODEL: A-16687701 S/N: W1407282045

BH-450
BUILDING HEATER
 MAKE: RUFFNECK 15KW
 MODEL NO.: FX5-RH191367-150WT
 C/W XP THERMOSTAT
 1/2 HP 1725 RPM 460 VOLT

F-400
SS BAG WATER FILTER
 MAKE:
 MODEL NO.:
 CAP: 800 M3/D (147 GPM)
 MAWP: 150 PSI @ 225°F
 FILTER: 1 MICRON NOMINAL

F-420
SS CARTRIDGE WATER FILTER
 MAKE:
 MODEL NO.:
 CAP:
 MAWP: 150 PSI @ 225°F
 FILTER: 0.5 MICRON NOMINAL

P-450
WATER INJECTION PUMP
 VENDOR: NATIONAL J100L
 PLUNGERS: 3" RATE FOR 6428kPa (933PSI)
 CAP: (147) USGPM - 800 M3/DAY
 DRIVER: 100 HP TECO WESTINGHS
 DP: 1200 RPM, 600V/3P/60Hz
 S/N:



NOTES:
 1.

Figure No. 11a



GOODLANDS
 16-10-1-24 W1M

PROCESS & INSTRUMENTATION DIAGRAM
 INJECTION PUMP BUILDING

| REV | DESCRIPTION | BY | DATE | CHK | APP |
|-----|-------------------|----|------------|-----|-----|
| 0 | ISSUED FOR REVIEW | JC | 17SEPT2016 | - | - |

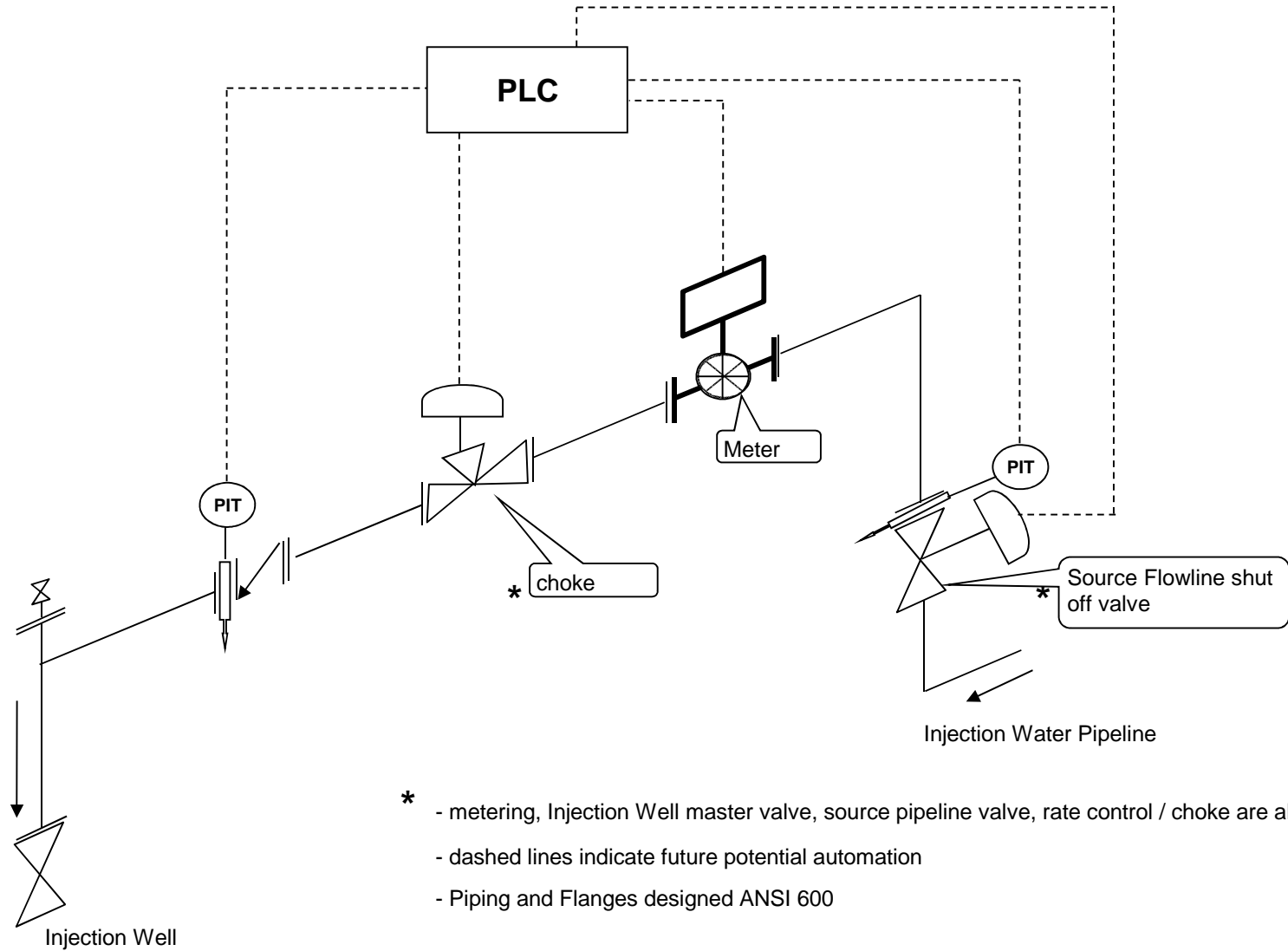
| REV | DESCRIPTION | BY | DATE | CHK | APP |
|-----|-------------------|----|------|-----|-----|
| - | REFERENCE DRAWING | | | | |

| | | | | |
|-----------------|---------------|------|--|--------------|
| DRAWN BY: JC | SCALE: NTS | AFE: | DRAWING NUMBER: 16-10-1-24-PID-2100 | REV NO: 0 |
|-----------------|---------------|------|--|--------------|

Figure No. 11b

Goodlands Unit No. 3

Proposed Injection Well Surface Piping P&ID



Goodlands Unit No. 3

EOR Waterflood Project

Planned Corrosion Control Program **

Source Well

- Continuous downhole corrosion inhibition
- Continuous surface corrosion inhibitor injection
- Downhole scale inhibitor injection
- Corrosion resistant valves and internally coated surface piping

Pipelines

- Source well to 11-30-1-25 Water Plant – Fiberglass
- New High Pressure Pipeline to Unit 9 injection wells – 2000 psi high pressure Fiberglass

Facilities

- 11-30-1-25 Water Plant and New Injection Pump Station
 - Plant piping – 600 ANSI schedule 80 pipe, Fiberglass or Internally coated
 - Filtration – Stainless steel bodies and PVC piping
 - Pumping – Ceramic plungers, stainless steel disc valves
 - Tanks – Fiberglass shell, corrosion resistant valves

Injection Wellhead / Surface Piping

- Corrosion resistant valves and stainless steel and/or internally coated steel surface piping

Injection Well

- Casing cathodic protection where required
- Wetted surfaces coated downhole packer
- Corrosion inhibited water in the annulus between tubing / casing
- Internally coated tubing surface to packer
- Surface freeze protection of annular fluid
- Corrosion resistant master valve
- Corrosion resistant pipeline valve

Producing Wells

- Casing cathodic protection where required
- Downhole batch corrosion inhibition as required
- Downhole scale inhibitor injection as required

Figure 13

** subject to final design and engineering

Proposed Goodlands Unit No. 3

Application for Enhanced Oil Recovery Waterflood Project

List of Tables

| | |
|---------|--|
| Table 1 | Tract Participation |
| Table 2 | Tract Factor Calculation |
| Table 3 | Current Well List and Status |
| Table 4 | Original Oil in Place and Recovery Factors |
| Table 5 | Reservoir and Fluid Properties |

TABLE NO. 1: TRACT PARTICIPATION FOR PROPOSED GOODLANDS UNIT NO. 3

| Working Interest | | | | Royalty Interest | | Tract Participation |
|------------------|------------------|------------------------------|-----------|------------------------------|-----------|---------------------|
| Tract No. | Land Description | Owner | Share (%) | Owner | Share (%) | Tract (%) |
| 1 | 01-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 1.691651890% |
| | | | | 5544573 Manitoba Ltd. | 25% | |
| | | | | 5153247 Manitoba Ltd. | 25% | |
| | | | | 6167471 Manitoba Ltd. | 25% | |
| 2 | 02-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 1.796707306% |
| | | | | 5544573 Manitoba Ltd. | 25% | |
| | | | | 5153247 Manitoba Ltd. | 25% | |
| | | | | 6167471 Manitoba Ltd. | 25% | |
| 3 | 03-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.779092359% |
| 4 | 04-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.615614457% |
| 5 | 05-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.580550249% |
| 6 | 06-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.694111213% |
| 7 | 07-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 3.127048063% |
| | | | | 5544573 Manitoba Ltd. | 25% | |
| | | | | 5153247 Manitoba Ltd. | 25% | |
| | | | | 6167471 Manitoba Ltd. | 25% | |
| 8 | 08-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 3.111231618% |
| | | | | 5544573 Manitoba Ltd. | 25% | |
| | | | | 5153247 Manitoba Ltd. | 25% | |
| | | | | 6167471 Manitoba Ltd. | 25% | |
| 9 | 09-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 1.528284892% |
| | | | | 5544573 Manitoba Ltd. | 8.333% | |
| | | | | 6167471 Manitoba Ltd. | 8.334% | |
| | | | | 5153247 Manitoba Ltd. | 8.333% | |
| | | | | Tundra Oil & Gas Partnership | 50.0% | |
| 10 | 10-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 25% | 1.562488053% |
| | | | | 5544573 Manitoba Ltd. | 8.333% | |
| | | | | 6167471 Manitoba Ltd. | 8.334% | |
| | | | | 5153247 Manitoba Ltd. | 8.333% | |
| | | | | Tundra Oil & Gas Partnership | 50.0% | |
| 11 | 11-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.836700563% |
| 12 | 12-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.849687422% |
| 13 | 13-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.853362342% |
| 14 | 14-09-001-24W1M | Tundra Oil & Gas Partnership | 100% | Meggison Resources Ltd. | 100% | 1.788883149% |

| Working Interest | | | | Royalty Interest | | Tract Participation |
|------------------|------------------|------------------------------|-----------|--------------------------------|-----------|---------------------|
| Tract No. | Land Description | Owner | Share (%) | Owner | Share (%) | Tract (%) |
| 15 | 01-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | Caroline Elizabeth Meggison | 25% | 1.670849285% |
| | | | | Douglas Clark Meggison | 25% | |
| | | | | 4442164 Manitoba Ltd. | 50% | |
| 16 | 02-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | Caroline Elizabeth Meggison | 25% | 1.501899199% |
| | | | | Douglas Clark Meggison | 25% | |
| | | | | 4442164 Manitoba Ltd. | 50% | |
| 17 | 03-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.940580292% |
| 18 | 04-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.585655272% |
| 19 | 05-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.693493881% |
| 20 | 06-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.492408416% |
| 21 | 11-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.690942744% |
| 22 | 12-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 1.721429674% |
| 23 | 13-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 2.759289195% |
| 24 | 14-10-001-24W1M | Tundra Oil & Gas Partnership | 100% | 4438851 Manitoba Ltd. | 100% | 2.639252975% |
| 25 | 03-11-001-24W1M | Tundra Oil & Gas Partnership | 100% | Minister of Finance - Manitoba | 100% | 1.293616157% |
| 26 | 04-11-001-24W1M | Tundra Oil & Gas Partnership | 100% | Minister of Finance - Manitoba | 100% | 1.262471634% |
| 27 | 05-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 2.468914554% |
| | | | | 5972435 Manitoba Ltd. | 33.333% | |
| | | | | 6537171 Manitoba Ltd. | 4.167% | |
| | | | | Kevin Lee Adams | 4.167% | |
| | | | | 6537180 Manitoba Ltd. | 8.333% | |
| 28 | 06-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 2.147288747% |
| | | | | 5972435 Manitoba Ltd. | 33.333% | |
| | | | | 6537171 Manitoba Ltd. | 4.167% | |
| | | | | Kevin Lee Adams | 4.167% | |
| | | | | 6537180 Manitoba Ltd. | 8.333% | |
| 29 | 11-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 1.985479337% |
| | | | | James C. Wynne (Estate) | 50.0% | |
| 30 | 12-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 2.140747802% |
| | | | | James C. Wynne (Estate) | 50.0% | |
| 31 | 13-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 2.626214099% |
| | | | | James C. Wynne (Estate) | 50.0% | |
| 32 | 14-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 2.463849160% |
| | | | | James C. Wynne (Estate) | 50.0% | |
| 33 | 15-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 2.177488056% |
| | | | | James C. Wynne (Estate) | 50.0% | |

| Working Interest | | | | Royalty Interest | | Tract Participation |
|------------------|------------------|------------------------------|-----------|---------------------------------------|-----------|---------------------|
| Tract No. | Land Description | Owner | Share (%) | Owner | Share (%) | Tract (%) |
| 34 | 16-14-001-24W1M | Tundra Oil & Gas Partnership | 100% | Nestibo Holdings Ltd. | 50.0% | 2.122860508% |
| | | | | James C. Wynne (Estate) | 50.0% | |
| 35 | 03-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 3.364356485% |
| | | | | 6864512 Manitoba Ltd. | 12.5% | |
| | | | | 6167552 Manitoba Ltd. | 12.5% | |
| | | | | Computershare Trust Company of Canada | 25.0% | |
| 36 | 04-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 3.464141218% |
| | | | | 6864512 Manitoba Ltd. | 12.5% | |
| | | | | 6167552 Manitoba Ltd. | 12.5% | |
| | | | | Computershare Trust Company of Canada | 25.0% | |
| 37 | 05-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 1.790714088% |
| | | | | 6864512 Manitoba Ltd. | 12.5% | |
| | | | | 6167552 Manitoba Ltd. | 12.5% | |
| | | | | Computershare Trust Company of Canada | 25.0% | |
| 38 | 06-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | Tundra Oil & Gas Partnership | 50.0% | 1.815663899% |
| | | | | 6864512 Manitoba Ltd. | 12.5% | |
| | | | | 6167552 Manitoba Ltd. | 12.5% | |
| | | | | Computershare Trust Company of Canada | 25.0% | |
| 39 | 07-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 5922250 Manitoba Ltd. | 100% | 1.479346565% |
| 40 | 08-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 5922250 Manitoba Ltd. | 100% | 1.750821641% |
| 41 | 09-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 100% | 1.704570453% |
| 42 | 10-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 100% | 1.458363451% |
| 43 | 11-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 50% | 1.455258282% |
| | | | | Computershare Trust Company of Canada | 50% | |
| 44 | 12-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 50% | 1.600458086% |
| | | | | Computershare Trust Company of Canada | 50% | |
| 45 | 13-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 50% | 1.835689180% |
| | | | | Computershare Trust Company of Canada | 50% | |
| 46 | 14-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 50% | 1.849111075% |
| | | | | Computershare Trust Company of Canada | 50% | |
| 47 | 15-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 100% | 2.839697725% |
| 48 | 16-15-001-24W1M | Tundra Oil & Gas Partnership | 100% | 2637490 Manitoba Ltd. | 100% | 3.182340791% |
| 49 | 03-16-001-24W1M | Tundra Oil & Gas Partnership | 100% | Minister of Finance - Manitoba | 100% | 2.079862422% |
| 50 | 04-16-001-24W1M | Tundra Oil & Gas Partnership | 100% | Minister of Finance - Manitoba | 100% | 2.129460077% |

100.00000000%

TABLE NO. 2: TRACT FACTOR CALCULATIONS FOR GOODLANDS UNIT NO. 3
TRACT FACTORS BASED ON OIL-IN-PLACE (OOIP) - CUMULATIVE PRODUCTION & LAST 12 MONTHS OF PRODUCTION TO JULY 2016

| LS-SE | Tract | OOIP (m3) | HZ Wells Cum Alloc Prod (m3) | Vert Wells Cum Prodn (m3) | Sum Hz + Vert Alloc Cum Prodn | OOIP - Cum | OOIP-Cum by LSD/Total OOIP | Last 12 Mths Alloc Prod (m3) | Vt Wells Last 12 Mths Prod (m3) | Sum Hz + Vert Alloc Last 12 Mths Prod (m3) | Last 12 Mths Prod by LSD/Total Prod | 50% OOIP-Cum + 50% Last 12 Mths Prod Tract Factor |
|-------|-----------------|-----------|------------------------------|---------------------------|-------------------------------|------------|----------------------------|------------------------------|---------------------------------|--|-------------------------------------|---|
| 01-09 | 01-09-001-24W1M | 121,217 | 9,811.6 | 1,922.9 | 11,734.5 | 109,482 | 0.01935403230 | 464.5 | 0.0 | 464.5 | 0.014479006 | 0.01691651890 |
| 02-09 | 02-09-001-24W1M | 123,040 | 9,104.2 | 3,244.8 | 12,349.0 | 110,691 | 0.01956777621 | 525.1 | 0.0 | 525.1 | 0.016366370 | 0.01796707306 |
| 03-09 | 03-09-001-24W1M | 124,700 | 9,232.2 | 4,595.5 | 13,827.7 | 110,872 | 0.01959979124 | 420.8 | 91.9 | 512.7 | 0.015982056 | 0.01779092359 |
| 04-09 | 04-09-001-24W1M | 125,522 | 7,587.0 | 5,102.0 | 12,689.0 | 112,833 | 0.01994641086 | 273.1 | 123.6 | 396.7 | 0.012365878 | 0.01615614457 |
| 05-09 | 05-09-001-24W1M | 126,282 | 4,837.9 | 2,100.4 | 6,938.3 | 119,344 | 0.02109735034 | 299.7 | 37.6 | 337.3 | 0.010513655 | 0.01580550249 |
| 06-09 | 06-09-001-24W1M | 125,630 | 5,341.2 | 2,913.7 | 8,254.9 | 117,375 | 0.02074935768 | 401.1 | 20.2 | 421.3 | 0.013132867 | 0.01694111213 |
| 07-09 | 07-09-001-24W1M | 123,880 | 6,056.8 | 3,371.7 | 9,428.5 | 114,451 | 0.02023246226 | 1,357.4 | 0.0 | 1,357.4 | 0.042308499 | 0.03127048063 |
| 08-09 | 08-09-001-24W1M | 121,568 | 6,802.9 | 4,300.2 | 11,103.1 | 110,465 | 0.01952776555 | 1,312.0 | 57.8 | 1,369.8 | 0.042696867 | 0.03111231618 |
| 09-09 | 09-09-001-24W1M | 124,307 | 2,266.4 | 4,515.4 | 6,781.8 | 117,526 | 0.02077593813 | 314.1 | 0.0 | 314.1 | 0.009789760 | 0.01528284892 |
| 10-09 | 10-09-001-24W1M | 126,142 | 2,189.4 | 886.0 | 3,075.4 | 123,067 | 0.02175547880 | 304.6 | 0.0 | 304.6 | 0.009494282 | 0.01562488053 |
| 11-09 | 11-09-001-24W1M | 126,880 | 6,401.8 | 2,229.5 | 8,631.3 | 118,249 | 0.02090373931 | 507.9 | 0.0 | 507.9 | 0.015830272 | 0.01836700563 |
| 12-09 | 12-09-001-24W1M | 127,400 | 6,519.0 | 2,825.6 | 9,344.6 | 118,055 | 0.02086955053 | 517.3 | 0.0 | 517.3 | 0.016124198 | 0.01849687422 |
| 13-09 | 13-09-001-24W1M | 129,271 | 3,322.4 | 2,074.6 | 5,397.0 | 123,874 | 0.02189819299 | 486.7 | 0.0 | 486.7 | 0.015169054 | 0.01853362342 |
| 14-09 | 14-09-001-24W1M | 128,136 | 3,186.4 | 4,293.2 | 7,479.6 | 120,656 | 0.02132936070 | 463.5 | 0.0 | 463.5 | 0.014448302 | 0.01788883149 |
| 01-10 | 01-10-001-24W1M | 110,118 | 8,876.6 | 0.0 | 8,876.6 | 101,241 | 0.01789720824 | 497.9 | 0.0 | 497.9 | 0.015519777 | 0.01670849285 |
| 02-10 | 02-10-001-24W1M | 116,306 | 5,195.6 | 2,870.7 | 8,066.3 | 108,239 | 0.01913431266 | 349.8 | 0.0 | 349.8 | 0.010903671 | 0.01501899199 |
| 03-10 | 03-10-001-24W1M | 120,047 | 13,050.9 | 2,410.5 | 15,461.4 | 104,585 | 0.01848835754 | 652.0 | 0.0 | 652.0 | 0.020323248 | 0.01940580292 |
| 04-10 | 04-10-001-24W1M | 121,008 | 8,266.1 | 3,013.2 | 11,279.3 | 109,729 | 0.01939768966 | 395.1 | 0.0 | 395.1 | 0.012315416 | 0.01585655272 |
| 05-10 | 05-10-001-24W1M | 122,199 | 8,171.7 | 6,160.9 | 14,332.6 | 107,867 | 0.01906845063 | 359.0 | 115.9 | 474.9 | 0.014801427 | 0.01693493881 |
| 06-10 | 06-10-001-24W1M | 122,382 | 7,195.5 | 4,129.8 | 11,325.3 | 111,057 | 0.01963239630 | 325.0 | 2.7 | 327.7 | 0.010215772 | 0.01492408416 |
| 11-10 | 11-10-001-24W1M | 123,093 | 7,630.8 | 5,127.9 | 12,758.7 | 110,334 | 0.01950462599 | 459.2 | 0.0 | 459.2 | 0.014314229 | 0.01690942744 |
| 12-10 | 12-10-001-24W1M | 123,573 | 7,833.5 | 4,574.9 | 12,408.4 | 111,164 | 0.01965143267 | 474.1 | 0.0 | 474.1 | 0.014777161 | 0.01721429674 |
| 13-10 | 13-10-001-24W1M | 123,834 | 3,881.3 | 6,579.0 | 10,460.3 | 113,373 | 0.02004190532 | 1,102.0 | 25.5 | 1,127.5 | 0.035143879 | 0.02759289195 |
| 14-10 | 14-10-001-24W1M | 121,239 | 3,771.7 | 4,850.0 | 8,621.7 | 112,617 | 0.01990824272 | 1,054.8 | 0.0 | 1,054.8 | 0.032876817 | 0.02639252975 |
| 03-11 | 03-11-001-24W1M | 112,008 | 5,742.7 | 0.0 | 5,742.7 | 106,265 | 0.01878538533 | 227.4 | 0.0 | 227.4 | 0.007086938 | 0.01293616157 |
| 04-11 | 04-11-001-24W1M | 110,433 | 5,429.5 | 0.0 | 5,429.5 | 105,003 | 0.01856223606 | 214.5 | 0.0 | 214.5 | 0.006687197 | 0.01262471634 |
| 05-14 | 05-14-001-24W1M | 122,094 | 5,000.3 | 5,482.0 | 10,482.3 | 111,612 | 0.01973054353 | 783.0 | 168.2 | 951.2 | 0.029647748 | 0.02468914554 |
| 06-14 | 06-14-001-24W1M | 121,250 | 5,106.6 | 2,640.4 | 7,747.0 | 113,503 | 0.02006484473 | 734.1 | 0.0 | 734.1 | 0.022880930 | 0.02147288747 |
| 11-14 | 11-14-001-24W1M | 119,800 | 5,822.1 | 2,018.6 | 7,840.7 | 111,959 | 0.01979196516 | 639.0 | 0.0 | 639.0 | 0.019917622 | 0.01985479337 |
| 12-14 | 12-14-001-24W1M | 121,431 | 5,884.9 | 4,963.0 | 10,847.9 | 110,583 | 0.01954870761 | 746.4 | 0.0 | 746.4 | 0.023266248 | 0.02140747802 |
| 13-14 | 13-14-001-24W1M | 120,843 | 10,003.1 | 0.0 | 10,003.1 | 110,840 | 0.01959406400 | 1,056.5 | 0.0 | 1,056.5 | 0.032930218 | 0.02626214099 |
| 14-14 | 14-14-001-24W1M | 119,318 | 9,763.4 | 3,444.5 | 13,207.9 | 106,110 | 0.01875799156 | 940.2 | 38.9 | 979.1 | 0.030518992 | 0.02463849160 |
| 15-14 | 15-14-001-24W1M | 118,320 | 4,031.5 | 3,430.7 | 7,462.2 | 110,858 | 0.01959720771 | 768.5 | 0.0 | 768.5 | 0.023952553 | 0.02177488056 |
| 16-14 | 16-14-001-24W1M | 120,163 | 3,412.7 | 3,225.2 | 6,637.9 | 113,525 | 0.02006867524 | 718.3 | 0.0 | 718.3 | 0.022388535 | 0.02122860508 |
| 03-15 | 03-15-001-24W1M | 121,829 | 7,676.9 | 0.0 | 7,676.9 | 114,152 | 0.02017953357 | 1,511.3 | 0.0 | 1,511.3 | 0.047107596 | 0.03364356485 |

| LS-SE | Tract | OOIP (m3) | HZ Wells Cum Alloc Prod (m3) | Vert Wells Cum Prodn (m3) | Sum Hz + Vert Alloc Cum Prodn | OOIP - Cum | OOIP-Cum by LSD/Total OOIP | Last 12 Mths Alloc Prod (m3) | Vt Wells Last 12 Mths Prod (m3) | Sum Hz + Vert Alloc Last 12 Mths Prod (m3) | Last 12 Mths Prod by LSD/Total Prod | 50% OOIP-Cum + 50% Last 12 Mths Prod Tract Factor |
|-------|-----------------|------------------|------------------------------|---------------------------|-------------------------------|------------------|----------------------------|------------------------------|---------------------------------|--|-------------------------------------|---|
| 04-15 | 04-15-001-24W1M | 124,598 | 7,367.2 | 0.0 | 7,367.2 | 117,231 | 0.02072388057 | 1,557.9 | 0.0 | 1,557.9 | 0.048558944 | 0.03464141218 |
| 05-15 | 05-15-001-24W1M | 125,885 | 10,502.4 | 4,579.4 | 15,081.8 | 110,803 | 0.01958748396 | 520.6 | 0.0 | 520.6 | 0.016226798 | 0.01790714088 |
| 06-15 | 06-15-001-24W1M | 123,708 | 10,625.7 | 2,926.8 | 13,552.5 | 110,155 | 0.01947306595 | 540.3 | 0.0 | 540.3 | 0.016840212 | 0.01815663899 |
| 07-15 | 07-15-001-24W1M | 122,053 | 6,021.3 | 2,863.2 | 8,884.5 | 113,168 | 0.02000568814 | 307.4 | 0.0 | 307.4 | 0.009581243 | 0.01479346565 |
| 08-15 | 08-15-001-24W1M | 122,293 | 6,503.0 | 4,121.8 | 10,624.8 | 111,668 | 0.01974048128 | 490.1 | 0.0 | 490.1 | 0.015275952 | 0.01750821641 |
| 09-15 | 09-15-001-24W1M | 122,241 | 3,737.9 | 3,223.6 | 6,961.5 | 115,279 | 0.02037880080 | 326.1 | 113.8 | 439.9 | 0.013712608 | 0.01704570453 |
| 10-15 | 10-15-001-24W1M | 122,357 | 2,970.5 | 3,142.9 | 6,113.4 | 116,243 | 0.02054923814 | 125.9 | 150.6 | 276.5 | 0.008618031 | 0.01458363451 |
| 11-15 | 11-15-001-24W1M | 123,883 | 7,131.9 | 1,793.3 | 8,925.2 | 114,958 | 0.02032199495 | 281.8 | 0.0 | 281.8 | 0.008783171 | 0.01455258282 |
| 12-15 | 12-15-001-24W1M | 125,783 | 6,695.7 | 3,667.2 | 10,362.9 | 115,420 | 0.02040370675 | 236.8 | 135.5 | 372.3 | 0.011605455 | 0.01600458086 |
| 13-15 | 13-15-001-24W1M | 127,180 | 8,514.3 | 0.0 | 8,514.3 | 118,666 | 0.02097753765 | 504.9 | 0.0 | 504.9 | 0.015736246 | 0.01835689180 |
| 14-15 | 14-15-001-24W1M | 124,206 | 8,705.6 | 0.0 | 8,705.6 | 115,500 | 0.02041786139 | 531.4 | 0.0 | 531.4 | 0.016564360 | 0.01849111075 |
| 15-15 | 15-15-001-24W1M | 122,465 | 10,275.2 | 0.0 | 10,275.2 | 112,190 | 0.01983264298 | 1,185.8 | 0.0 | 1,185.8 | 0.036961312 | 0.02839697725 |
| 16-15 | 16-15-001-24W1M | 121,799 | 11,324.8 | 0.0 | 11,324.8 | 110,474 | 0.01952933439 | 1,415.4 | 0.0 | 1,415.4 | 0.044117481 | 0.03182340791 |
| 03-16 | 03-16-001-24W1M | 127,904 | 6,446.3 | 0.0 | 6,446.3 | 121,457 | 0.02147099783 | 645.7 | 0.0 | 645.7 | 0.020126251 | 0.02079862422 |
| 04-16 | 04-16-001-24W1M | 128,796 | 6,753.8 | 0.0 | 6,753.8 | 122,042 | 0.02157430210 | 674.2 | 0.0 | 674.2 | 0.021014899 | 0.02129460077 |
| | | 6,130,410 | 337,982.5 | 135,615.0 | | 5,656,812 | 1.00000000000 | | | 32,082.2 | 1.000000000 | 1.00000000000 |

Table No. 4: OOIP Calculation

| LSD | OOIP (bbls) | OOIP (m3) |
|--------------|-------------|-----------|
| 1-9-1-24W1 | 762430 | 121217 |
| 2-9-1-24W1 | 773900 | 123040 |
| 3-9-1-24W1 | 784340 | 124700 |
| 4-9-1-24W1 | 789510 | 125522 |
| 5-9-1-24W1 | 794290 | 126282 |
| 6-9-1-24W1 | 790190 | 125630 |
| 7-9-1-24W1 | 779180 | 123880 |
| 8-9-1-24W1 | 764640 | 121568 |
| 9-9-1-24W1 | 781870 | 124307 |
| 10-9-1-24W1 | 793410 | 126142 |
| 11-9-1-24W1 | 798050 | 126880 |
| 12-9-1-24W1 | 801320 | 127400 |
| 13-9-1-24W1 | 813090 | 129271 |
| 14-9-1-24W1 | 805950 | 128136 |
| 1-10-1-24W1 | 692620 | 110118 |
| 2-10-1-24W1 | 731540 | 116306 |
| 3-10-1-24W1 | 755070 | 120047 |
| 4-10-1-24W1 | 761120 | 121008 |
| 5-10-1-24W1 | 768610 | 122199 |
| 6-10-1-24W1 | 769760 | 122382 |
| 11-10-1-24W1 | 774230 | 123093 |
| 12-10-1-24W1 | 777250 | 123573 |
| 13-10-1-24W1 | 778890 | 123834 |
| 14-10-1-24W1 | 762570 | 121239 |
| 3-11-1-24W1 | 704510 | 112008 |
| 4-11-1-24W1 | 694600 | 110433 |

| LSD | OOIP (bbls) | OOIP (m3) |
|--------------|-------------|-----------|
| 5-14-1-24W1 | 767950 | 122094 |
| 6-14-1-24W1 | 762640 | 121250 |
| 11-14-1-24W1 | 753520 | 119800 |
| 12-14-1-24W1 | 763780 | 121431 |
| 13-14-1-24W1 | 760080 | 120843 |
| 14-14-1-24W1 | 750490 | 119318 |
| 15-14-1-24W1 | 744210 | 118320 |
| 16-14-1-24W1 | 755800 | 120163 |
| 3-15-1-24W1 | 766280 | 121829 |
| 4-15-1-24W1 | 783700 | 124598 |
| 5-15-1-24W1 | 791790 | 125885 |
| 6-15-1-24W1 | 778100 | 123708 |
| 7-15-1-24W1 | 767690 | 122053 |
| 8-15-1-24W1 | 769200 | 122293 |
| 9-15-1-24W1 | 768870 | 122241 |
| 10-15-1-24W1 | 769600 | 122357 |
| 11-15-1-24W1 | 779200 | 123883 |
| 12-15-1-24W1 | 791150 | 125783 |
| 13-15-1-24W1 | 799940 | 127180 |
| 14-15-1-24W1 | 781230 | 124206 |
| 15-15-1-24W1 | 770280 | 122465 |
| 16-15-1-24W1 | 766090 | 121799 |
| 3-16-1-24W1 | 804490 | 127904 |
| 4-16-1-24W1 | 810100 | 128796 |

TOTAL 38559120 6130410

Sw = 40%
Porosity = 10%
Bo = 1.17

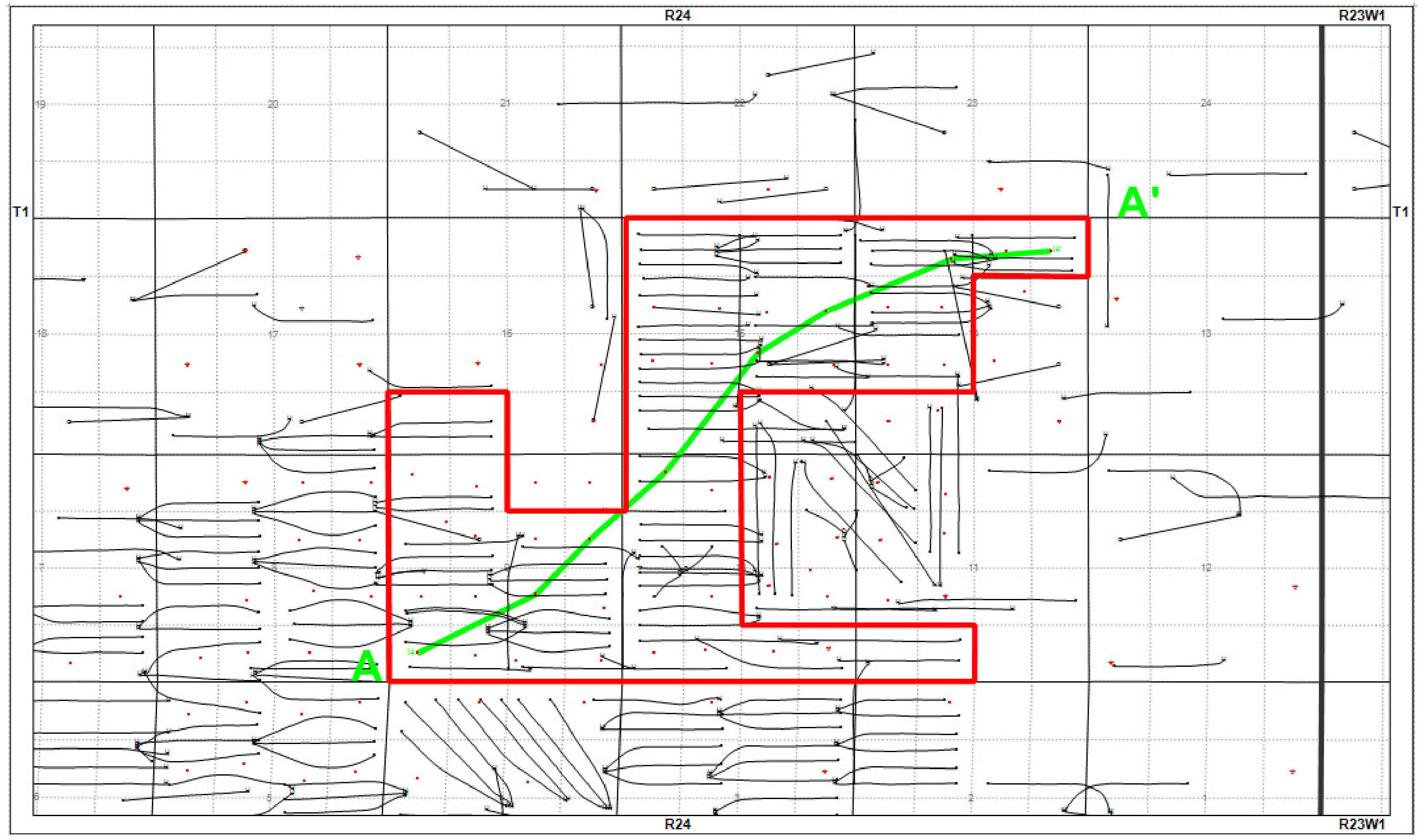
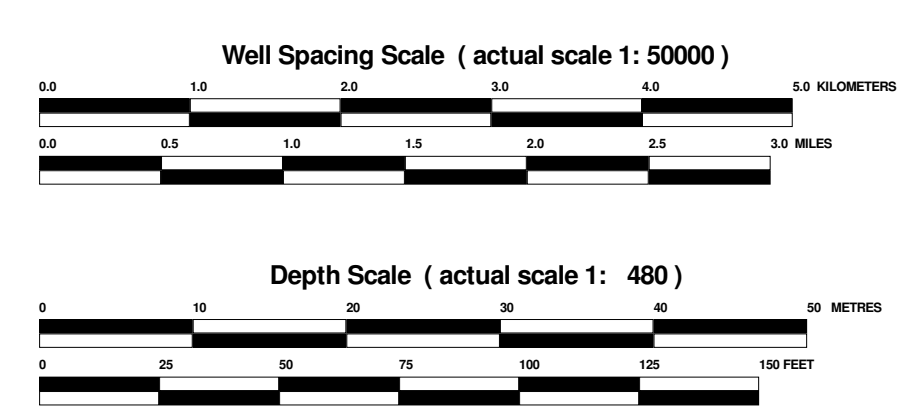
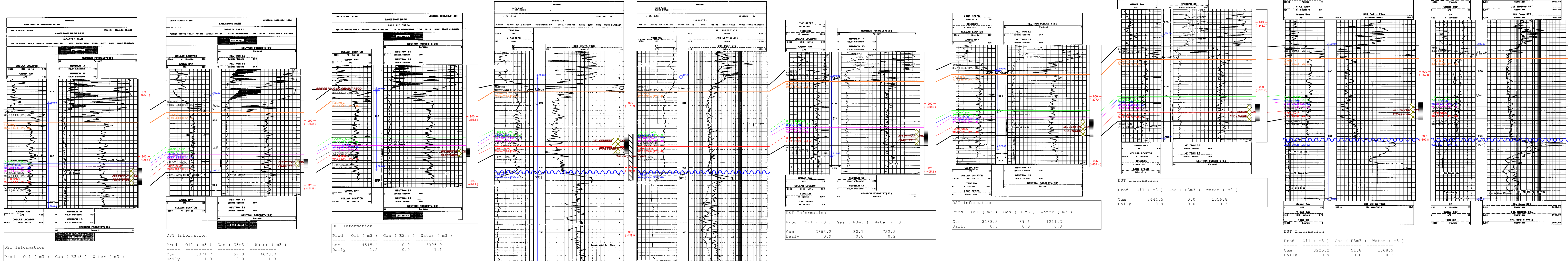
Table No. 5**Proposed Goodlands Unit No. 3****LOWER AMARANTH FORMATION ROCK & FLUID PARAMETERS**

| | | |
|---------------------------------|--|------------------------------------|
| Formation Pressure | 8500 kPa | Initial Average Reservoir Pressure |
| Formation Temperature | 45 C | |
| Saturation Pressure | 4220 kPa | Bubble Point |
| GOR | 20 - 50 m ³ /m ³ | Gas Oil Ratio |
| API Oil Gravity | 37.2 | |
| Swi (fraction) | 0.40 | Initial Water Saturation |
| Produced Water Specific Gravity | 1.08 | |
| Produced Water pH | 7.1 - 7.3 | |
| Produced Water TDS | 180,000 | |
| Wettability | Moderately oil-wet | |

| | | | | | | | |
|---|---|---|--|--|--|---|--|
| 00/04-09-001-24W1/0 KB: 490.4 m RR: 2004-09-18 TD: 920.0 m [TV] FormID: AMRNTHL Mode: Prod Fluid: Oil TUNDRA WASKADA 4-9-1-24(WPM) 933.8m to next well | 00/07-09-001-24W1/0 KB: 513.2 m RR: 2004-07-05 TD: 920.0 m [TV] FormID: TILSTNBD Mode: Prod Fluid: Oil TUNDRA WASKADA 7-9-1-24 (WPM) 541.4m to next well | 00/09-09-001-24W1/0 KB: 514.9 m RR: 2004-06-29 TD: 920.0 m [TV] FormID: TILSTNBD Mode: Prod Fluid: Oil TUNDRA WASKADA 9-9-1-24 (WPM) 716.9m to next well | 00/13-10-001-24W1/0 KB: 520.1 m RR: 1996-11-19 TD: 985.0 m [TV] FormID: LODGEPOL Mode: Prod Fluid: Oil TUNDRA ET AL GOODLANDS 13-10-1-24 1059.0m to next well | 00/07-15-001-24W1/0 KB: 519.8 m RR: 2004-06-15 TD: 925.0 m [TV] FormID: AMRNTHL Mode: Prod Fluid: Oil TUNDRA WASKADA 7-15-1-24(WPM) 564.9m to next well | 00/09-15-001-24W1/0 KB: 522.6 m RR: 2004-08-07 TD: 925.0 m [TV] FormID: AMRNTHL Mode: Prod Fluid: Oil TUNDRA WASKADA 9-15-1-24(WPM) 952.8m to next well | 00/14-14-001-24W1/0 KB: 526.3 m RR: 2004-08-17 TD: 922.0 m [TV] FormID: AMRNTHL Mode: Prod Fluid: Oil TUNDRA WASKADA 14-14-1-24(WPM) 700.2m to next well | 00/16-14-001-24W1/0 KB: 522.2 m RR: 2004-08-22 TD: 948.0 m [TV] FormID: TILSTNBD Mode: Prod Fluid: Oil TUNDRA WASKADA 16-14-1-24(WPM) 700.2m to previous well |
|---|---|---|--|--|--|---|--|

A

A'

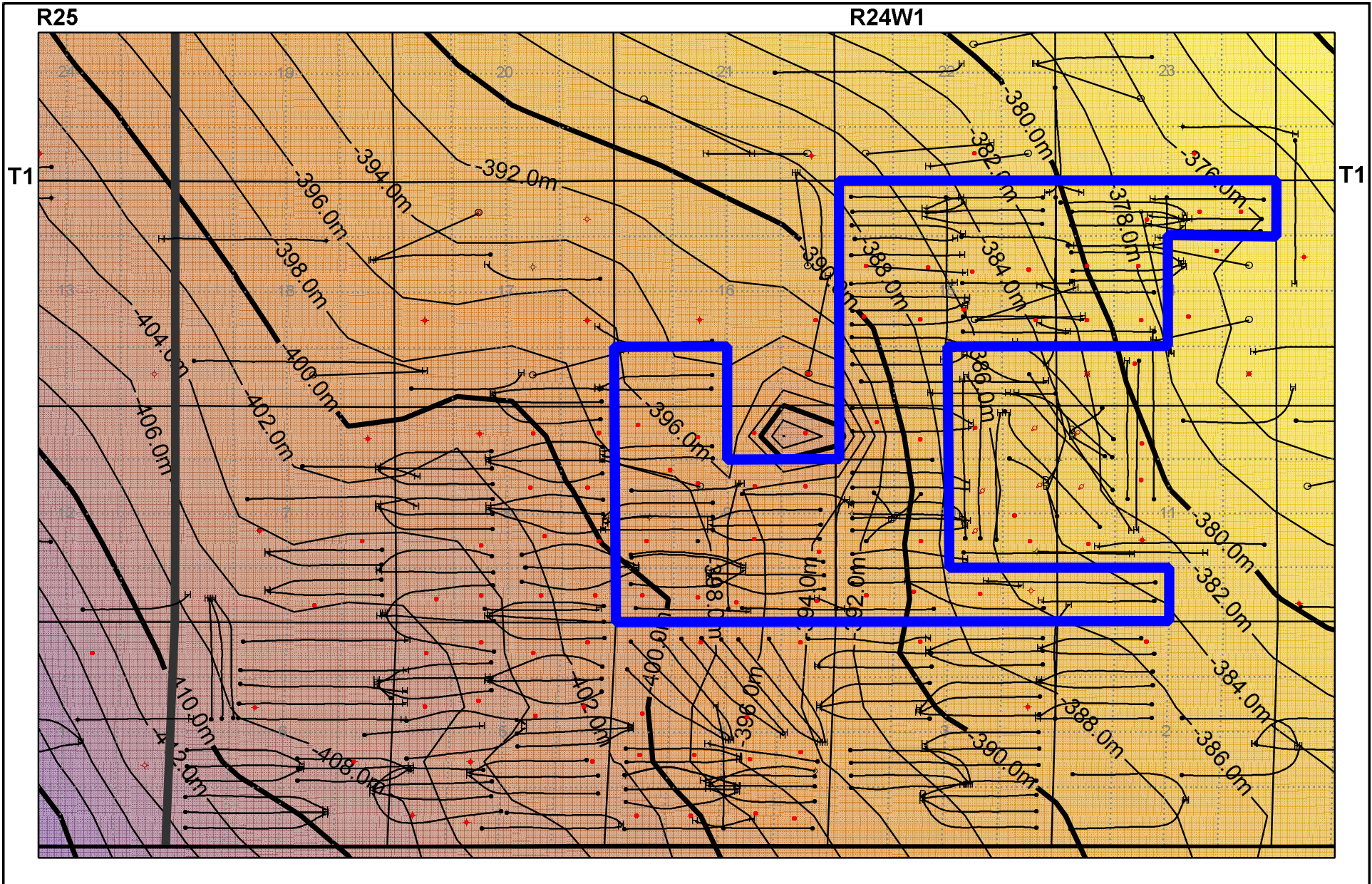


Tundra

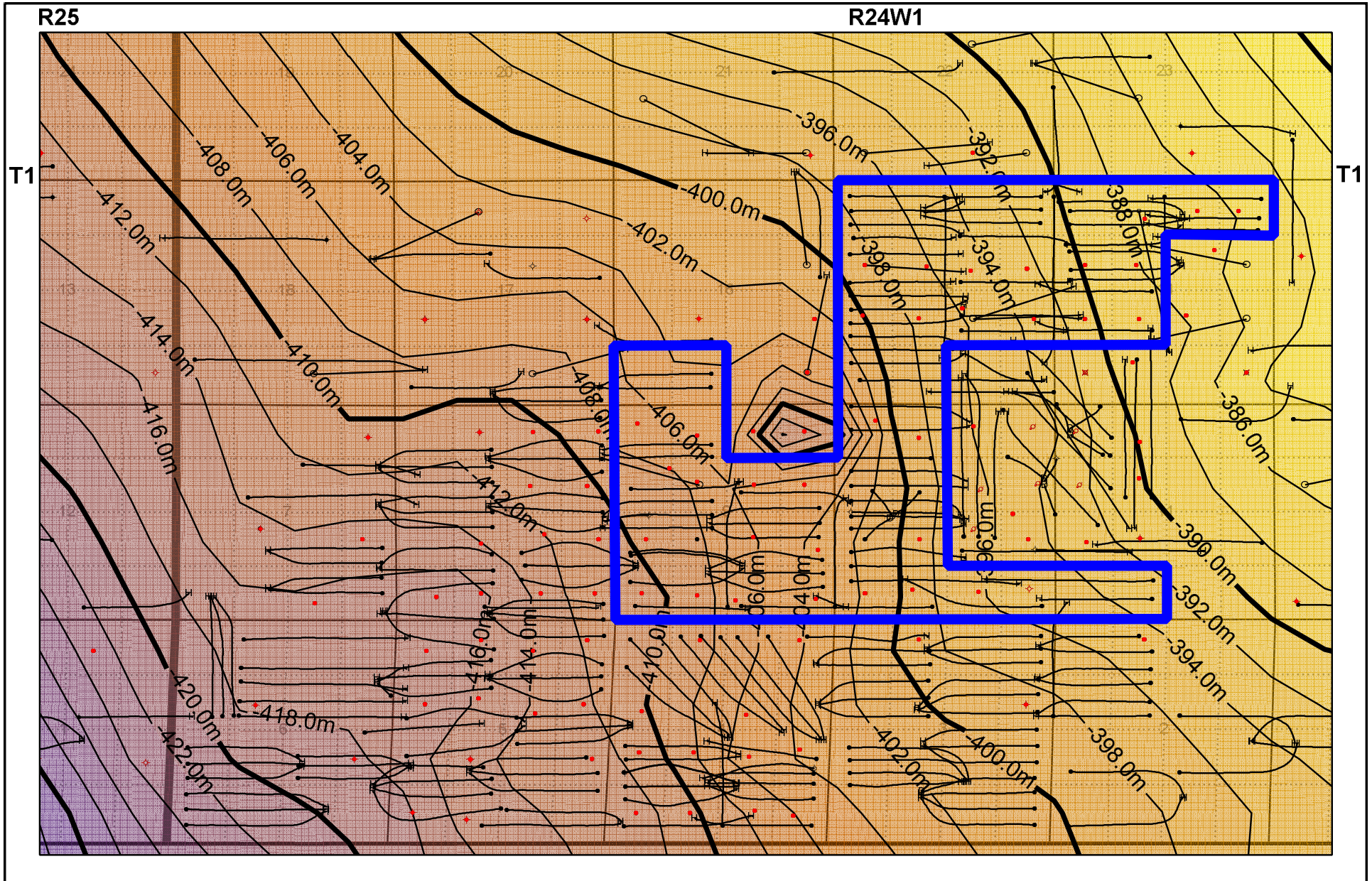
Goodlands Unit 3 Cross Section

Appendix No. 1

| | |
|--|--|
| Produced by: Author: NIS Modified On: Friday, June 03, 2016 04:47PM Vetter: E3, 117846 Datum: NAD83 Copyright 2015, NIS | Author: NIS Modified On: Friday, June 03, 2016 04:47PM Vetter: E3, 117846 Star Formation: 5m above AMRNTHL End Formation: 5m below Top Depth Cross Section Name: WASKADAN14 |
|--|--|

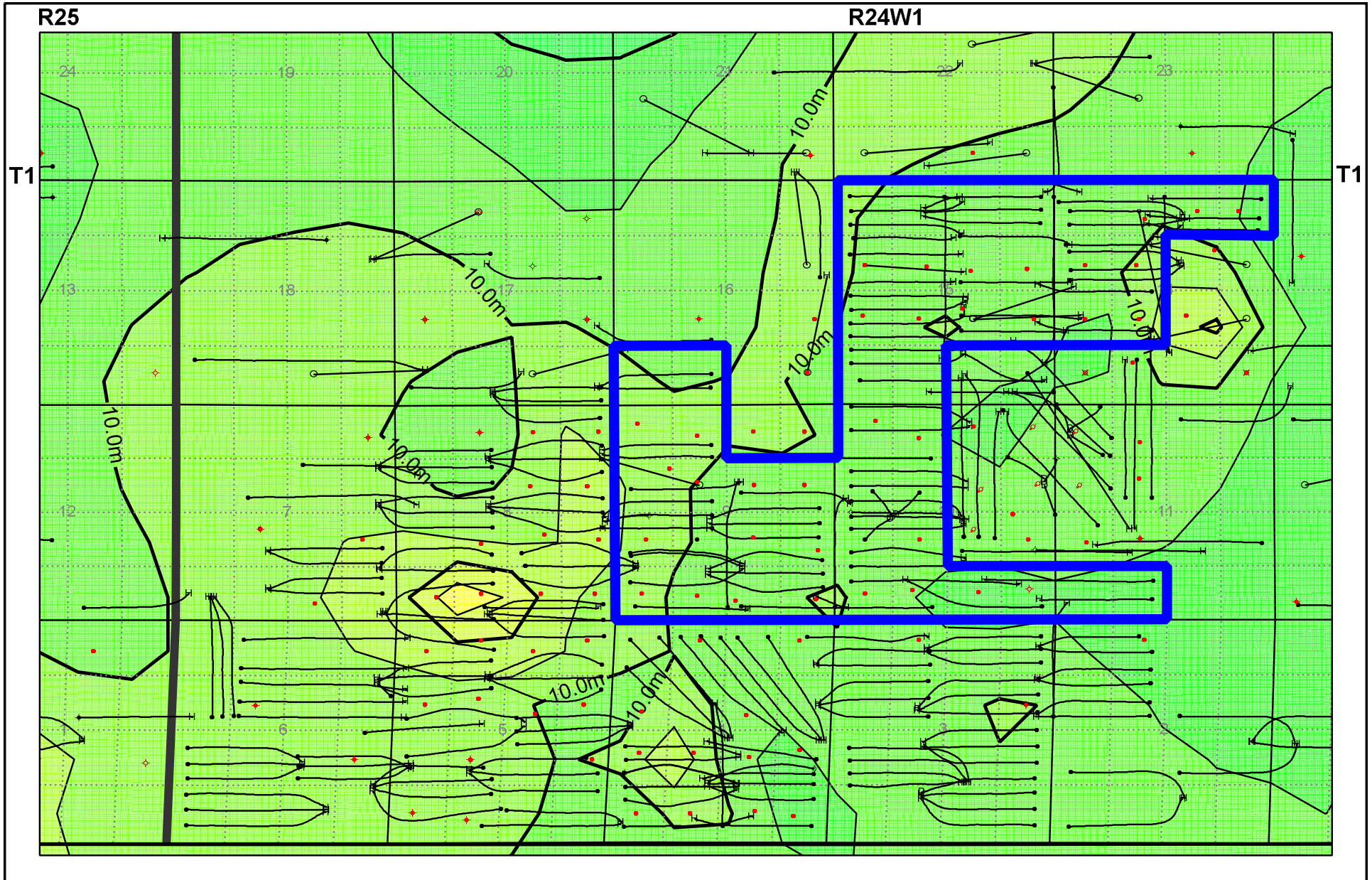


| |
|--|
| Goodlands Unit 3 Application |
| Green Sand Structure (Top of Reservoir) |
| June 07, 2016 |

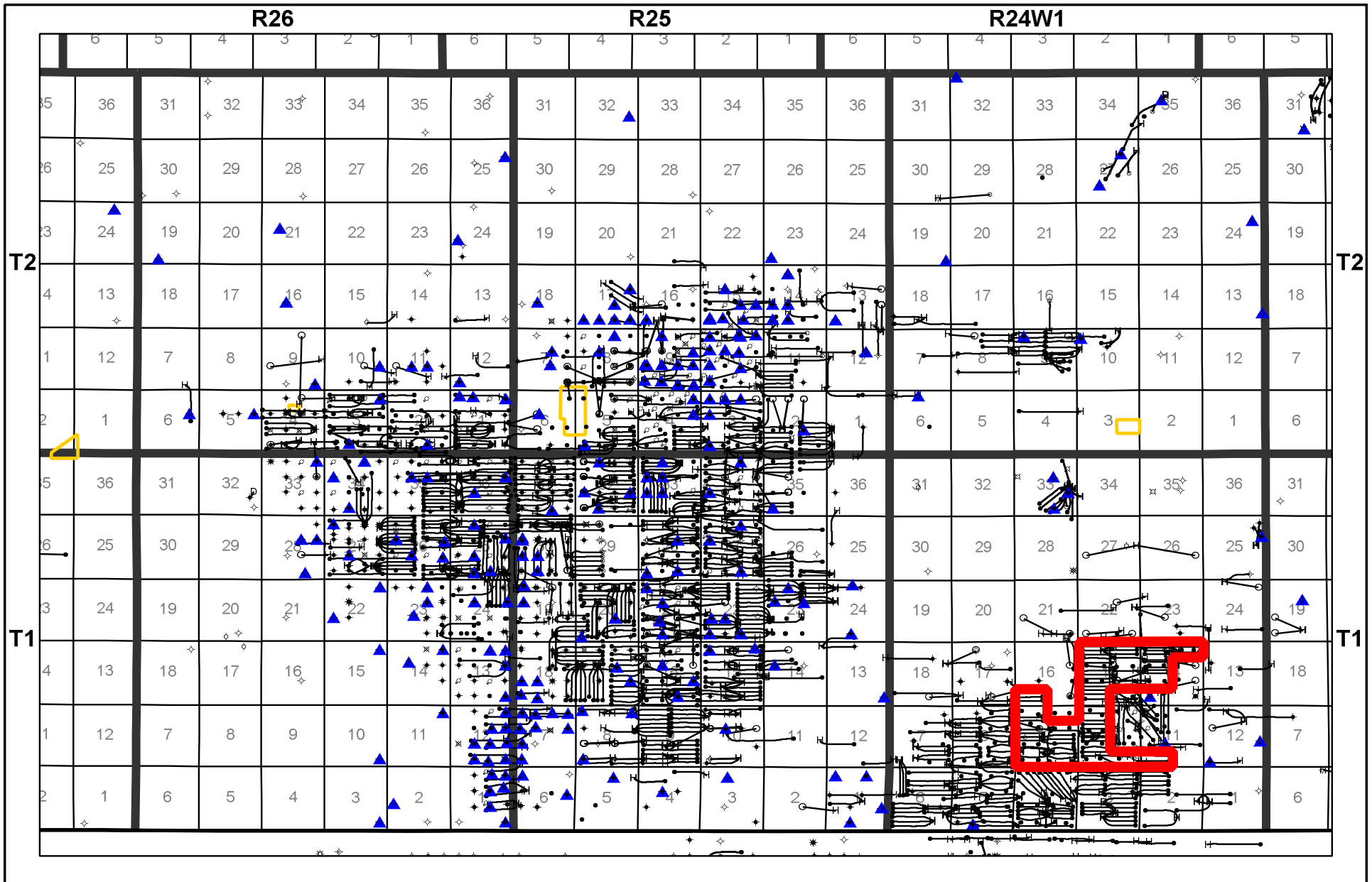


| |
|---|
| Goodlands Unit 3 Application |
| Lower Sand Structure (Base of Reservoir) |
| June 07, 2016 |





| |
|-------------------------------|
| Goodlands Unit 3 Application |
| Reservoir Isopach |
| (Green to Lower Sand Isopach) |
| June 07, 2016 |



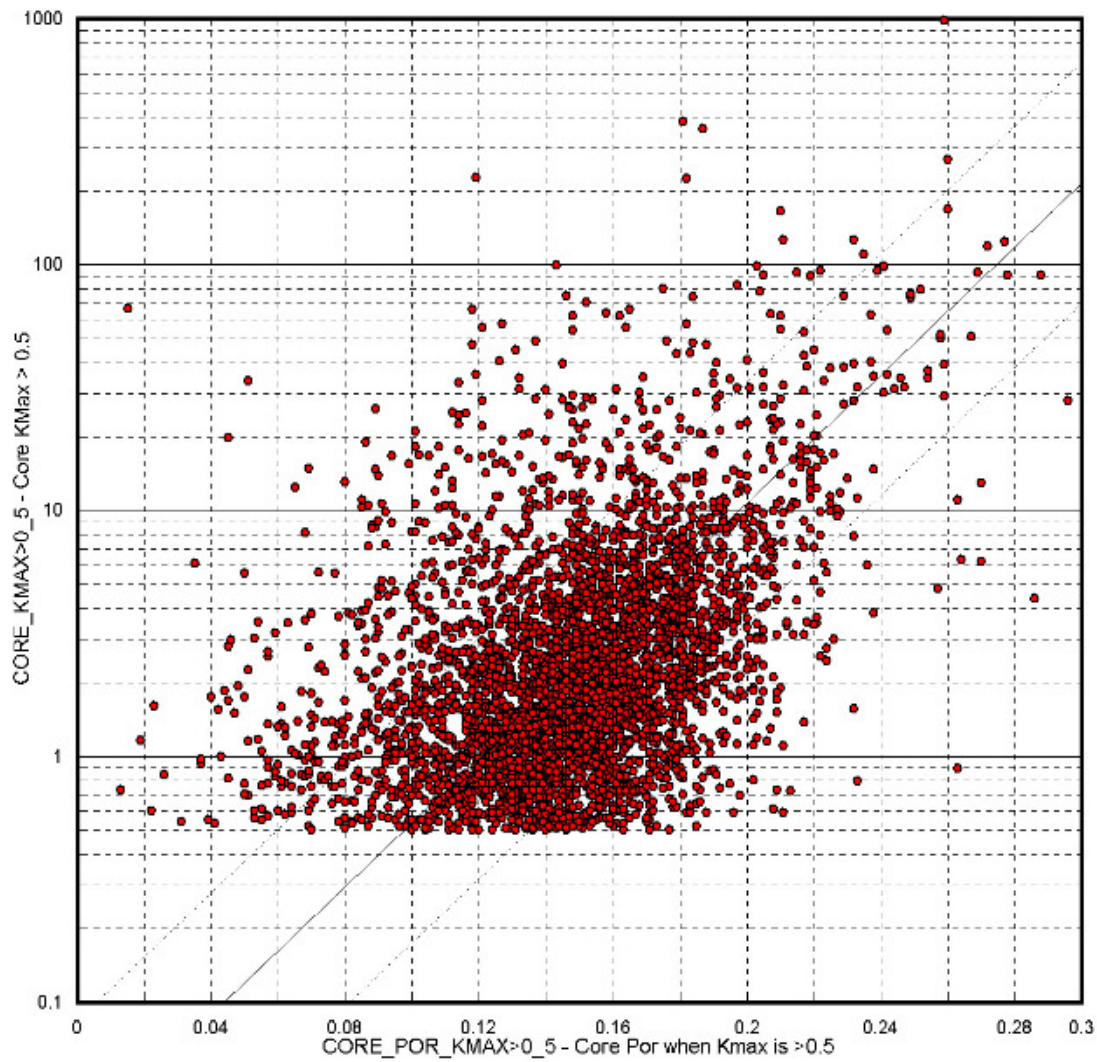
Goodlands Unit 3 Application
 Wells with Core Analysis Used to Create
 Core Perm vs Core Porosity Cross Plot
 June 07, 2016

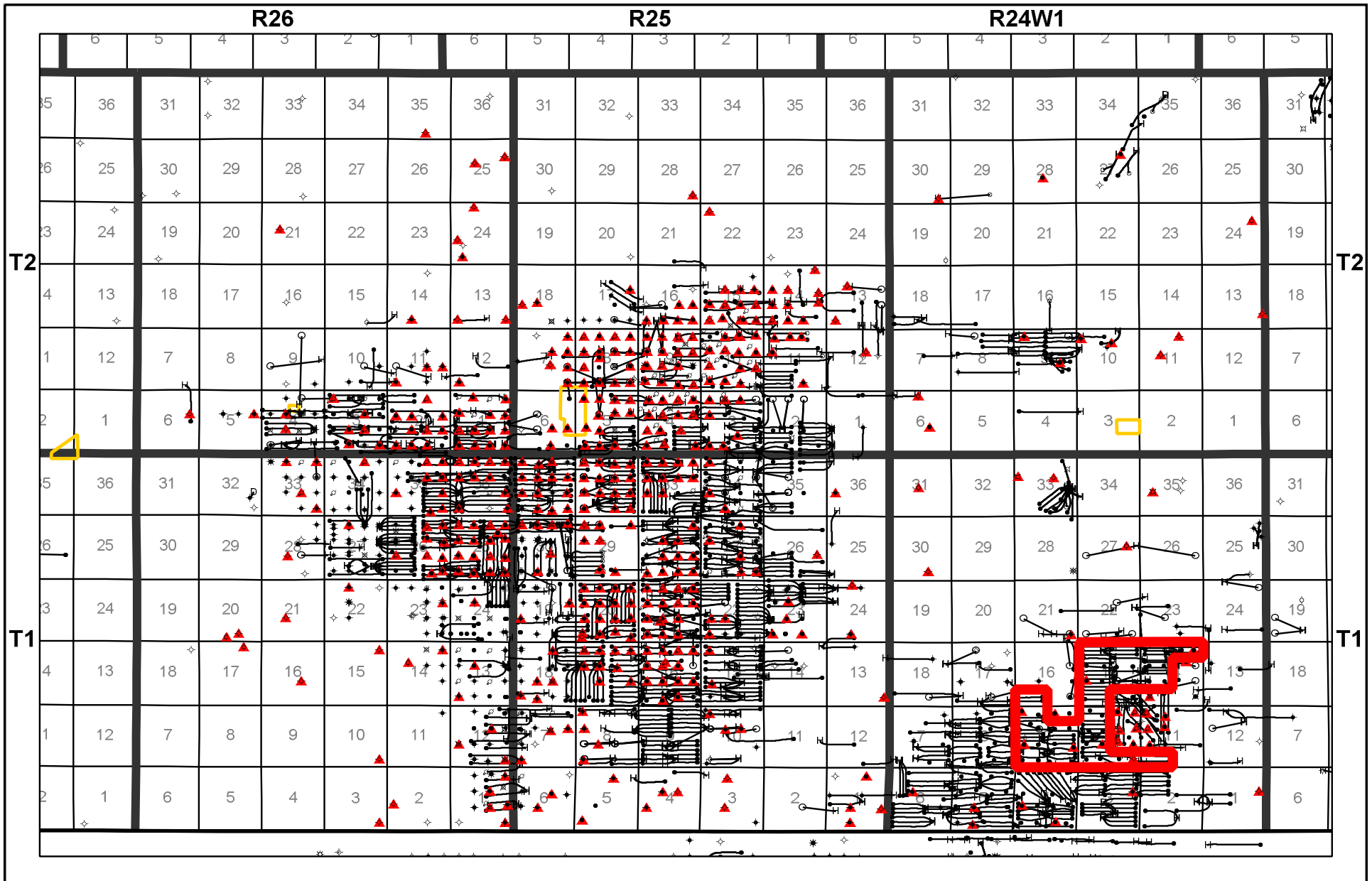


Tundra Pierson Waskada Project

Core Kmax vs Core Porosity >0.5mD

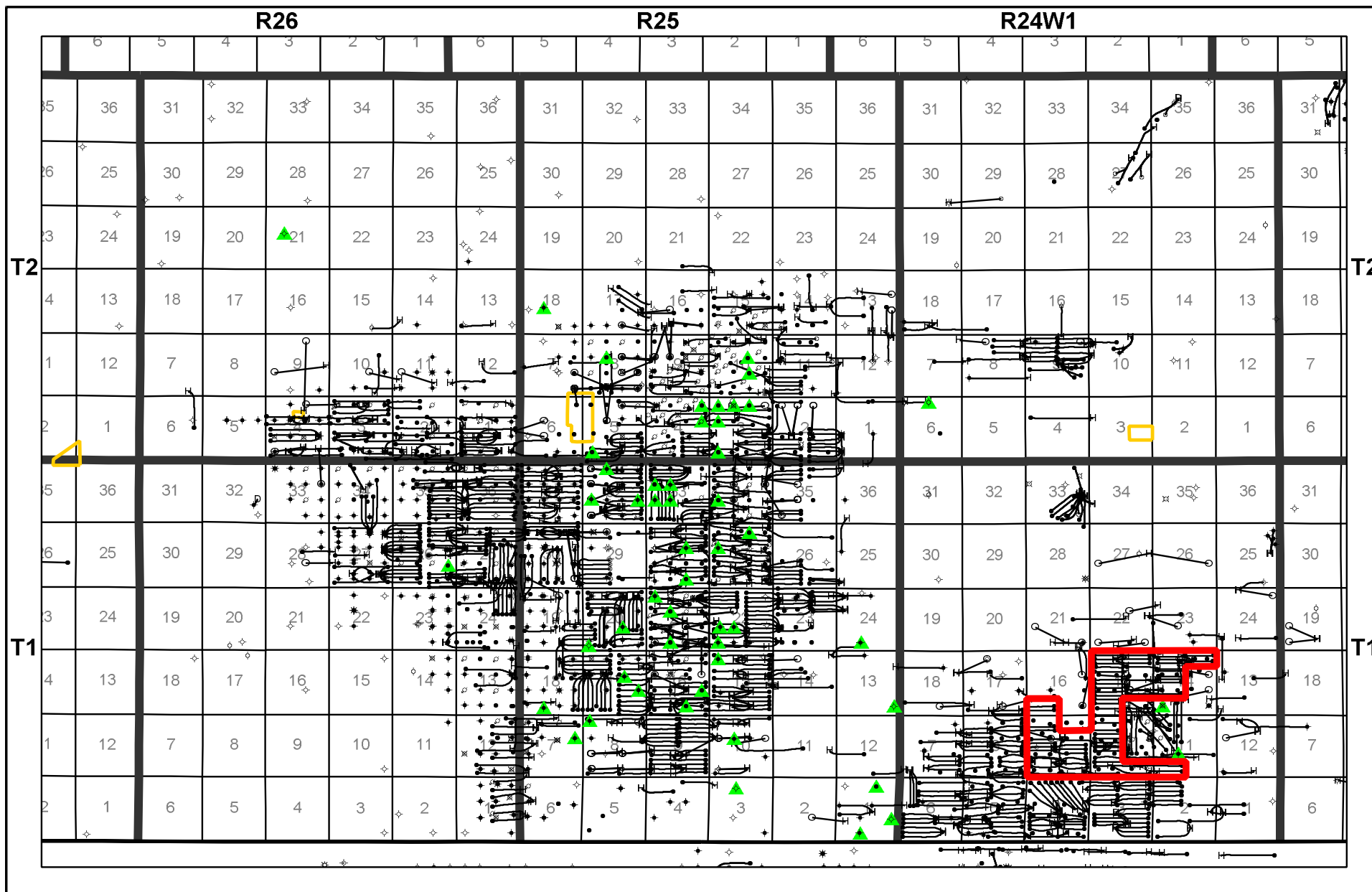
10686 Samples for 231 out of 231 Wells


$$\text{LOG}(\text{CORE_KMAX}>0_5) = 12.99873743 * \text{CORE_POR_KMAX}>0_5 - 1.5681 \quad \text{Corr}=0.422 \quad \text{StdErr}=0.4908$$



| |
|-------------------------------|
| Goodlands Unit 3 Application |
| Wells with Digital Sonic Logs |
| June 07, 2016 |



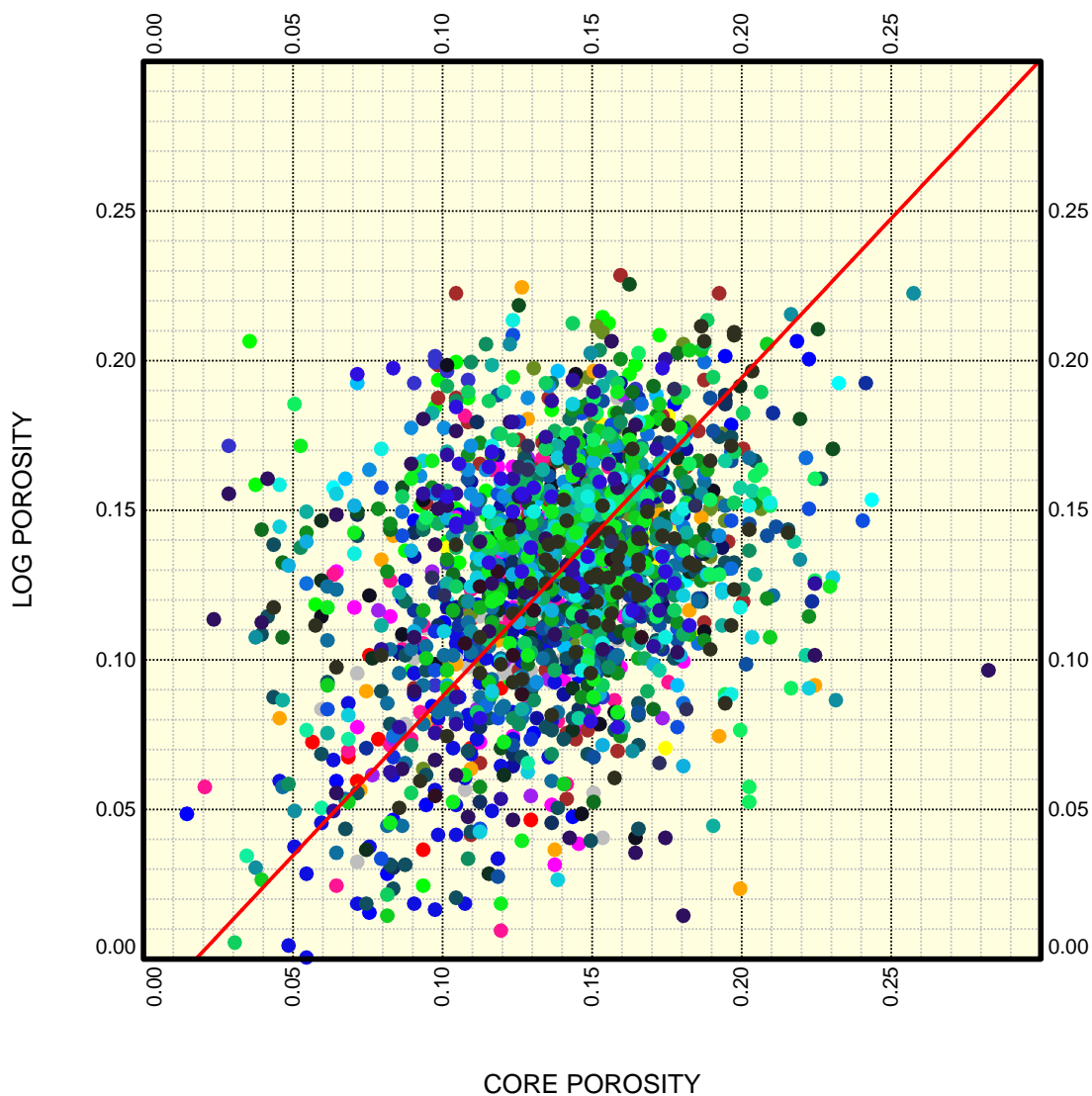


Goodlands Unit 3 Application
 Wells with Digital Sonic Logs and Core Analysis
 over the Lower Amaranth Reservoir Interval
 June 07, 2016



Log Porosity vs Core Porosity Crossplot

Well: 52 Wells



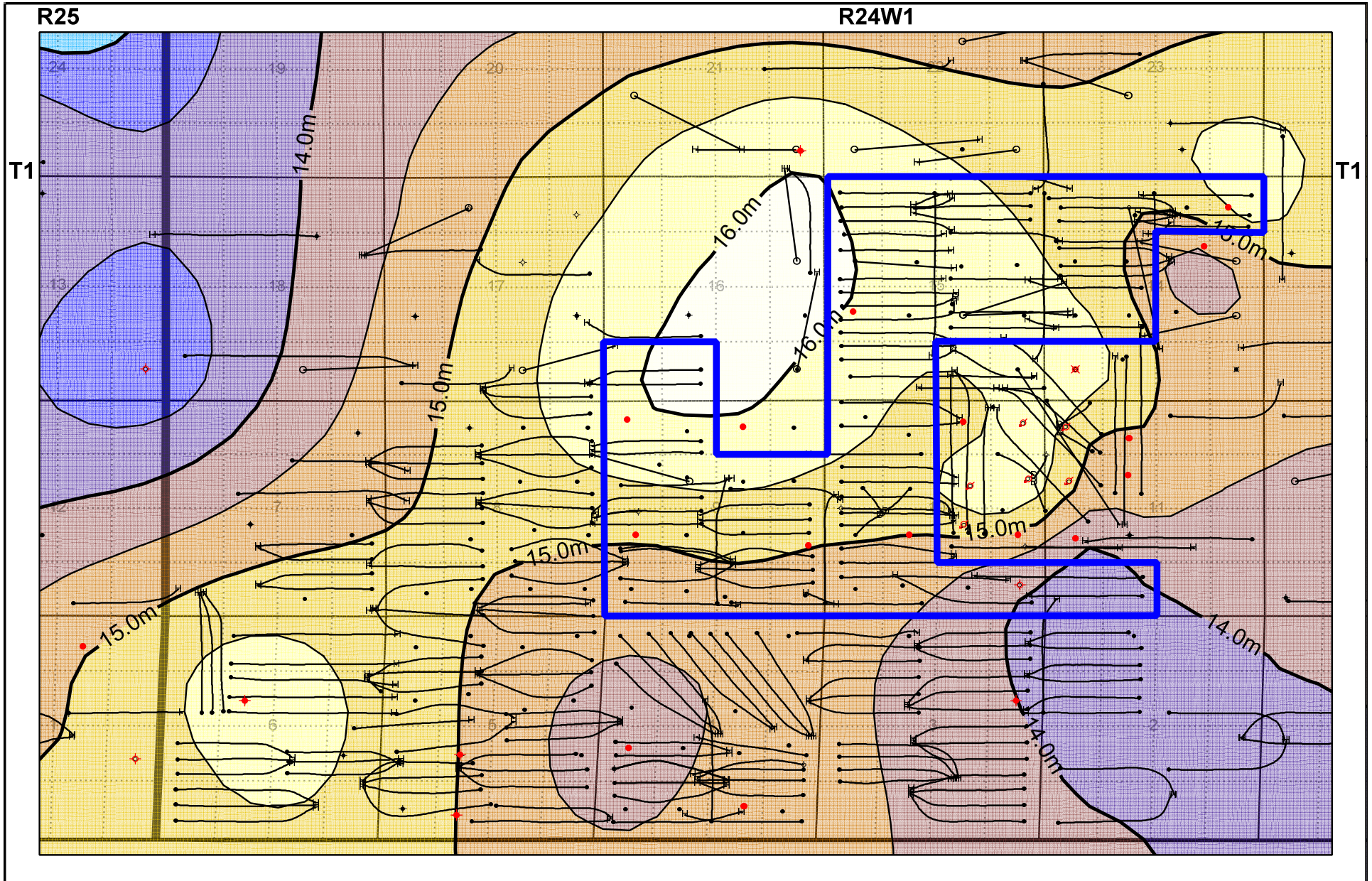
Wells:

| | | | | |
|------------------|------------------|------------------|------------------|------------------|
| 100011300125W100 | 100021600125W100 | 100022800125W100 | 100030100125W100 | 100031800125W100 |
| 100032100125W100 | 100032400125W100 | 100040300225W100 | 100040500225W100 | 100041400124W100 |
| 100042000125W100 | 100042200125W100 | 100052200125W100 | 100053200125W100 | 100053300125W100 |
| 100053400125W100 | 100061100124W100 | 100061800225W100 | 100062200125W100 | 100063300125W100 |
| 100071000225W100 | 100072000125W100 | 100080100125W100 | 100081600125W100 | 100081700125W100 |
| 100082600126W100 | 100083200125W100 | 100090400225W100 | 100090700125W100 | 100101000225W100 |
| 100101700125W100 | 100102800125W100 | 100110800225W100 | 100111000125W100 | 100112100125W100 |
| 100112100226W100 | 100113300125W100 | 100120300225W100 | 100122700125W100 | 100123300125W100 |
| 100130300225W100 | 100130800125W100 | 100131500125W100 | 100132100125W100 | 100140300125W100 |
| 100140300225W100 | 100140600224W100 | 100143200125W100 | 100150100125W100 | 100150300225W100 |
| 100152700125W100 | 100160400225W100 | | | |

Intervals: U-GREEN_SAND U-BLUE_SAND U-PURPLE_SAND U-BROWN_SAND U-RED_SAND U-LWR_SAND

Functions:

test: Regression Logs: CORE.POROSITY, PHIE, CC: 0.329356
 $PHIE = (-0.0186548 + 1.06436*(POROSITY))$

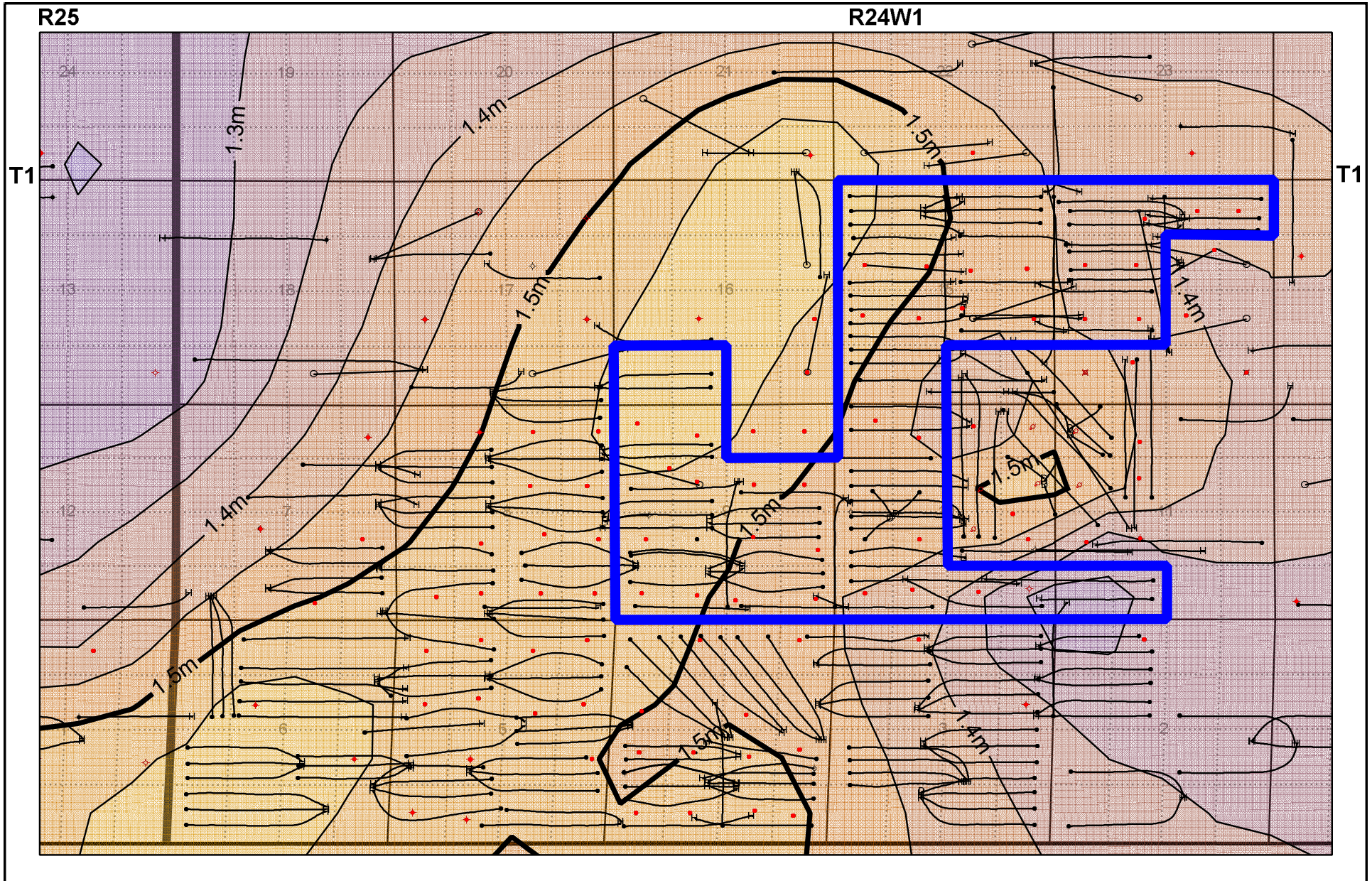


Goodlands Unit 3 Application

Mean Sonic Porosity from Top Green to Base Red
Control Points in Red
Values in Percent

July 12, 2016

REVISIONS



| |
|------------------------------|
| Goodlands Unit 3 Application |
| Phi_h at 10% cut off |
| June 07, 2016 |